

Supporting Information

Comparative analysis of aromatic compounds steam reforming over Rh supported on γ -Al₂O₃

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S1.Catalyst characterisation

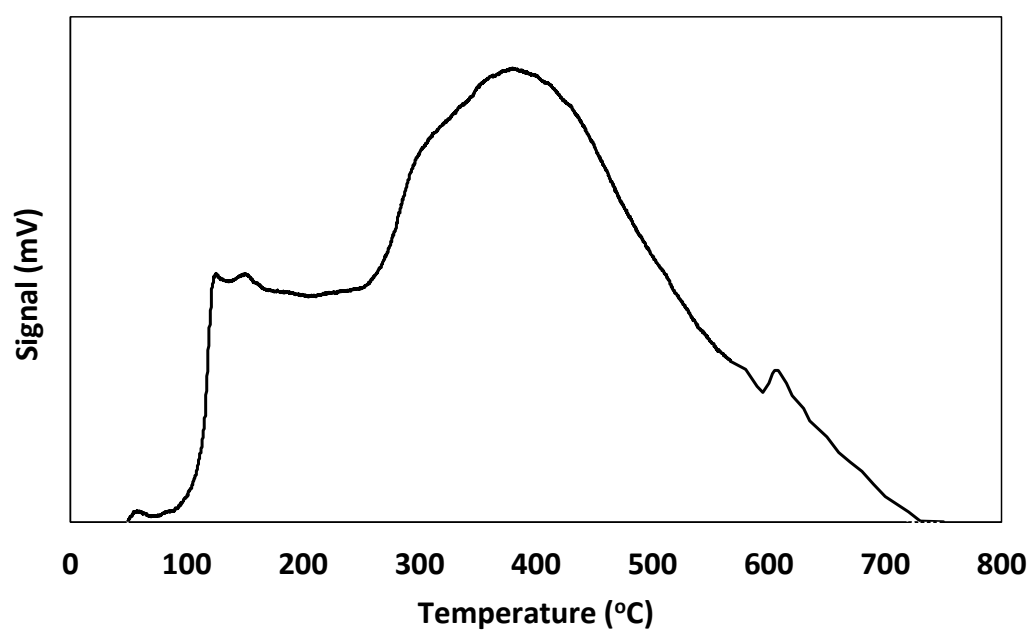


Figure S1. Temperature-programmed reduction (TPR) profile of calcined Rh/ γ -Al₂O₃ catalyst.

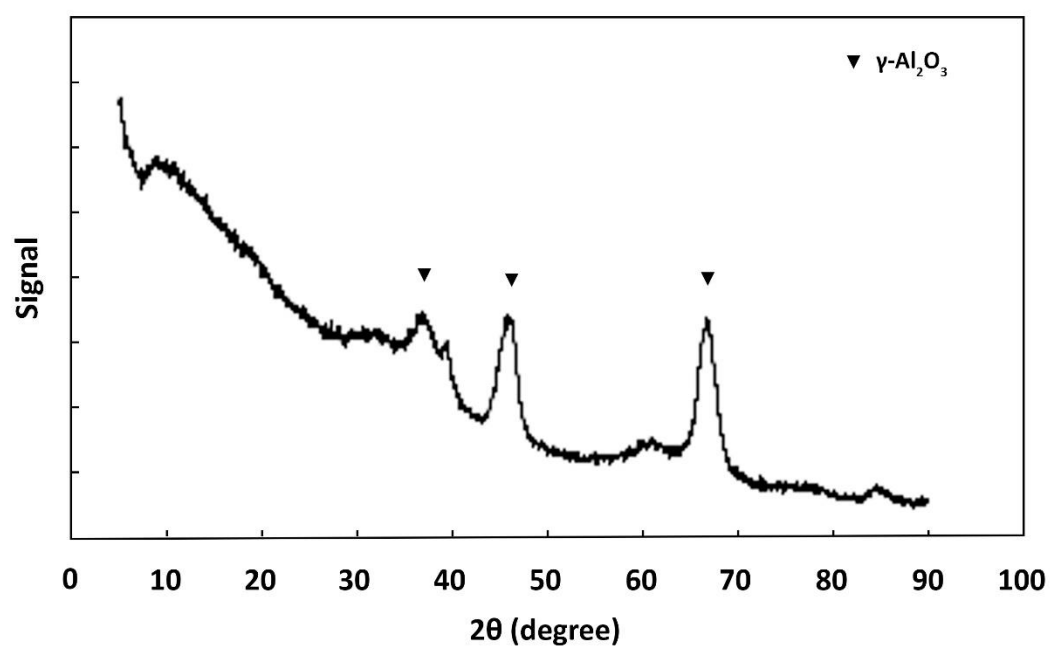


Figure S2. X-ray diffractogram of calcined Rh/ γ -Al₂O₃ catalyst.

