

Supplementary Information

Integrating hydrogen utilization in CO₂ electrolysis with reduced energy loss

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1. Supplementary Tables

Supplementary Table 1. The comparison of thermodynamic data between conventional and H₂-integrated CO₂RR at standard conditions.

reaction of conventional CO ₂ RR	$\Delta_r G$ (kJ mol ⁻¹)	E ₀ (V)	reaction of H ₂ -integrated CO ₂ RR	$\Delta_r G$ (kJ mol ⁻¹)	E ₀ (V)
CO ₂ + H ₂ O → HCOOH + 0.5O ₂	257.18	1.41	CO ₂ + H ₂ → HCOOH	34.95	0.18
CO ₂ → CO + 0.5O ₂	272.09	1.33	CO ₂ + H ₂ → CO + H ₂ O	20.04	0.10
CO ₂ + 2H ₂ O → CH ₄ + 2O ₂	818.12	1.06	CO ₂ + 4H ₂ → CH ₄ + 2H ₂ O	-130.45	-0.17
2CO ₂ + 2H ₂ O → C ₂ H ₄ + 3O ₂	1331.37	1.15	2CO ₂ + 6H ₂ → C ₂ H ₄ + 4H ₂ O	-91.48	-0.08

E₀ is the Nernst potential at standard conditions.

Supplementary Table 2. Mass loadings of Zn nanosheets on a 1×2 cm² Cu foam.

	M _{Cu foam} (mg)	M _{Cu foam + Zn} (mg)	M _{Zn} (mg)	Zn loading (mg cm ⁻²)
Zn-Cu-100	129.54	139.31	9.77	4.89
Zn-Cu-500	116.56	134.02	17.46	8.73
Zn-Cu-1000	122.68	149.39	26.71	13.36

Supplementary Table 3. Fitting results of the EIS plot in Figure 2h.

Potential (V vs. RHE)	$R_{ct}(\Omega)$	$R_w(\Omega)$	C(F)
1.40	0.24	2.90	0.81
1.50	0.21	0.90	0.75
1.65	0.15	0.50	0.75
1.80	0.24	-	0.70

Supplementary Table 4. Fitting results of the EIS plot in Figure 2i.

DoC (%)	$R_{ct}(\Omega)$	$R_w(\Omega)$	$C(F)$
0	0.20	0.70	0.75
30	0.22	1.20	0.77
60	0.19	1.40	0.77
100	4.19	-	0.70

Supplementary Table 5. Fitting results of the EIS plot in Figure 2j.

Reaction	$R_{ct}(\Omega)$	$R_w(\Omega)$	$C(F)$
NiOR	0.20	0.70	0.75
OER-NiOOH	4.19	-	0.70
OER-Co ₃ O ₄	2.45	-	0.84

Supplementary Table 6. Fitting results of the EIS plot in Supplementary Fig.15.

Potential (V vs. RHE)	$R_{ct}(\Omega)$	$R_w(\Omega)$	$C(F)$
1.25	0.20	1.18	0.68
1.15	0.23	1.90	0.87
1.05	0.25	4.30	0.90

Supplementary Table 7. The product FE, cell voltage, electrode potentials, and overpotentials (η) in combined CO₂RR+NiOR for CO production.

Current density (mA cm ⁻²)	H ₂ FE (%)	CO FE (%)	Cell voltage (V)	Potential _{cathode} (V vs. RHE)	η_{cathode} (mV)	Potential _{anode} (V vs. RHE)	η_{anode} (mV)
20	24.4	70.6	1.82	-0.40	300	1.39	40
50	22.7	71.3	2.15	-0.52	420	1.53	180
70	21.9	73.1	2.30	-0.59	490	1.58	230
100	19.9	75.6	2.47	-0.66	560	1.62	270
120	19.6	76.4	2.59	-0.70	600	1.66	310
150	17.7	81.9	2.72	-0.74	640	1.70	350
200	18.1	78.5	2.91	-0.79	690	1.74	390
250	20.2	76.5	3.10	-0.85	750	1.78	430

Supplementary Table 8. The product FE, cell voltage, electrode potentials, and overpotentials (η) in combined CO₂RR+OER for CO production.

Current density (mA cm ⁻²)	H ₂ FE (%)	CO FE (%)	Cell voltage (V)	Potential _{cathode} (V vs. RHE)	η_{cathode} (mV)	Potential _{anode} (V vs. RHE)	η_{anode} (mV)
20	28.6	65.5	2.01	-0.42	320	1.56	330
50	27.8	71.3	2.32	-0.52	420	1.70	470
70	27.2	72.5	2.50	-0.60	500	1.77	540
100	23.4	74.6	2.67	-0.66	560	1.82	590
120	22.7	76.4	2.76	-0.69	590	1.84	610
150	22.1	77.4	2.89	-0.73	630	1.87	640
200	19.3	76.4	3.06	-0.78	680	1.90	670
250	20.4	72.6	3.25	-0.84	740	1.94	710

Supplementary Table 9. The product FE, cell voltage, electrode potentials, and overpotentials (η) in combined CO₂RR+NiOR for formate production.

Current density (mA cm ⁻²)	H ₂ FE (%)	formate FE (%)	Cell voltage (V)	Potential _{cathode} (V vs. RHE)	η_{cathode} (mV)	Potential _{anode} (V vs. RHE)	η_{anode} (mV)
20	10.2	87.8	1.90	-0.46	280	1.39	40
50	5.1	93.8	2.17	-0.54	360	1.53	180
70	5.2	94.8	2.30	-0.60	420	1.58	230
100	5.6	94.3	2.47	-0.70	520	1.64	290
120	4.0	95.1	2.53	-0.73	550	1.67	320
150	4.2	95.3	2.61	-0.75	570	1.70	350
200	4.3	95.0	2.81	-0.77	590	1.74	390
250	12.0	84.2	3.01	-0.79	610	1.78	430

Supplementary Table 10. The product FE, cell voltage, electrode potentials, and overpotentials (η) in combined CO₂RR+OER for formate production.

Current density (mA cm ⁻²)	H ₂ FE (%)	formate FE (%)	Cell voltage (V)	Potential _{cathode} (V vs. RHE)	η_{cathode} (mV)	Potential _{anode} (V vs. RHE)	η_{anode} (mV)
20	10.0	87.8	2.10	-0.47	290	1.56	330
50	5.0	92.7	2.34	-0.54	360	1.70	470
70	5.0	93.3	2.50	-0.60	420	1.77	540
100	5.0	93.6	2.64	-0.70	520	1.82	590
120	5.0	94.0	2.72	-0.73	550	1.84	610
150	4.0	95.0	2.81	-0.75	570	1.87	640
200	4.0	93.7	3.01	-0.76	580	1.90	670
250	13.0	83.0	3.24	-0.80	620	1.94	710

Supplementary Table 11. Various polarization losses in H₂-integrated and conventional CO₂RR process at 50 mA cm⁻².

