

**Supplementary Online Material for “Chlorine (Cl) and hydrogen chloride (HCl)
solubility in hydrous silicate melts: implications for volcanic gas composition” by
Rusiecka, M.K., and Wood, B.J., Contributions to Mineralogy and Petrology**

Equations used for the MRK gas speciation:

Chlorine

Chloride capacity (this study):

$$\log C_{Cl} = 1.15 + \frac{4359X_{Ca} - 3055X_{Si} + 2059X_{Fe} - 3875X_K + 163X_{Mg} - 514P}{T}$$

T in Kelvin, P in GPa, X_M on single cation basis.

HCl fugacity (this study):

$$f_{HCl} = K_{HCl} \times \frac{(f_{H_2O})^{0.5}}{(K_{H_2O})^{0.5}} \times \frac{Cl \text{ (wt.\%)}}{C_{Cl}}$$

$$\log_{10} K_{H_2O} = \frac{12850}{T} - 2.8675$$

$$\log_{10} HCl = \frac{4894.6}{T} + 0.3436$$

Water

Moore (1998):

a = 2565; b_{Al₂O₃} = -1.997; b_{FeO_{tot}} = -0.9275; b_{Na₂O} = 2.736; c = 1.171; d = -14.21;

$$\ln f_{H_2O} = \frac{2 \log X_{H_2O} - \frac{a}{T} - \sum_i b_i X_{i,T}^P - d}{c}$$

P in bars, T in Kelvin, X_i on anhydrous basis.

Burnham (1994):

$$(a_w^m)_{P,T,X_w^m \leq 0.5} = k_w (X_w^m)^2$$

$$(a_w^m)_{P,T,X_w^m > 0.5} = 0.25 k_w \exp \left(\frac{6.52 - \frac{2667}{T}}{X_w^m - 0.5} \right)$$

$$\ln k_w = 5.00 + \ln P (4.481 \times 10^{-8} T^2 - 1.51 \times 10^{-4} T - 1.137) + (\ln P)^2 (1.831 \times 10^{-8} T^2 - 4.882 \times 10^{-5} T + 0.04656) + 7.8 \times 10^{-3} (\ln P)^3 - 5.012 \times 10^{-4} (\ln P)^4 + T (4.754 \times 10^{-3} - 1.621 \times 10^{-6} T)$$

P in bars, t in Kelvin, X on eight oxygen basis.

Sulphur

Sulphide and sulphate capacities (Gorojovsky and Wood 2025)

$$\log C_{S^{2-}} = 0.65 + (-3368X_{Si_{0.5}O} - 1233X_{Al_{0.6}O} + 1295X_{CaO} + 44885X_{K_2O} + 10914X_{FeO} \cdot X_{Si_{0.5}O} - 871864X_{FeO} \cdot X_{K_2O} - 225569X_{FeO} \cdot X_{Na_2O} + 54392X_{FeO} \cdot X_{Al_{0.5}O} - 7585) / T + 3.9 \operatorname{erf}[X_{FeO}]$$

$$\log C_{S^{6+}} = 196.0 + (-7633X_{Si_{0.5}O} - 10670X_{Ti_{0.5}O} - 6901X_{Al_{0.6}O} - 4625X_{FeO} + 19114X_{MnO} + 11740X_{CaO} + 33267X_{Na_2O} - 4095) / T - 57.3 \log(T)$$

Reaction constants (Bouillong and Wood 2021, 2023)

$$\log_{10} K_{SO_2} = \frac{18880}{T} - 3.8018$$

$$\log_{10} K_{H_2S} = \frac{27103}{T} - 4.1973$$

Effect of P (Thomas and Wood 2026)

$$\frac{\delta \log C_{S^{2-}}}{\delta P} = \frac{-0.056(\pm 0.008)}{T}$$

$$\frac{\delta \log C_{S^{6+}}}{\delta P} = \frac{-0.165(\pm 0.004)}{T}$$

T in Kelvin, P in bars, X_M on single oxygen basis.

Oxygen

FMQ base (Frost 1991)

$$\log fO_2 = \frac{-25096.3}{T} + 8.735 + 0.110 \frac{(P-1)}{T}$$

NNO base (Frost 1991)

$$\log fO_2 = \frac{-24930}{T} + 9.36 + 0.046 \frac{(P-1)}{T}$$

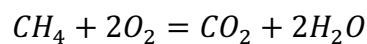
CCO base (Jakobsson and Oskarsson 1994)

$$\log fO_2 = \frac{-21803}{T} + 4.325 + 0.171 \frac{(P-1)}{T}$$

P in bars, T in Kelvin.

Carbon

CH4 equilibrium (Ohmoto and Kerrick 1977)



$$\log_{10} K_{CH_4} = \frac{41997}{T} + 0.719 \log_{10} T - 2.404$$

$$P_{trans} (kbar) = 0.025T + 12.592 \text{ (Day 2012)}$$

if $P_{kbar} < P_{trans}$

$$\log_{10} K1 = 40.07639 - 2.53932 \times 10^{-2}T + 5.27096 \times 10^{-6}T^2 + 0.0267 \frac{(P(kbar)-1)}{T}$$

(Holloway et al. 1992)