S2.Thermodynamic analysis

The Aspen plus software was used for the thermodynamic analysis of the steam reforming reaction of the aromatic compounds, using the R-Gibbs reactor with the Peng-Robinson property method. The carbon selectivities are presented as a function of temperature ranging from 300 to 800 °C and S/C ratio ranging from 0.25 to 2 mol_{H₂O} mol_C⁻¹. Based on experimental results, the possible products considered in the simulations consisted of H₂, H₂O, CO, CO₂, CH₄, C₆H₆ (benzene), C₁₀H₈ (naphthalene), C₅H₆ (cyclopentadiene), the aromatics under study, namely C₆H₆O (phenol), C₆H₆O₂ (hydroquinone), C₇H₈O (benzyl alcohol) and C₇H₈ (toluene), and carbon (graphite).

The equilibrium calculations indicate the complete conversion of all model compounds under the examined conditions, forming H₂, CO, CO₂, CH₄ and solid C (graphite). The general trends of the carbon selectivities are similar for all the model compounds. Specifically, at lower temperature and S/C ratio solid carbon and methane are the main products. However, increasing the temperature and S/C ratio the solid carbon and methane formation reduce, with CO and CO₂ being the main products.

S2.1. Hydroquinone steam reforming

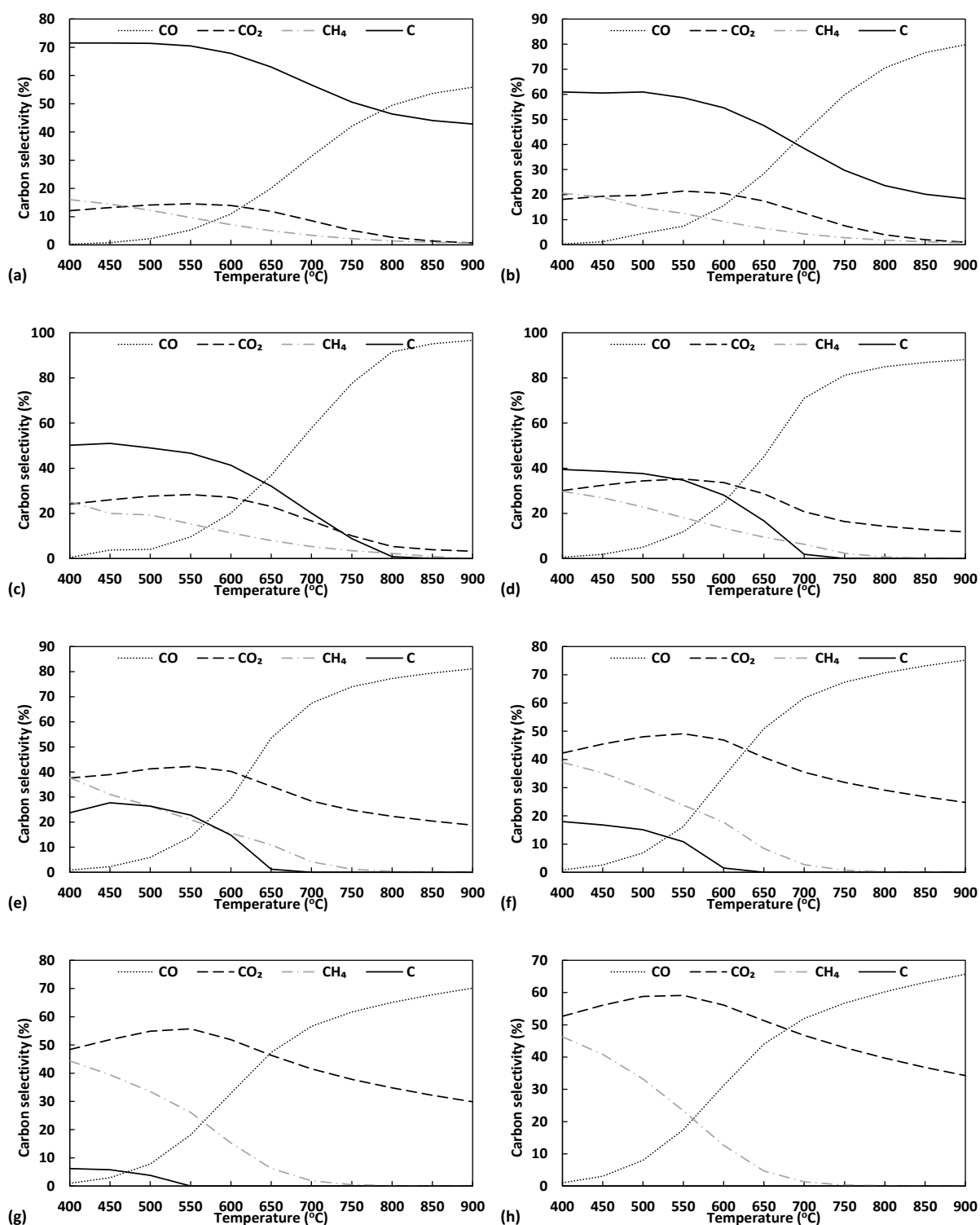


Figure S3. Temperature effect on the equilibrium product composition (CO, CO₂, CH₄ and C) during hydroquinone steam reforming at S/C = 0.25 (a), 0.5 (b), 0.75 (c), 1 (d), 1.25 (e), 1.5 (f), 1.75 (g) and 2 (h).

