

Capture of aqueous radioiodine species by metalated adsorbents and applications for the nuclear industry: a mini review

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Table S1. Comparison of properties of all metalated adsorbents discussed in the review for aqueous iodine adsorption.

Line	Adsorbent matrix	Loading metal	Synthesis	BET surface area (m ² g ⁻¹)	Metal loading achieved (mg g ⁻¹) (mmol g ⁻¹)	Iodine capacity (mg g ⁻¹) (mmol g ⁻¹)	Iodine species targeted	Iodine concentration in solution (mg L ⁻¹)	Adsorbent mass per L solution in static studies (g)	Relevant conditions/ co-contaminants	Determination of capacity	Time taken for adsorption equilibrium	Flowrate for dynamic experiments (mL hr ⁻¹)	Leaching test on iodine-loaded material	Notes	Reference
1	Activated carbon	Ag	Commercially available	1193	11 0.097	N/A	Iodide	0.6-6	10	Simulated Hanford low activity aqueous waste. ~8 M Na	N/A	<2 days	N/A	Water (~1 mg g ⁻¹ Ag leached) and 7.8 M NaOH (minimal leaching)	Distribution coefficient, rather than maximum uptake was measured (5.8 x 10 ⁶)	Asmussen <i>et al.</i> [1]
2	Activated carbon	Ag	Ag-doped form commercially available. Treated with HCl to produce AgCl-loaded form	802	8.7 0.081	13 0.10	Iodide	1.27 x 10 ⁻⁶ - 1.27	0.4	Contaminated ground water. High nitrate (>1000 mg L ⁻¹)	Estimated from isotherm (not modelled)	3 days	Not stated	Mild acid (pH 4.5) and base (pH 9) Ag leaching was <0.1% of total mass	10% of the loaded Ag bled from column experiments at pH 4.5	Karanfil <i>et al.</i> [2]
3	Activated carbon	Cu	Solvothermal: polyamine loaded with Cu(II) ions and heated in autoclave with activated carbon	N/A	170 2.7	41 0.32	Iodide	1-30	0.2-8	Chloride and sulfate (200 mg L ⁻¹). 10-15% reduction in performance	Isotherm (Langmuir model)	~60 min (90% within 20 min)	N/A	Mild acid (pH 5) and base (pH 9) up to 6% iodide leached		Zhang <i>et al.</i> [3]
4	TrisKem International CL resin / non-functionalised XAD-4 resin (3:4 ratio)	Ag	Immersion of resin in Ag ⁺ solution	N/A	7.5 0.070	25 0.20	Not defined	N/A (activity measurements were used)	N/A	1 M nitric acid (molybdate removed by alumina pre-column)	I-131 activity in column effluent	2.5 hr (~90% within 30 mins)	5400-11200	N/A	Functionality not disclosed but is selective for PGMS. Described as an "extraction chromatography" resin, so likely solvent-impregnated	Decamp and Happel [4]