Overpotential (V)	H ₂ -integrated CO ₂ RR to CO	H ₂ -integrated CO ₂ RR to formate	Water electrolysis	Conventional CO ₂ RR to CO	Conventional CO ₂ RR to formate
Ohmic loss	0.11	0.11	-	0.1	0.1
η_{co2RR}	0.42	0.36	-	0.42	0.36
η_{AE1}	0.18	0.18	-	-	-
η_{AE2}	0.03	0.03	-	-	-
η_{OER}	-	-	-	0.47	0.47
η_{HOR}	0.03	0.03	-	-	-
η_{SOEC}	-	-	0.02	-	-
η_{AWE}	-	-	0.20	-	-

Supplementary Table 12. The cell voltage comparison of CO₂RR+HOR (Step 1+2), CO₂RR+NiOR (Step 1) with the state-of-the-art CO₂RR processes in the literature.

Method	Main product of CO ₂ RR	Current density	Cell voltage	Cell configuration	Reference
CO ₂ RR+HOR (Step 1+2)	CO	50 mA cm ⁻²	0.87 V	membrane-free flow cell	our work
CO ₂ RR+NiOR (Step 1)	CO	50 mA cm ⁻²	2.15 V	membrane-free flow cell	our work
CO ₂ RR+OER	CO	50 mA cm ⁻²	2.0 V	zero-gap flow cell	[1]
CO ₂ RR+OER	CO	50 mA cm ⁻²	2.17 V	zero-gap flow cell	[2]
CO ₂ RR+OER	CO	50 mA cm ⁻²	2.35 V	zero-gap flow cell	[3]
CO ₂ RR+OER	CO	50 mA cm ⁻²	2.50 V	zero-gap flow cell	[4]
CO ₂ RR+OER	CO	50 mA cm ⁻²	2.62 V	zero-gap flow cell	[5]
CO ₂ RR+OER	CO	50 mA cm ⁻²	4.27	flow cell	[1]
CO ₂ RR+GOR	CO	50 mA cm ⁻² (j _{co})	1.32 V	flow cell	[6]
CO ₂ RR+MOR	HCOO ⁻	50 mA cm ⁻²	1.52 V	H-cell	[7]
CO ₂ RR+GOR	CO	50 mA cm ⁻²	1.64 V	flow cell	[8]
CO ₂ RR+UOR	CO	50 mA cm ⁻²	2.25 V	flow cell	[9]
CO ₂ RR+GOR	HCOO ⁻	50 mA cm ⁻²	2.30 V	flow cell	[10]
CO ₂ RR+COR	CO	50 mA cm ⁻²	2.47 V	flow cell	[11]
CO ₂ RR+HMFOR	CO	50 mA cm ⁻²	2.64 V	H-cell	[12]
CO ₂ RR+COR	CO	50 mA cm ⁻²	3.55 V	H-cell	[13]
CO ₂ RR+MOR	HCOO ⁻	100 mA cm ⁻²	2.06 V	flow cell	[14]
CO ₂ RR+SOR	HCOO ⁻	20 mA cm ⁻²	2.0 V	H-cell	[15]
CO ₂ RR+octylamine electrooxidation	HCOO ⁻	20 mA cm ⁻²	2.20 V	H-cell	[16]
CO ₂ RR+EDTA-Fe ²⁺ oxidation	CO	14 mA cm ⁻²	2.50 V	H-cell	[17]

Notes: 1. UOR is urea oxidation reactions; HMFOR is 5-hydroxymethyl furfural oxidation reactions; COR is chlorine oxidation reaction; MOR is methanol oxidation reaction; GOR is glycerol oxidation reaction; SOR is sulfide oxidation reaction.

2. Voltage and current data are obtained from the polarization curves in papers where specific values are not offered.

Supplementary Table 13. The cell voltage and efficiency comparison of “H₂-electricity” conversion (Step 2) with the-state-of-art in the literature at 50 mA cm⁻².

Method	Cell voltage	Voltage efficiency	Reference
H ₂ -electricity conversion (Step 2)	1.28 V	95%	Our work
H ₂ fuel cell	0.90 V	73%	[18]
H ₂ fuel cell	0.90 V	73%	[19]
H ₂ fuel cell	0.89 V	72%	[20]
H ₂ fuel cell	0.88 V	72%	[21]
H ₂ fuel cell	0.87 V	71%	[22]
H ₂ fuel cell	0.82 V	67%	[23]
H ₂ fuel cell	0.80 V	65%	[24]
H ₂ fuel cell	0.77 V	63%	[25]
H ₂ fuel cell	0.72 V	59%	[26]

Note: Voltage and current data are obtained from the polarization curves in papers where specific values are not offered.

Supplementary Table 14. The comparison of energy consumption for CO production between H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR in 1 M KOH at different current densities.

	Current density (mA cm ⁻²)	20	50	70	100
H ₂ -integrated CO ₂ RR+SOEC	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.51	0.87	1.05	1.26
	CO FE (%)	70.6	71.3	73.1	75.6
	Electricity-CO ₂ RR (GJ per tonne CO)	5.0	8.4	9.9	11.5
	Cell voltage (V) -SOEC	0.930	0.940	0.945	0.951
	Electricity-water electrolysis (GJ per tonne CO)	9.1	9.1	8.9	8.7
	Energy consumption (GJ per tonne CO)	14.1	17.5	18.8	20.2
H ₂ -integrated CO ₂ RR+AWE	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.51	0.87	1.05	1.26
	CO FE (%)	70.6	71.3	73.1	75.6
	Electricity (GJ per tonne CO)	5.0	8.4	9.9	11.5
	Cell voltage (V) -AWE	1.39	1.43	1.46	1.48
	Electricity-water electrolysis (GJ per tonne CO)	13.6	13.8	13.8	13.5
	Energy consumption (GJ per tonne CO)	18.6	22.2	23.7	25.0
conventional CO ₂ RR	Cell voltage (V) -conventional CO ₂ RR	2.01	2.34	2.50	2.64
	CO FE (%)	65.5	71.3	72.5	74.6
	Energy consumption (GJ per tonne CO)	21.1	22.4	23.8	24.7

Supplementary Table 15. The comparison of energy consumption for formate production between H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR in 1 M KOH at different current densities.