S2.2. Phenol steam reforming

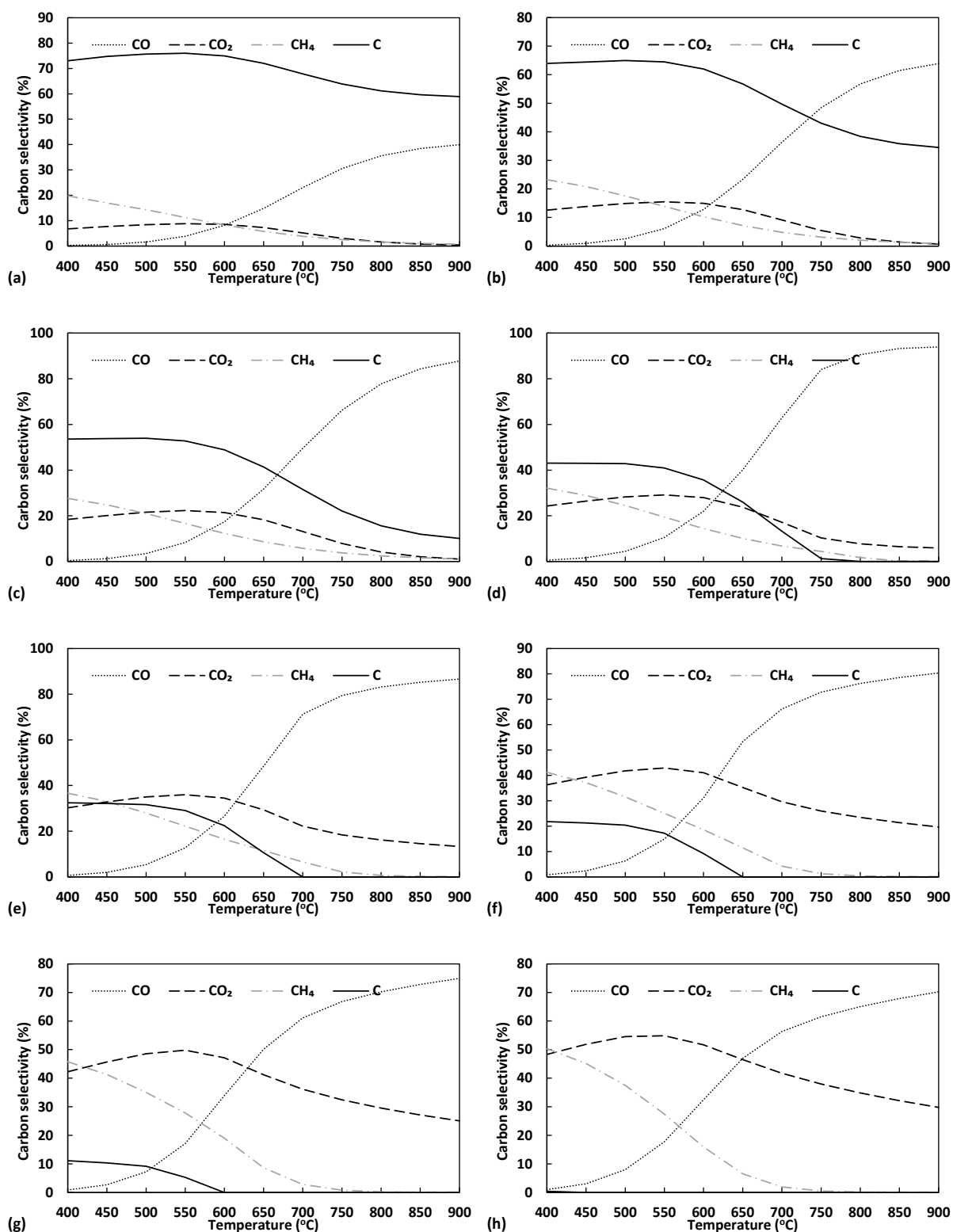


Figure S4. Temperature effect on the equilibrium product composition (CO, CO₂, CH₄ and C) during phenol steam reforming at S/C = 0.25 (a), 0.5 (b), 0.75 (c), 1 (d), 1.25 (e), 1.5 (f), 1.75 (g) and 2 (h).