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5	Bisipicolylamine ion-exchange resin	Cu	Contact with CuCl ₂ solution	N/A	80 1.3	300-450 2.4-3.5	iodide and iodine	50-2000	2	pH 0-13, 10:1 molar ratios of nitrate and molybdate (55% reduction in performance)	Isotherm (Langmuir / Dubinin-Radushkevich model)	N/A	5.5	N/A	Cu ²⁺ was reduced to Cu ⁺ in-situ, causing formation of I ₃ ⁻	Robshaw <i>et al.</i> [5]
6	Synthetic zeolite derived from coal fly ash	Ag	Activation with NaOH, then contact with aqueous Ag ⁺ to cause cation-exchange, then reduction to Ag(0) claimed	34-51	20 0.19	20 0.16	iodide	75-450	5	Chloride, carbonate, bromide and chromate (300 mg L ⁻¹). Negligible reduction in performance	Estimated from isotherm (not modelled)	>10 days	N/A	HCl (pH 2.5) and water. 1.4% iodine leached	The adsorbent had to be kept in the dark prior to use, to prevent oxidation of Ag nanoparticles.	Tauanov and Inglezakis, [6]
7	Zeolite	Ag	Commercially available	310	350 3.2	N/A	iodide	0.6-6	10	Simulated Hanford low activity aqueous waste. ~8 M Na	-	<1 day	N/A	Water (~40 mg g ⁻¹ Ag leached) and 7.8 M NaOH (~20 mg g ⁻¹ Ag leached)	Distribution coefficient, rather than maximum uptake was measured (4.1 x 10 ⁵)	Asmussen <i>et al.</i> [1]
8	Titanate	Ag	Reaction of Ti salt with NaOH in autoclave, then contact with aqueous Ag ⁺ , causing exchange of Na ⁺ , then Ag ₂ O precipitation	157	410 3.8	430 3.4	iodide	100-1100	1	Chloride only (100:1 molar ratio contaminant:iodide). No effect on performance	Estimated from isotherm (not modelled)	1 hr (adsorption is much faster in high chloride concentrations)	24-72	0.1 M NaCl. Minimal leaching		Bo <i>et al.</i> [7]
9	Titanate	Ag	Treatment of TiO ₂ with AgNO ₃ under UV light. Exchange of Na ⁺ , then Ag ₂ O precipitation	154	60 0.56	210 1.7	iodide	≤1400 (estimated from isotherm)	1	Very high chloride only (130 g L ⁻¹ , causing 10% decrease in iodide uptake)	Isotherm (Langmuir model)	6 hr	N/A	N/A	Used visible light for photocatalytic reduction of Ag(0) to Ag ⁺ , activating the adsorbent for iodide capture. Adsorbed species was a silver polyiodide complex (desorbed at 350°C)	Liu <i>et al.</i> [8]
10	Silica aerogel	Ag	Aerogel functionalised with mercapto-silanes, contacted with Ag ⁺ , reduced to Ag(0) with H ₂	85	360 3.3	88 0.69 (iodide)	iodide and iodate	5.6-7 (iodide only)	10	Simulated Hanford site waste (off-gas condensate simulant). 4580 mg L ⁻¹ nitrate, 1450 mg L ⁻¹ fluoride and 2340 mg L ⁻¹ sulfate	single batch experiment at extremely high [I ⁻] (17 g L ⁻¹)	1 hr in deionised water. ~2 days in simulated off-gas condensate	N/A	N/A	Iodate removal mechanism was by reduction to iodide (forming AgI)	Asmussen <i>et al.</i> [9]
11	Argentite	Ag	Precipitation from addition of AgNO ₃ to Na ₂ S	1.1	900 8.3	N/A	iodide	0.6-6	10	Simulated Hanford low activity aqueous waste. ~8 M Na	-	~15 days	N/A	Water (~2 mg g ⁻¹ Ag leached) and 7.8 M NaOH (minimal leaching)	Distribution coefficient, rather than maximum uptake was measured (2.5 x 10 ⁵)	Asmussen <i>et al.</i> [1]