	Current density (mA cm ⁻²)	20	50	70	100
H ₂ -integrated CO ₂ RR+SOEC	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.59	0.89	1.05	1.25
	Formate FE (%)	87.8	93.8	94.8	94.3
	Electricity-CO ₂ RR (GJ per tonne formate)	3.2	4.6	5.3	6.4
	Cell voltage (V) -SOEC	0.930	0.940	0.945	0.951
	Electricity-water electrolysis (GJ per tonne formate)	5.1	4.8	4.8	4.9
	Energy consumption (per tonne formate)	8.3	9.4	10.1	11.3
H ₂ -integrated CO ₂ RR+AWE	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.59	0.89	1.05	1.25
	Formate FE (%)	87.8	93.8	94.8	94.3
	Electricity (GJ per tonne formate)	3.2	4.6	5.3	6.4
	Cell voltage (V) -AWE	1.39	1.43	1.46	1.48
	Electricity-water electrolysis (GJ per tonne formate)	7.6	7.4	7.4	7.6
	Energy consumption (GJ per tonne formate)	10.8	12.0	12.7	14.0
conventional CO ₂ RR	Cell voltage (V) -conventional CO ₂ RR	2.10	2.34	2.50	2.64
	Formate FE (%)	87.8	92.7	93.3	93.6
	Energy consumption (GJ per tonne formate)	11.6	12.2	12.9	13.6

Supplementary Table 16. The comparison of energy consumption between H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR in 1 M KOH when water electrolyzer was operated at the industrially-relevant conditions.

	CO production		Formate production	
H ₂ -integrated CO ₂ RR+SOEC	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.87	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.89
	CO FE (%)	71.3	Formate FE (%)	93.8
	Electricity-CO ₂ RR (GJ per tonne CO)	8.4	Electricity-CO ₂ RR (GJ per tonne formate)	4.6
	Cell voltage (V) -SOEC	1.28	Cell voltage (V) -SOEC	1.28
	Electricity-water electrolysis (GJ per tonne CO)	12.4	Electricity-water electrolysis (GJ per tonne formate)	6.6
	Energy consumption (GJ per tonne CO)	20.8	Energy consumption (GJ per tonne formate)	11.2
H ₂ -integrated CO ₂ RR+AWE	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.87	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.89
	CO FE (%)	71.3	Formate FE (%)	93.8
	Electricity (GJ per tonne CO)	8.4	Electricity (GJ per tonne formate)	4.6
	Cell voltage (V) -AWE	1.47	Cell voltage (V) -AWE	1.47
	Electricity-water electrolysis (GJ per tonne CO)	14.2	Electricity-water electrolysis (GJ per tonne formate)	7.6
	Energy consumption (GJ per tonne CO)	22.6	Energy consumption (GJ per tonne formate)	12.2
conventional CO ₂ RR	Cell voltage (V) -conventional CO ₂ RR	2.34	Cell voltage (V) -conventional CO ₂ RR	2.34
	CO FE (%)	71.3	Formate FE (%)	92.7
	Energy consumption (GJ per tonne CO)	22.4	Energy consumption (GJ per tonne formate)	12.2

Supplementary Table 17. The comparison of energy consumption for CO production between H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR in 1 M KHCO₃ at different current densities.

	Current density (mA cm ⁻²)	20	50	70	100
H ₂ -integrated CO ₂ RR+SOEC	Cell voltage (V) H ₂ -integrated CO ₂ RR	0.93	1.21	1.38	1.59
	CO FE (%)	60.6	63.3	66.1	70.6
	Electricity-CO ₂ RR (GJ per tonne CO)	10.6	13.2	14.4	15.5
	Anode gas separation (GJ per tonne CO)	0	0	0	0
	Cell voltage (V) -SOEC	0.930	0.940	0.945	0.951
	Electricity-water electrolysis (GJ per tonne CO)	10.6	10.2	9.9	9.3
	Energy consumption (GJ per tonne CO)	21.2	23.4	24.3	24.8
H ₂ -integrated CO ₂ RR+AWE	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.93	1.21	1.38	1.59
	CO FE (%)	60.6	63.3	66.1	70.6
	Electricity (GJ per tonne CO)	10.6	13.2	14.4	15.5
	Anode gas separation (GJ per tonne CO)	0	0	0	0
	Cell voltage (V) -AWE	1.39	1.43	1.46	1.48
	Electricity-water electrolysis (GJ per tonne CO)	15.8	15.6	15.2	14.4
	Energy consumption (GJ per tonne CO)	26.4	28.8	29.6	29.9
conventional CO ₂ RR	Cell voltage (V) -conventional CO ₂ RR	2.46	2.66	2.84	3.01
	CO FE (%)	55.8	62.8	65.5	70.6
	Electricity (GJ per tonne CO)	30.4	29.2	29.9	29.4
	Anode gas separation (GJ per tonne CO)	11.3	10.0	9.6	8.9
	Energy consumption (GJ per tonne CO)	41.7	39.2	39.5	38.3

Note: At 100 mA cm⁻², the geometric area of mediator was 3×3 cm².

Supplementary Table 18. The comparison of energy consumption for formate production between H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR in 1 M KHCO₃ at different current densities.

	Current density (mA cm ⁻²)	20	50	70	100
H ₂ -integrated CO ₂ RR+SOEC	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.84	1.2	1.44	1.79
	Formate FE (%)	81.8	85.8	89.8	89.3
	Electricity-CO ₂ RR (GJ per tonne formate)	5.0	6.7	7.7	9.7
	Anode gas separation (GJ per tonne formate)	0	0	0	0
	Cell voltage (V) -SOEC	0.930	0.940	0.945	0.951
	Electricity-water electrolysis (GJ per tonne formate)	5.5	5.3	5.1	5.1
	Energy consumption (GJ per tonne formate)	10.5	12.0	12.8	14.8
H ₂ -integrated CO ₂ RR+AWE	Cell voltage (V) - H ₂ -integrated CO ₂ RR	0.84	1.2	1.44	1.79
	Formate FE (%)	81.8	85.8	89.8	89.3
	Electricity (GJ per tonne formate)	5.0	6.7	7.7	9.7
	Anode gas separation (GJ per tonne formate)	0	0	0	0
	Cell voltage (V) -AWE	1.39	1.43	1.46	1.48
	Electricity-water electrolysis (GJ per tonne formate)	8.2	8.0	7.8	8.0
	Energy consumption (GJ per tonne formate)	13.2	14.7	15.5	17.7
conventional CO ₂ RR	Cell voltage (V) -conventional CO ₂ RR	2.36	2.7	2.9	3.2
	Formate FE (%)	81.8	84.7	88.8	89.3
	Electricity (GJ per tonne formate)	13.9	15.4	15.8	17.3
	Anode gas separation (GJ per tonne formate O)	5.4	5.2	5.0	4.9
	Energy consumption (GJ per tonne formate)	19.3	20.6	20.8	22.2

Note: At 100 mA cm⁻², the geometric area of mediator was 3×3 cm².