S2.3. Benzyl alcohol steam reforming

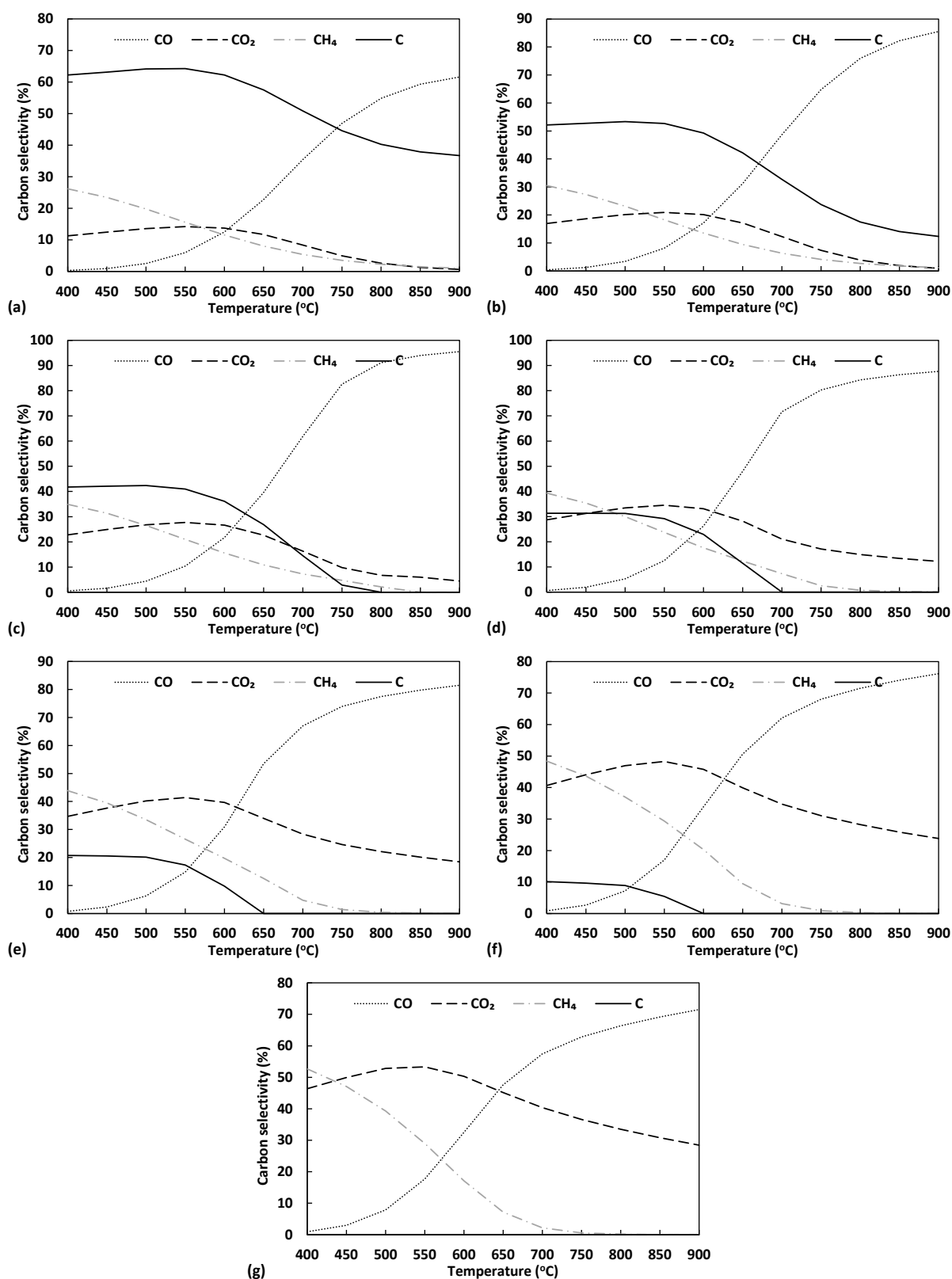


Figure S5. Temperature effect on the equilibrium product composition (CO, CO₂, CH₄ and C) during benzyl alcohol steam reforming at S/C = 0.5 (a), 0.75 (b), 1 (c), 1.25 (d), 1.5 (e), 1.75 (f) and 2 (g).