If $P_{kbar} \geq P_{trans}$:

$$\log_{10} K1 = 0.2450 - \frac{2.027 \times 10^4}{T} - \frac{4.730 \times 10^4}{T^2} + 0.0267 \frac{(1.949 \times 10^{-7} P(Pa) - 10^6)}{T} \quad (\text{Duncan and Dasgupta 2017})$$

$$\ln XCO_3^{2-} = -\frac{2.384 \times 10^{-5} P(Pa)}{RT} + \frac{-1.6448 \times 10^5}{RT} + \frac{1.4732 \times 10^3 \ln fCO_2}{T} + \frac{-43.6385}{R} + 3.291 NBO + \frac{(1.68 \times 10^5 XCaO + 1.7590 \times 10^5 XNa_2O + 2.1085 \times 10^5 XK_2O)}{RT}$$

Dissolved carbon (Eguchi and Dasgupta 2018)

$$\ln XCO_2 = -\frac{1.9244 \times 10^{-5} P(Pa)}{RT} + \frac{-9.0212 \times 10^4}{RT} + \frac{1.1149 \times 10^3 fCO_2}{T} + \frac{-43.0815}{R} - 7.0937 NBO$$

$$wt. \% CO_3^{2-} = \left[\frac{44.01 \times XCO_3^{2-}}{44.01 \times XCO_3^{2-} + (1 - (XCO_3^{2-} + XCO_2)) FWone} \right] \times 100$$

$$wt. \% CO_2 = \left[\frac{44.01 \times XCO_2}{44.01 \times XCO_2 + (1 - (XCO_3^{2-} + XCO_2)) FWone} \right] \times 100$$

FWone = one-oxygen formula weight of one mol of volatile free melt in g/mol

NBO = non bridging oxygens

If NBO > 0.5, wt. % CO₂ = 0

$$wt. \% CO_{2\text{tot}} = wt. \% CO_3^{2-} + wt. \% CO_2$$

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Attainment of equilibrium

Figure illustrating homogenous distribution of Cl in the experimental glass sample. The profile (red line) on the right panel corresponds with composition profile in the left panel (red line on the SE image). Sample DCB-2, Brothers volcano dacite, 1200 °C, 1.63 GPa, 2 hours.

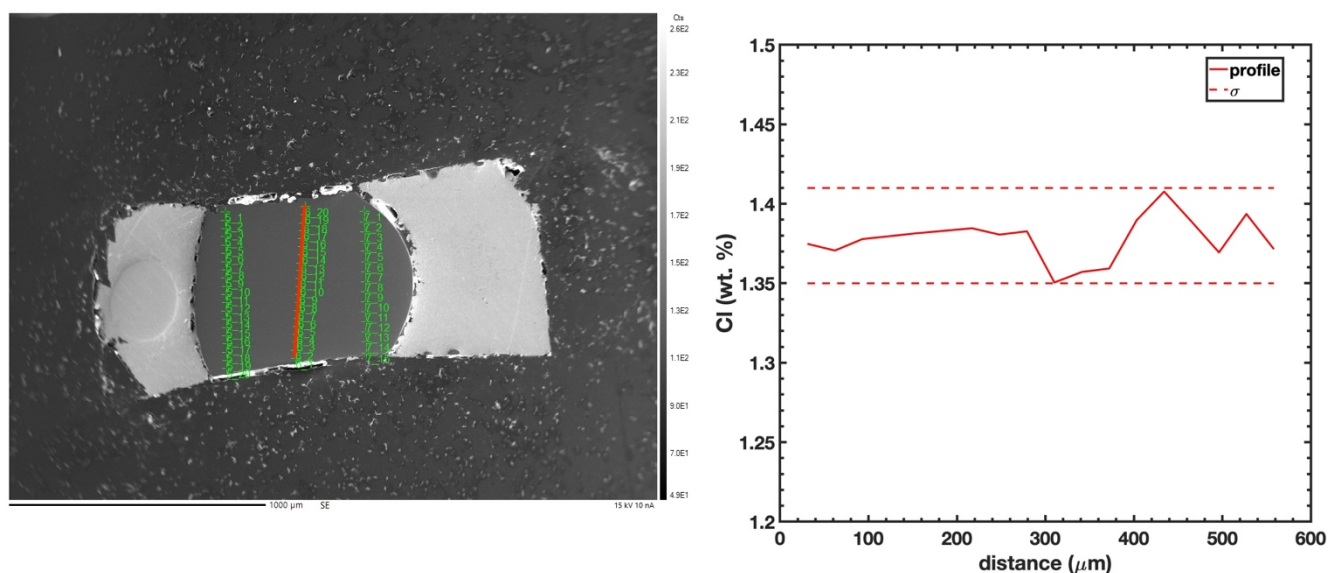


Table showing representative analyses of the AgI/Cl buffer

<i>Na</i>	<i>Mg</i>	<i>Si</i>	<i>Al</i>	<i>K</i>	<i>Ca</i>	<i>Fe</i>	<i>Cl</i>	<i>Ag</i>	<i>I</i>	<i>Pt</i>	<i>Total</i>
<i>-0.0106</i>	-0.565	0.0439	0.108	-0.071	-0.05	-0.005	4.411	62.17	37.03	-0.086	102.97
<i>0.032</i>	-0.527	0.007	0.124	-0.057	-0.07	-0.048	4.37	58.92	38.89	0.0856	101.73
<i>0.1325</i>	-0.503	0.0325	0.145	-0.076	-0.01	-0.008	3.613	56.6	41.27	0.1243	100.48
<i>0.2356</i>	-0.437	0.0223	0.08	-0.088	-0.05	0.063	3.479	57.89	41.89	0.1105	99.235
<i>0.2405</i>	-0.534	0.0367	0.091	-0.02	0	-0.01	3.536	57.26	41.79	0.2627	97.989