Supplementary Table 19. The comparison of energy consumption between H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR in 1 M KHCO₃ when water electrolyzer was operated at the industrially-relevant conditions.

	CO production		Formate production	
H ₂ -integrated CO ₂ RR+SOEC	Cell voltage (V) - H ₂ -integrated CO ₂ RR	1.21	Cell voltage (V) - H ₂ -integrated CO ₂ RR	1.2
	CO FE (%)	63.3	Formate FE (%)	85.8
	Electricity-CO ₂ RR (GJ per tonne CO)	13.2	Electricity-CO ₂ RR (GJ per tonne formate)	6.7
	Anode gas separation (GJ per tonne CO)	0	Anode gas separation (GJ per tonne formate)	0
	Cell voltage (V) -SOEC	1.28	Cell voltage (V) -SOEC	1.28
	Electricity-water electrolysis (GJ per tonne CO)	13.9	Electricity-water electrolysis (GJ per tonne formate)	7.2
	Energy consumption (GJ per tonne CO)	27.1	Energy consumption (GJ per tonne formate)	13.9
H ₂ -integrated CO ₂ RR+AWE	Cell voltage (V) - H ₂ -integrated CO ₂ RR	1.21	Cell voltage (V) - H ₂ -integrated CO ₂ RR	1.2
	CO FE (%)	63.3	Formate FE (%)	85.8
	Electricity (GJ per tonne CO)	13.2	Electricity (GJ per tonne formate)	6.7
	Anode gas separation (GJ per tonne CO)	0	Anode gas separation (GJ per tonne formate)	0
	Cell voltage (V) -AWE	1.47	Cell voltage (V) -AWE	1.47
	Electricity-water electrolysis (GJ per tonne CO)	16.0	Electricity-water electrolysis (GJ per tonne formate)	8.3
	Energy consumption (GJ per tonne CO)	29.2	Energy consumption (GJ per tonne formate)	15.0
conventional CO ₂ RR	Cell voltage (V) -conventional CO ₂ RR	2.66	Cell voltage (V) -conventional CO ₂ RR	2.70
	CO FE (%)	62.8	Formate FE (%)	84.7
	Electricity (GJ per tonne CO)	29.2	Electricity (GJ per tonne formate)	15.4
	Anode gas separation (GJ per tonne CO)	10.0	Anode gas separation (GJ per tonne formate)	5.2
	Energy consumption (GJ per tonne CO)	39.2	Energy consumption (GJ per tonne formate)	20.6

Supplementary Table 20. The unit cost of component materials.

Component	Cost	Units	Source
Zn-Cu foam GDE	12.8	\$ m ⁻²	a
Co ₃ O ₄ electrode	9.8	\$ m ⁻²	a
Ni(OH) ₂ /NiOOH	14.0	\$ m ⁻²	a
Pt GDE	16.0	\$ m ⁻²	a
Separator	2.0	\$ m ⁻²	[27]
Nafion membrane	350	\$ m ⁻²	[28]
Cathode of SOEC (Ni+YSZ)	81.5	\$ m ⁻²	a
Anode of SOEC (LSM)	53.8	\$ m ⁻²	a

a. based on the chemicals/materials cost in Supplementary Table 21.

Supplementary Table 21. The cost of chemicals and materials.

Chemicals/materials	Cost	Units	Source
Carbon black	0.04	\$ kg ⁻¹	a
PTFE	10.3	\$ kg ⁻¹	b
Zn	8.0	\$ kg ⁻¹	c
Cu foam	2.4	\$ m ⁻²	c
Co	75.0	\$ kg ⁻¹	c
Ni foam	6.0	\$ m ⁻²	[29]
Ni	14.0	\$ kg ⁻¹	c
Pt	32035.0	\$ kg ⁻¹	c
NiO	14.0	\$ kg ⁻¹	c
ZrO ₂	45.8	\$ kg ⁻¹	d
La _{0.8} Sr _{0.2} MnO _{3-x}	7000.0	\$ kg ⁻¹	e
GDL	0.006	\$ m ⁻²	[30]

a. Taken from online report of “carbon black price trend and forecast” (<https://www.chemanalyst.com/>).

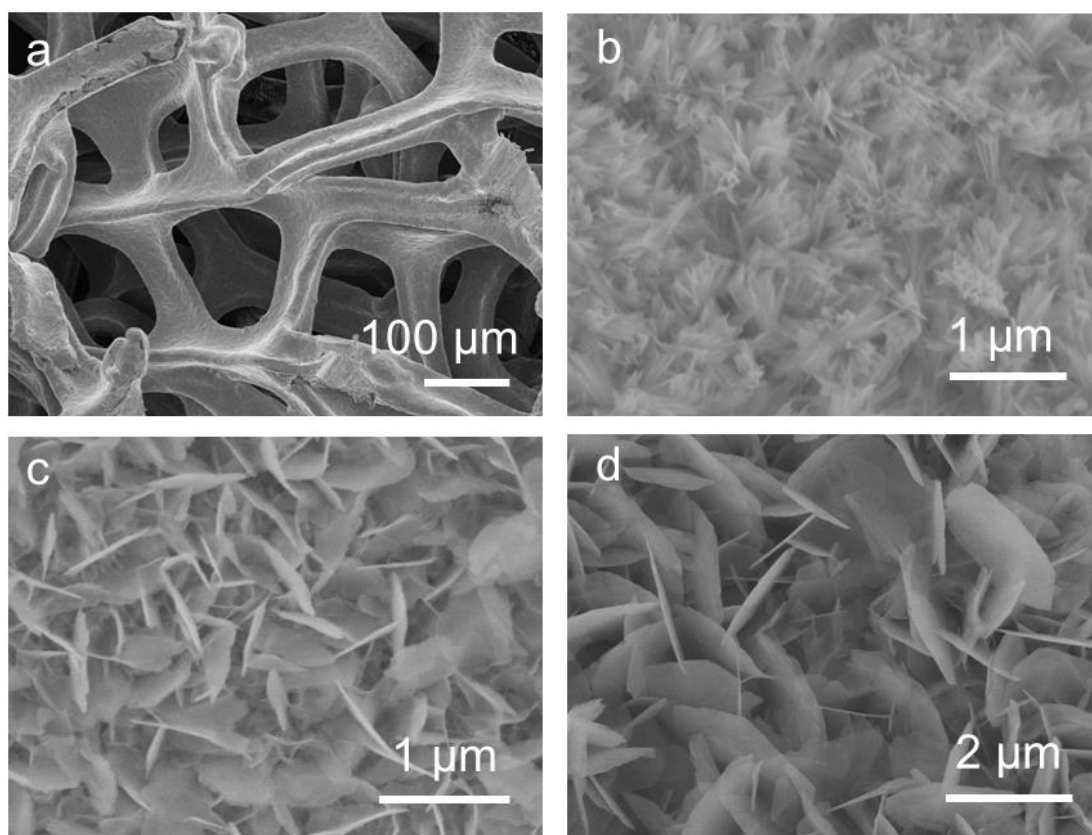
b. Taken from online report of “PTFE prices rising due to improvement in downstream market demand” (<https://www.chemanalyst.com/>).

c. Taken from the report of daily metal prices (<https://www.dailymetalprice.com/>).