S2.4. Toluene steam reforming

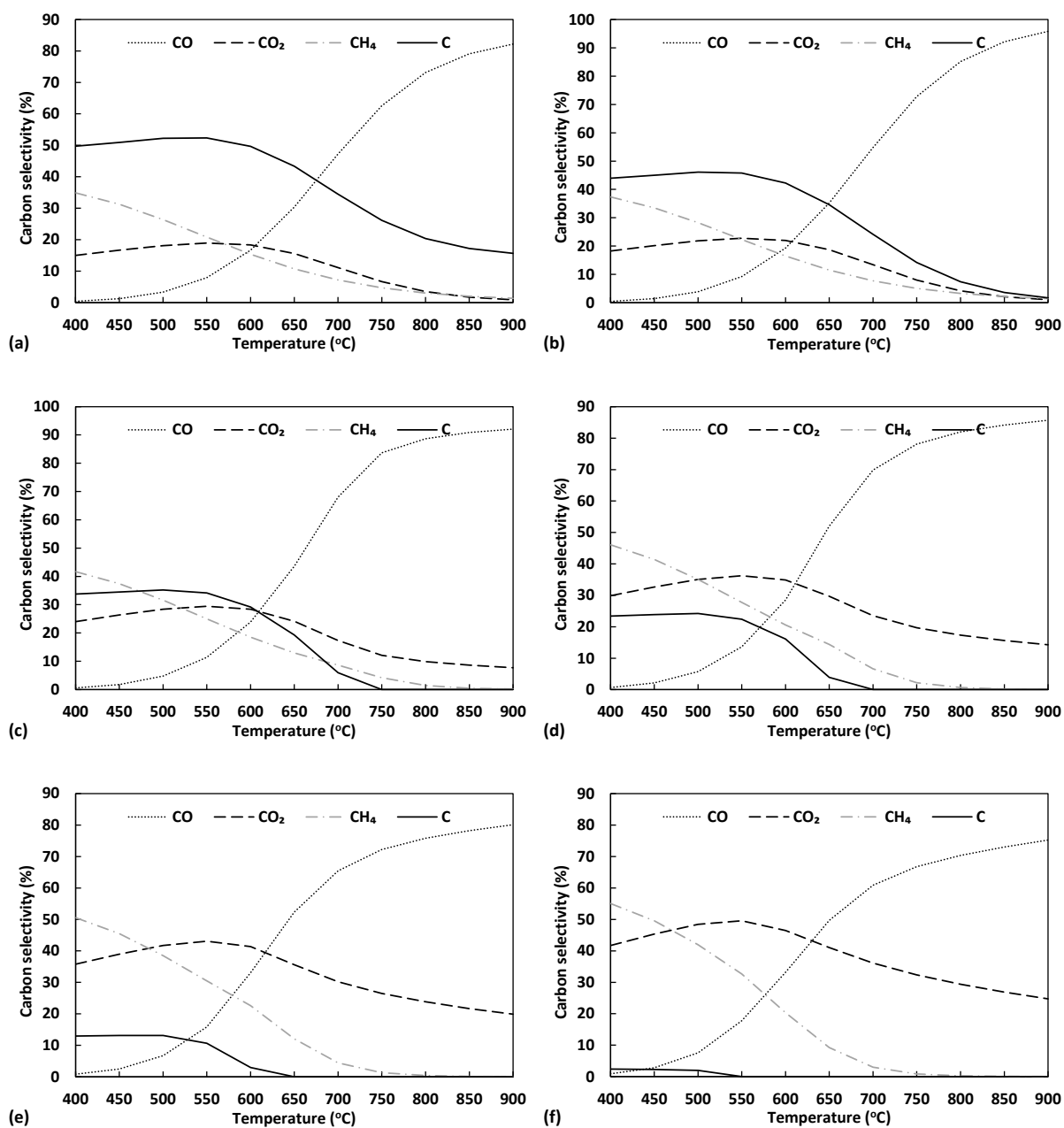


Figure S6. Temperature effect on the equilibrium product composition (CO, CO₂, CH₄ and C) during toluene steam reforming at S/C = 0.85 (a), 1 (b), 1.25 (c), 1.5 (d), 1.75 (e) and 2 (f).