Line	Adsorbent matrix	Loading metal	Synthesis	BET surface area (m ² g ⁻¹)	Metal loading achieved (mg g ⁻¹) (mmol g ⁻¹)	Iodine capacity (mg g ⁻¹) (mmol g ⁻¹)	Iodine species targeted	Iodine concentration in solution (mg L ⁻¹)	Mass of adsorbent used per L solution in static studies (g)	Relevant conditions/ co-contaminants	Determination of capacity	Time taken for adsorption equilibrium	Flowrate for dynamic experiments (mL hr ⁻¹)	Leaching test on iodine-loaded material	Notes	Reference
12	Mg(OH) ₂	Ag	Mixing of MgO and AgNO ₃ in water	78	350 3.2	370 2.9	iodide	0.5-800 (estimated from isotherm)	1	Chloride, sulfate, nitrate and carbonate (100:1 molar ratio contaminant:iodide). Minimal reduction in performance	Estimated from isotherm (not modelled)	<20 min	N/A	Mild acid (pH 3) and water. Minimal leaching		Chen <i>et al.</i> [10]
13	Cu ₂ O	Ag	Reduction of CuSO ₄ , with incorporation Ag(0) sol	N/A	10 0.093 (Ag only)	26 0.20	iodide	2.5-25	1	Chloride, sulfate, nitrate and carbonate (10:1 molar ratio contaminant:iodide). Carbonate caused 20% reduction in performance	Estimated from isotherm	1 hr	N/A	N/A	Superior performance in the absence of visible light, due to photocatalytic activity	Mao <i>et al.</i> [11]
14	Bismuth oxide powder	Bi	Solvothermal: Bi(NO ₃) ₃ dissolved in ethylene glycol/ethanol and heated in autoclave	N/A	920 4.4	290 2.2 (iodide) 230 1.3 (iodate)	iodide and iodate	0.5-700	0.2	Synthetic seawater and individual competing anions (20 g L ⁻¹). Chloride and carbonate caused large reduction (75%) in performance	Isotherm (Langmuir model)	~90 min (90% within 20 min)	N/A	Water. 2.3% loaded iodide leached		Liu <i>et al.</i> [12]
15	Mineral (copper carbonates malachite and azurite)	Cu	Mixing with powdered Cu(0)	0.18-0.33	Not calculated	Not calculated	iodide only	1270-12700	93	Deionised water only	N/A	~4 days	N/A	N/A		Lefevre <i>et al.</i> [13]
16	Cu ₂ O	Cu	hydrothermal reduction of Cu(NO ₃) ₂ by formic acid in water/ethanol with ammonia	N/A	800 13	23 0.18	iodide only	2.5-38	1	pH 3-10 (ineffective at higher pH). 100:1 molar ratios of chloride (~30% performance reduction), carbonate (~60% reduction), sulfate and nitrate (minimal reduction)	Isotherm (Langmuir model)	~ 6hr	N/A	N/A		Mao <i>et al.</i> [14]
17	Mineral (BiPbO ₂ (NO ₃))	Pb/Bi	Solid-state heating of Pb and Bi salts	N/A	Not calculated	Not calculated	iodide	150	200	pH 14, carbonate, nitrite and nitrate with total concentration ~400 g L ⁻¹ (caustic scrubbing solution simulation)	N/A	10 hr	N/A	N/A		Kodama [15]

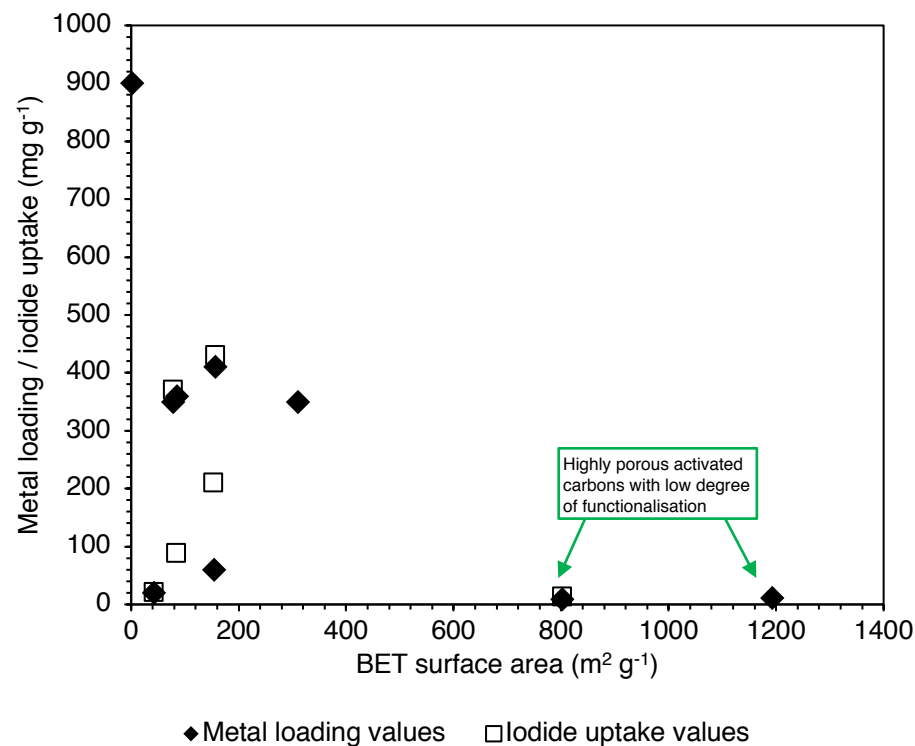


Figure S1. Relationships between measured BET surface areas of adsorbents with extent of metal-loading and iodide uptake capacity.

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