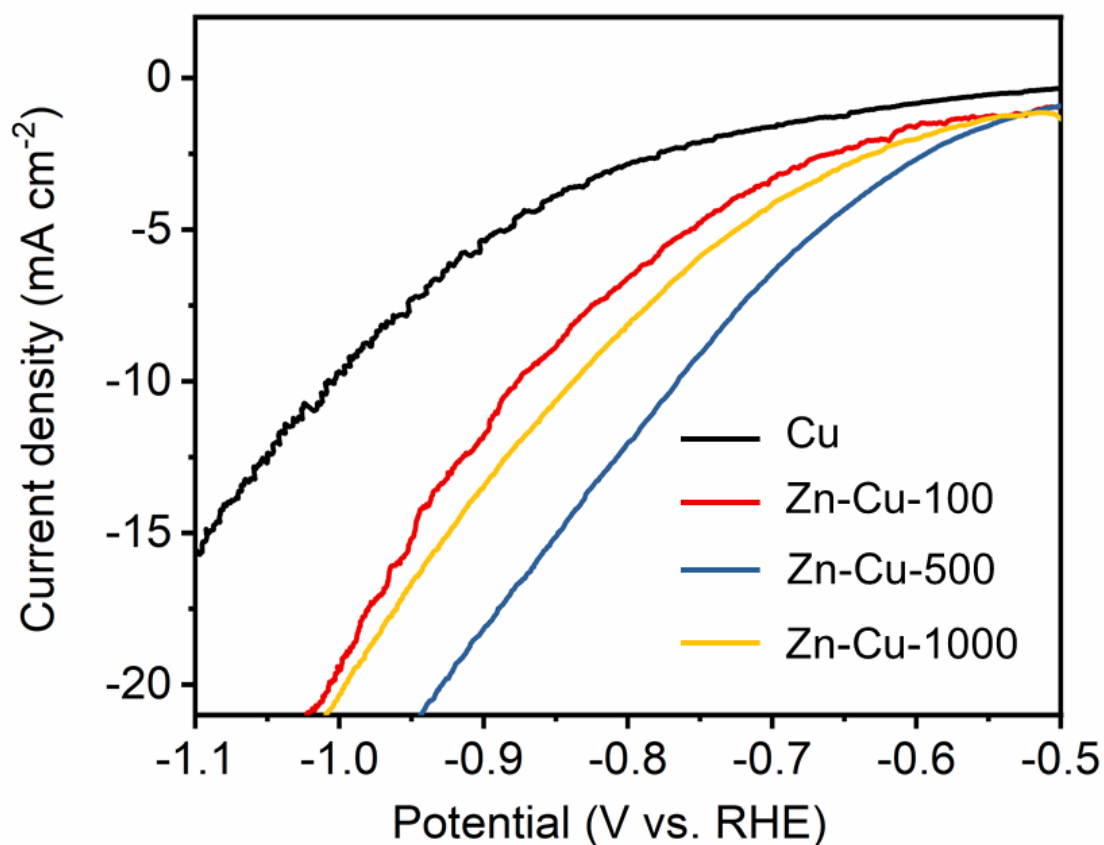
d. Taken from online trade market. (https://www.made-in-china.com/products-search/hot-china-products/ZrO2_Zirconia_Powder_Price.html)

e. Taken from online trade market. (<https://www.sigmaaldrich.cn/CN/zh/product/aldrich/704261>)