S3.Product yields

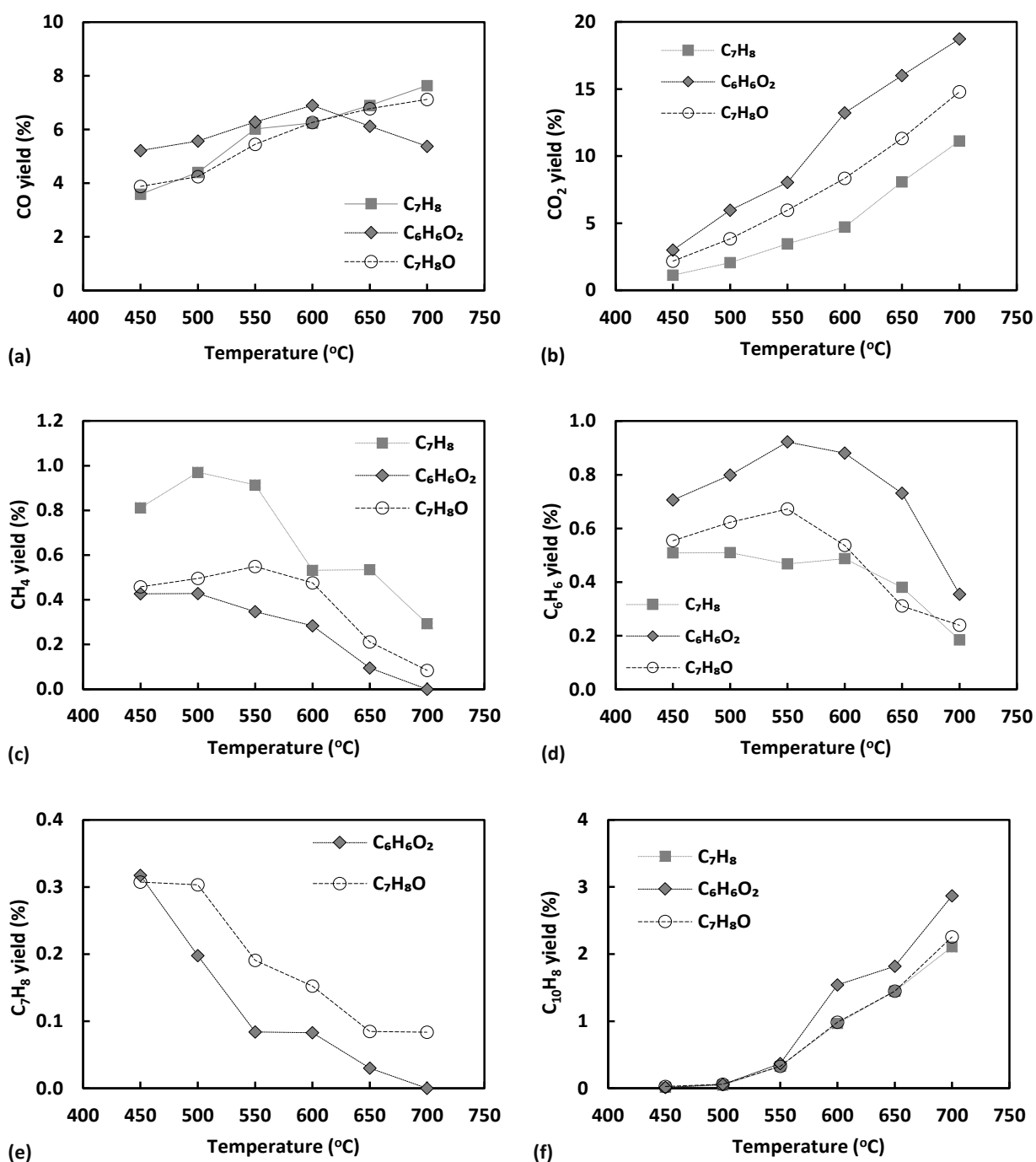


Figure S7. Temperature effect on yields of CO (a), CO₂ (b), CH₄ (c), C₆H₆ (d), C₇H₈ (e) and C₁₀H₈ (f) during the steam reforming of toluene, hydroquinone and benzyl alcohol ($W/F_{0, \text{Aromatics}} = 50 \text{ g}_{\text{cat}} \text{ s g}_{\text{Aromatics}}^{-1}$, $P = 1.9 \text{ bar}$, $S/C = 2$, aromatics ratio = $3 \text{ mol}_{\text{Compound}}/\text{mol}_{\text{Phenol}}$).