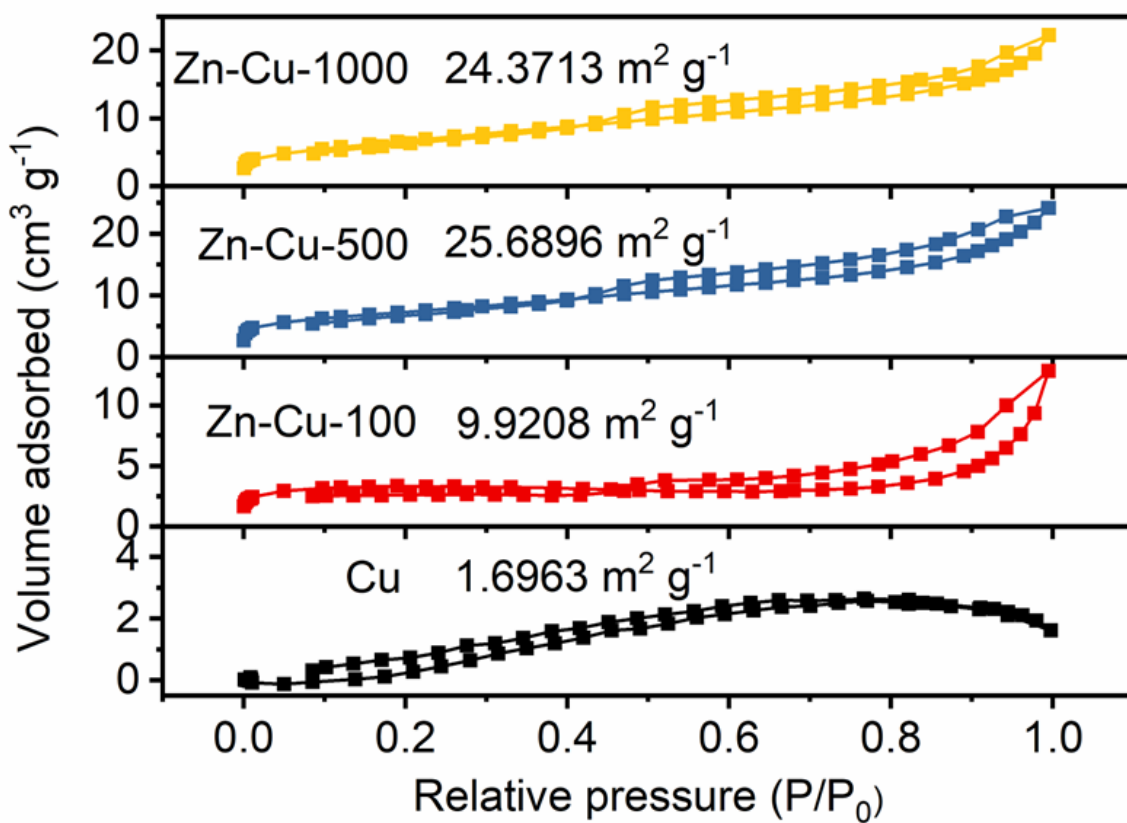
2. Supplementary Figures



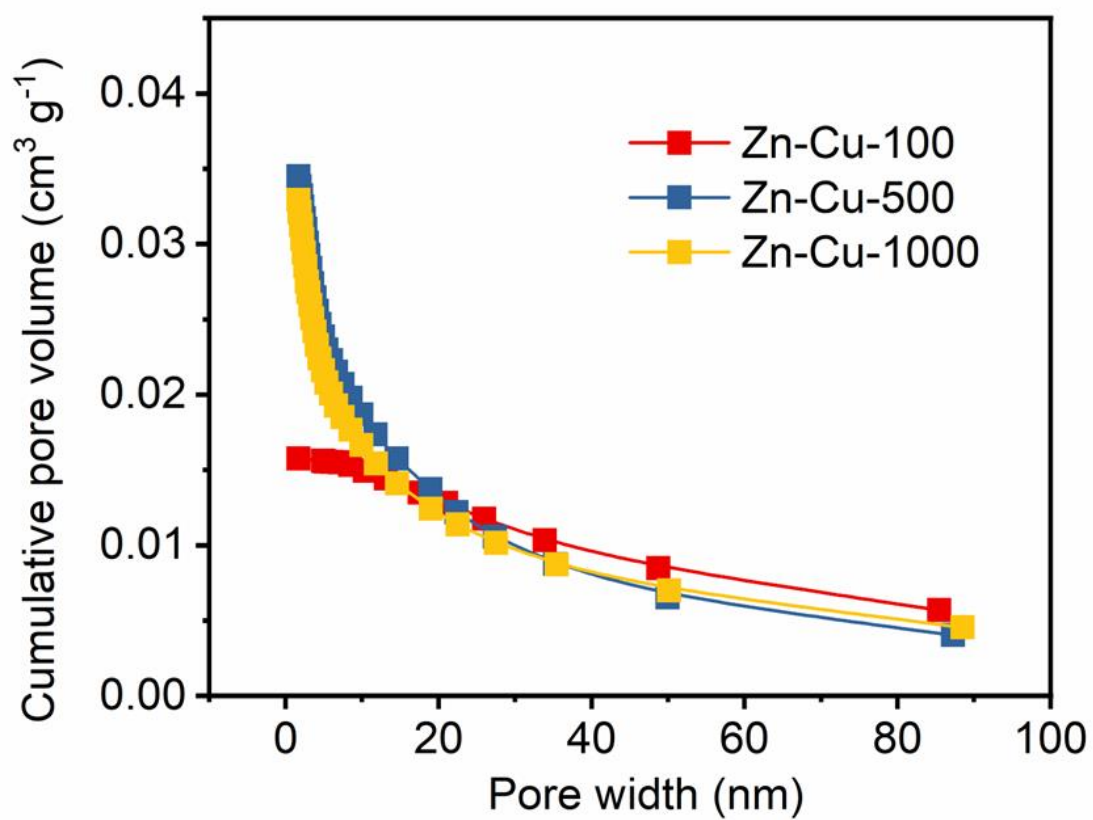
Supplementary Fig. 1. The surface morphology of Zn-Cu electrode. SEM images of (a) Cu foam, (b) Zn-Cu-100, (c) Zn-Cu-500, and (d) Zn-Cu-1000.



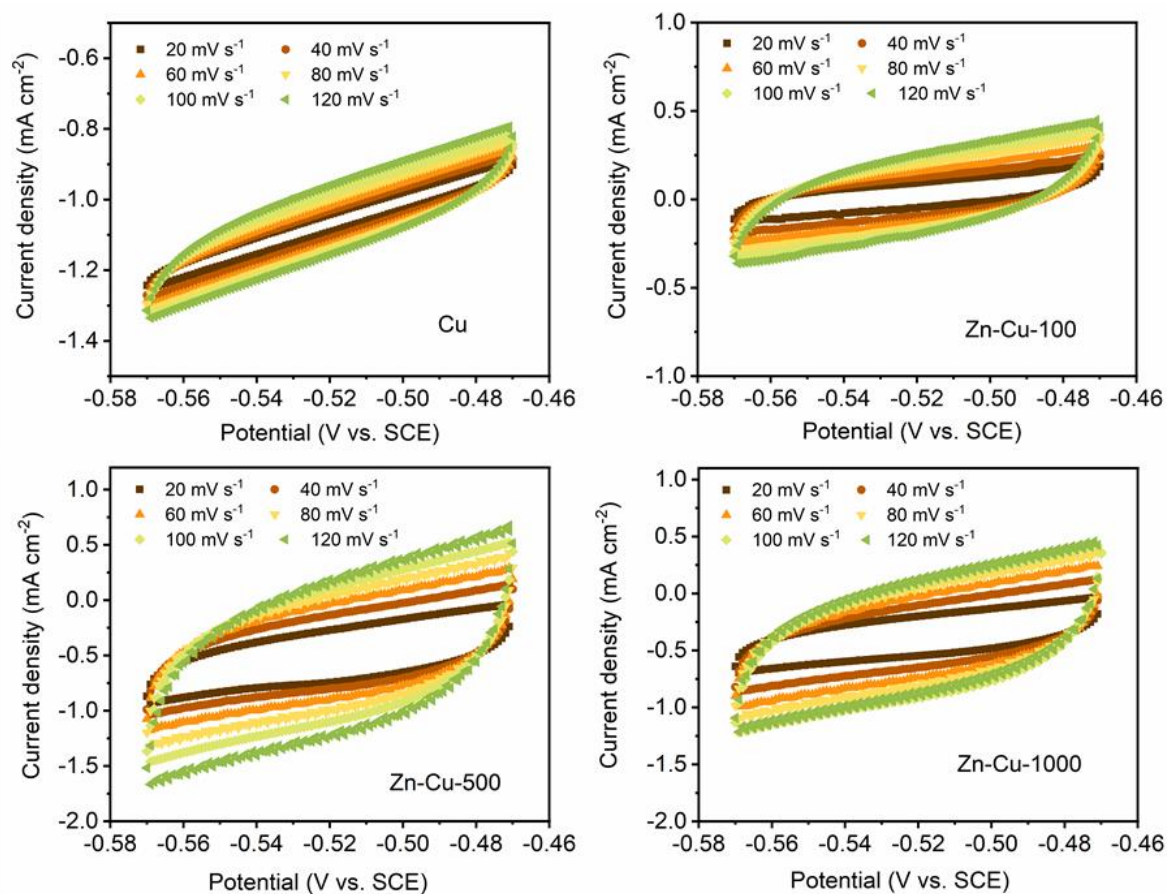
Supplementary Fig. 2. The electrochemical performance of Zn-Cu electrode. LSV curves of Cu, Zn-Cu-100, Zn-Cu-500, and Zn-Cu-1000 in CO_2 -saturated 0.1 M KHCO_3 electrolyte with a scan rate of 5 mV s^{-1} . The solution resistance of Cu, Zn-Cu-100, Zn-Cu-500, and Zn-Cu-1000 electrodes were 7.89, 8.18, 8.83, and 7.75 Ω , respectively.



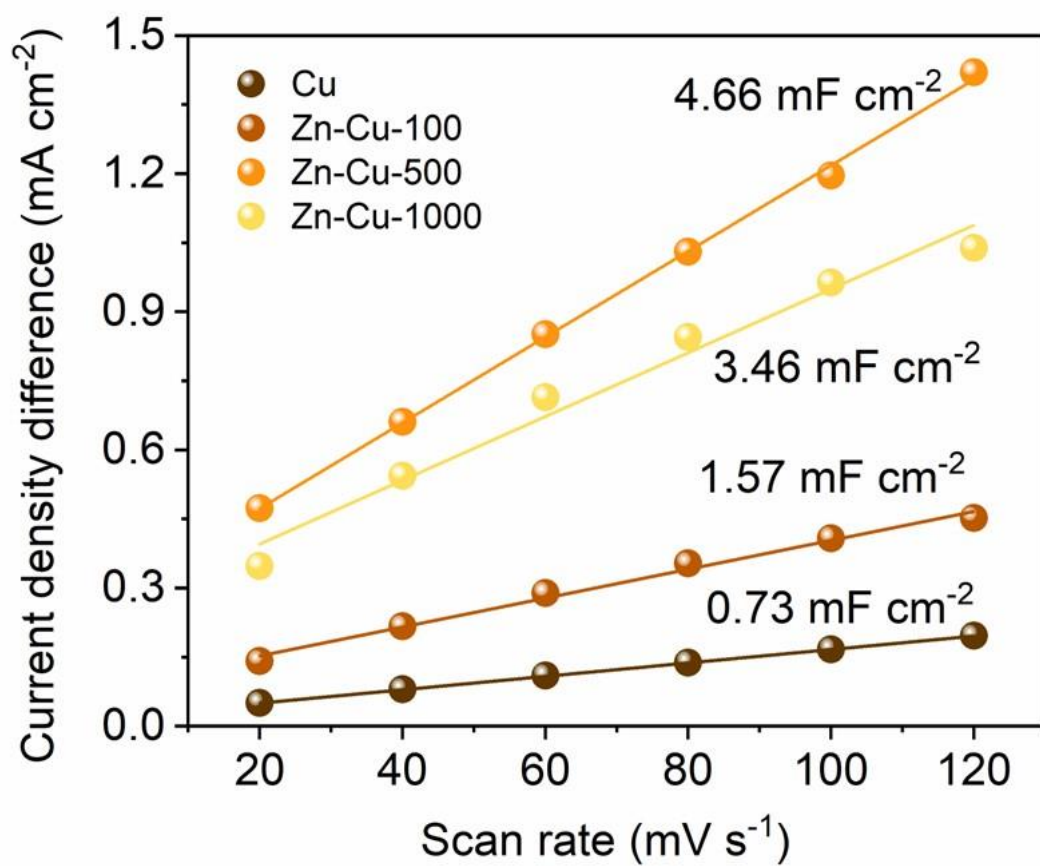
Supplementary Fig. 3. The specific surface area of Zn electrode. Nitrogen adsorption-desorption isotherms of Cu, Zn-Cu-100, Zn-Cu-500, and Zn-Cu-1000.



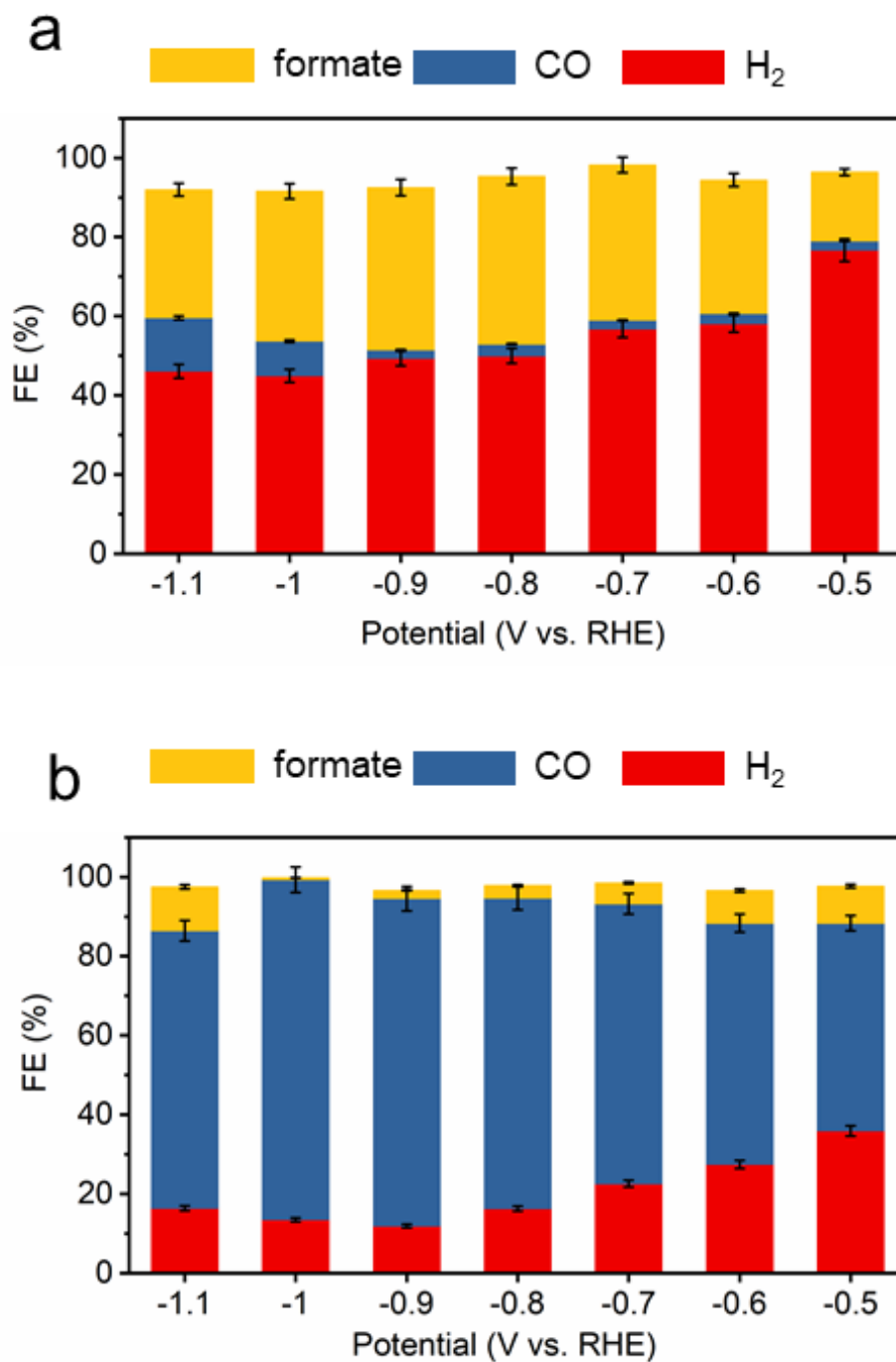
Supplementary Fig. 4. Cumulative pore volume distributions of Zn-Cu-100, Zn-Cu-500, and Zn-Cu-1000.