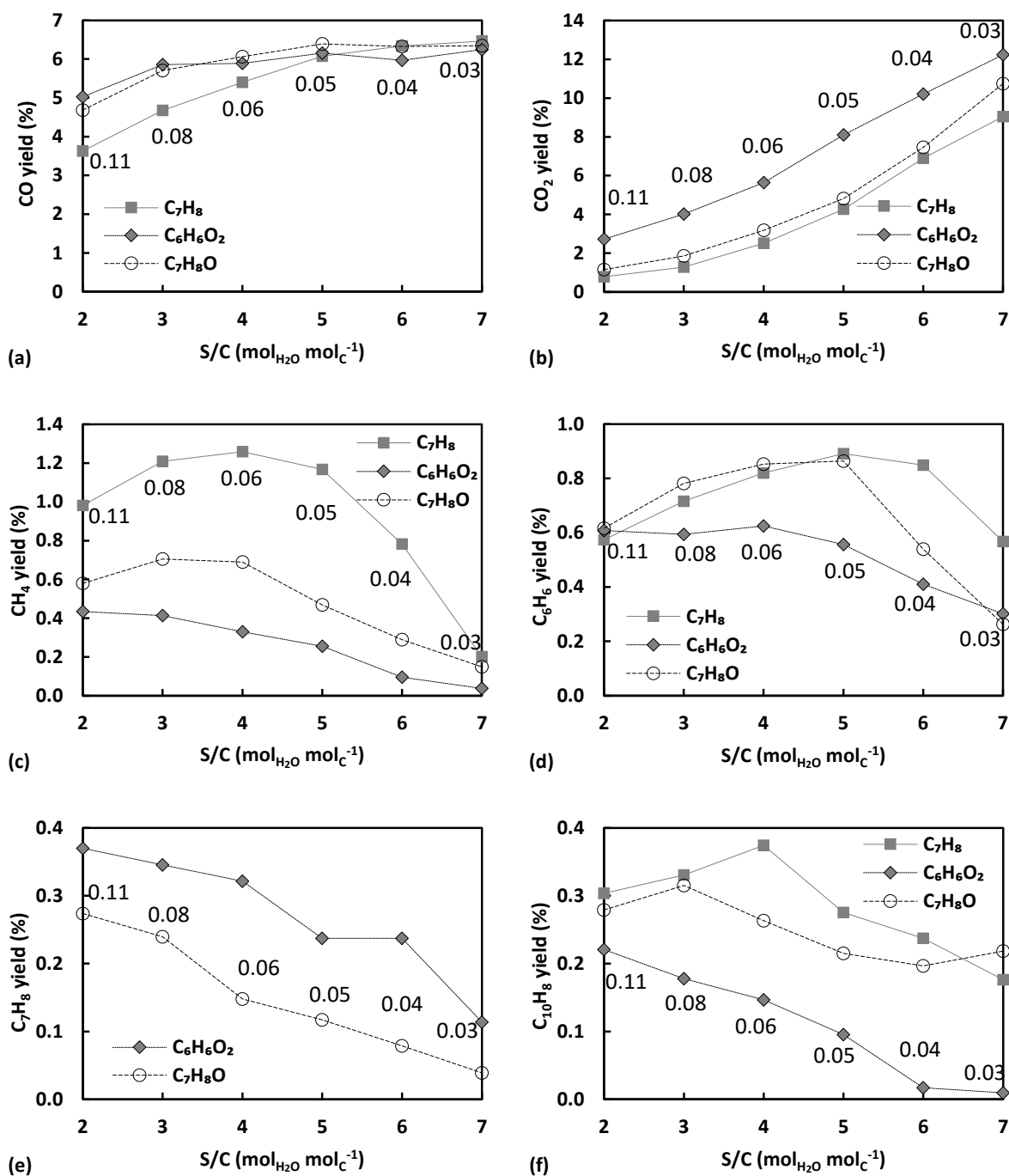


Figure S8. Partial pressure effect of aromatic compounds on yields of CO (a), CO₂, (b), CH₄ (c), C₆H₆ (d), C₇H₈ (e) and C₁₀H₈ (f) at 600°C presented as a S/C variation with numbers on plot annotating the equivalent partial pressures of phenol in bar ($P = 1.9$ bar, $Q_{\text{tot}} = 210$ NmL min⁻¹, aromatics ratio = 3 mol_{Compound}/mol_{Phenol}).

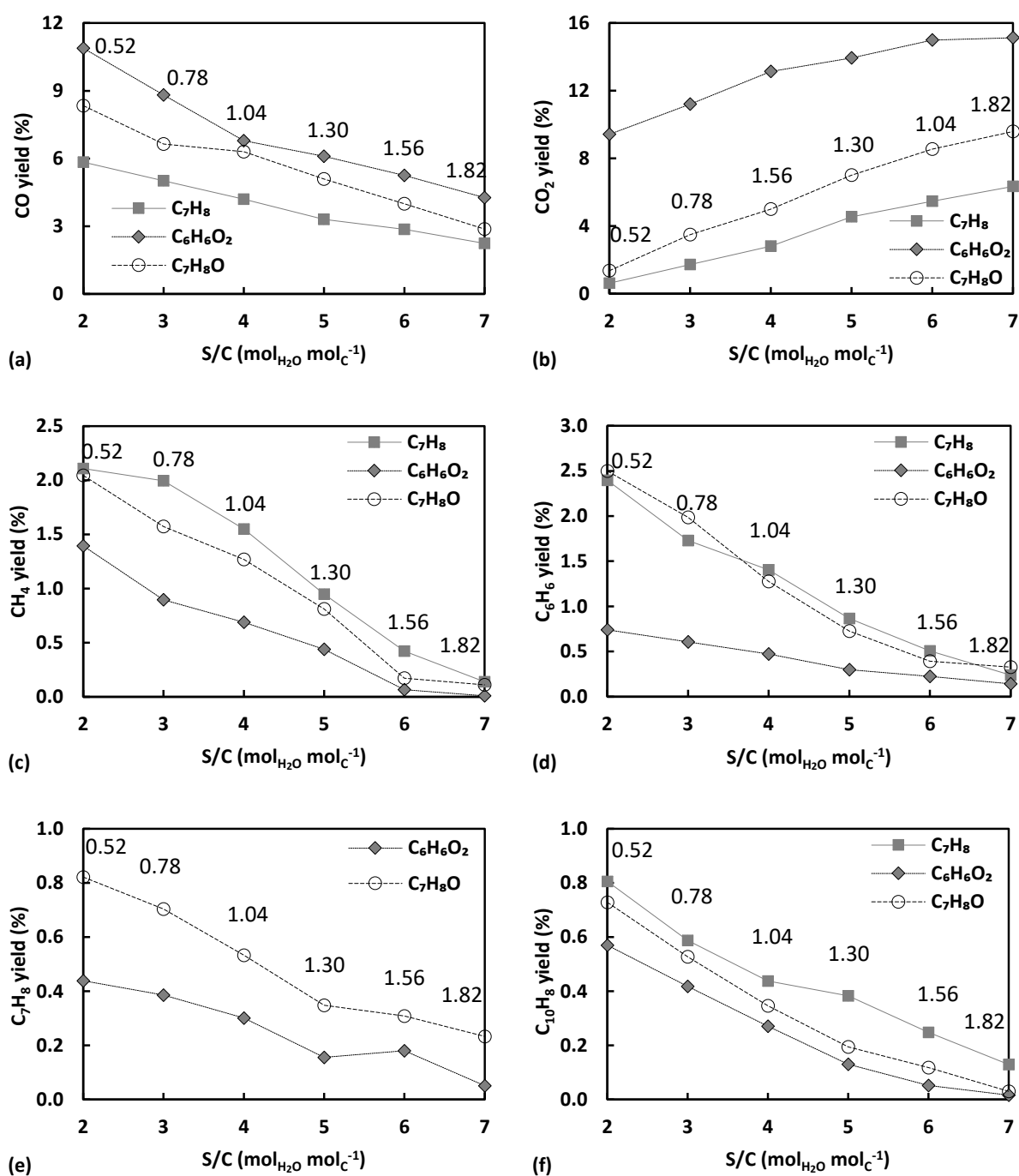


Figure S9. Partial pressure effect of water on yields of CO (a), CO₂, (b), CH₄ (c), C₆H₆ (d), C₇H₈ (e) and C₁₀H₈ (f) at 600 °C presented as a S/C variation with numbers on plot annotating the equivalent partial pressures of water in bar (P = 1.9 bar, Q_{tot} = 230 NmL min⁻¹, aromatics ratio = 3 mol_{Compound}/mol_{Phenol}).

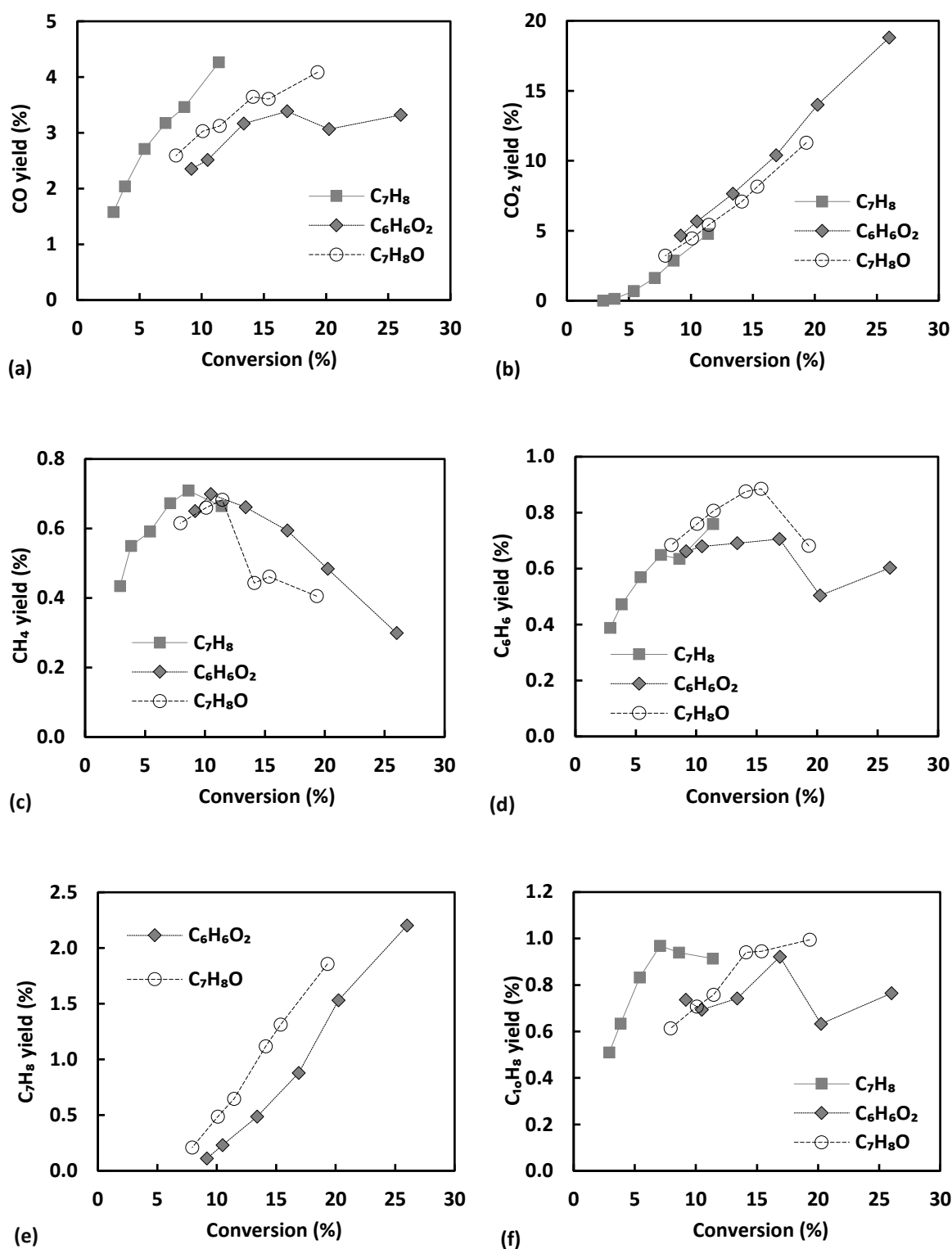


Figure S10. Yields of CO (a), CO₂, (b), CH₄ (c), C₆H₆ (d), C₇H₈ (e) and C₁₀H₈ (f) versus the total conversion observed during W/F₀ variation at 600 °C (P = 1.8 bar, S/C = 2, aromatics ratio = 3 mol_{Compound}/mol_{Phenol}).