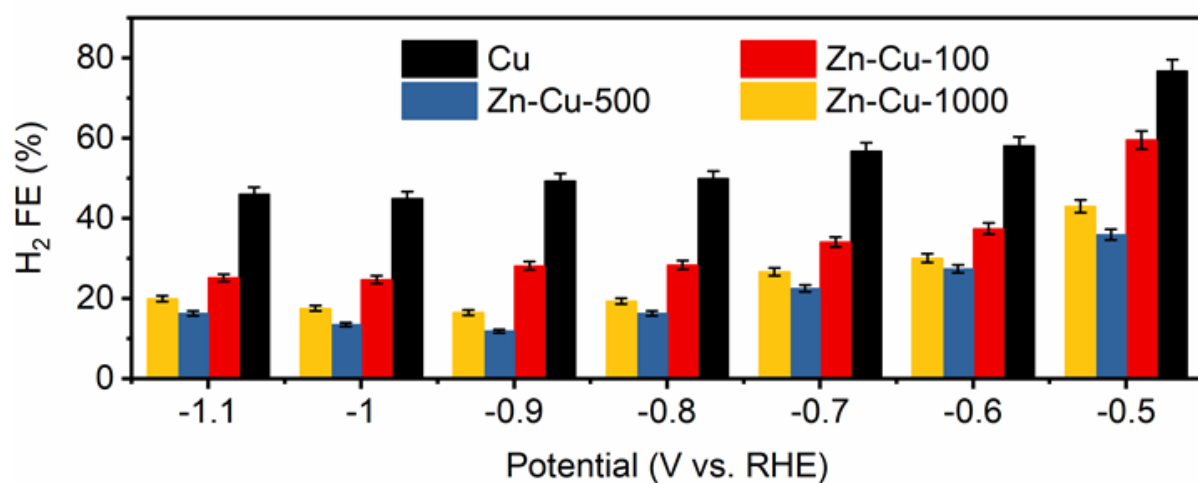
Supplementary Fig. 5. Capacitive behaviors of Zn electrodes. CV curves of Cu, Zn-Cu-100, Zn-Cu-500, and Zn-Cu-1000 with a potential range from -0.46 to -0.57 V vs. SCE in an Ar-saturated 0.5 M Na₂SO₄ electrolyte.



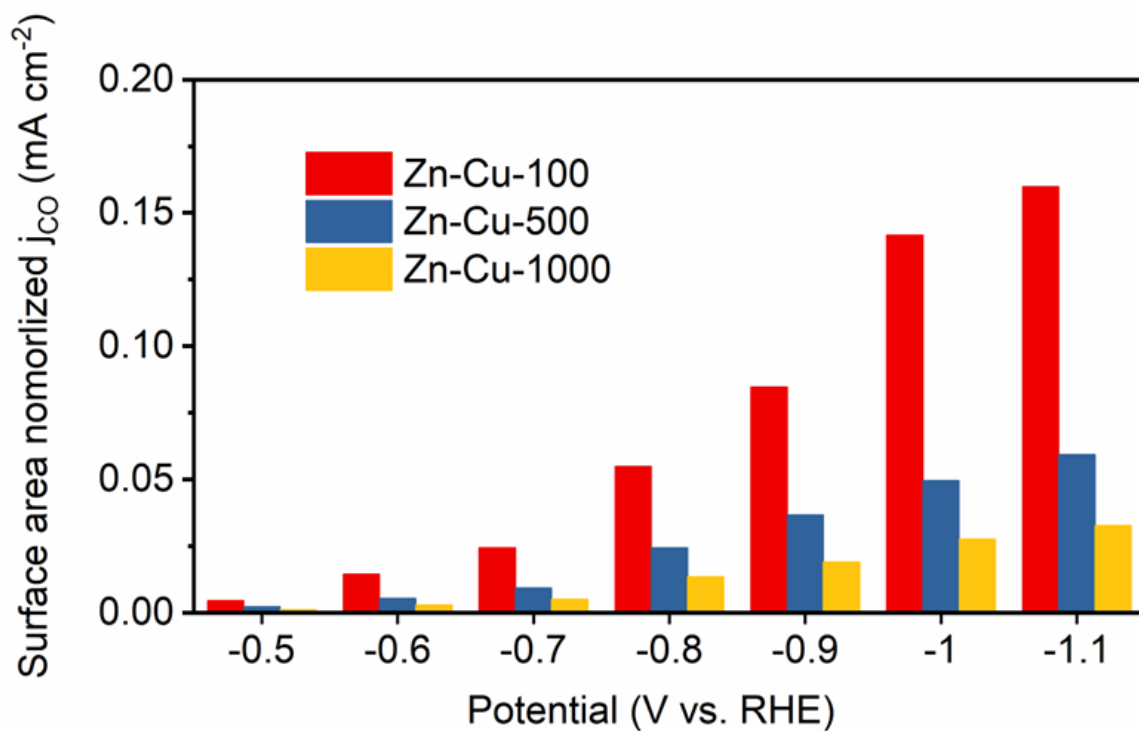
Supplementary Fig. 6. The capacitance (C_{dl}) of Zn electrodes. The plot of charging current density difference versus the scan rate.



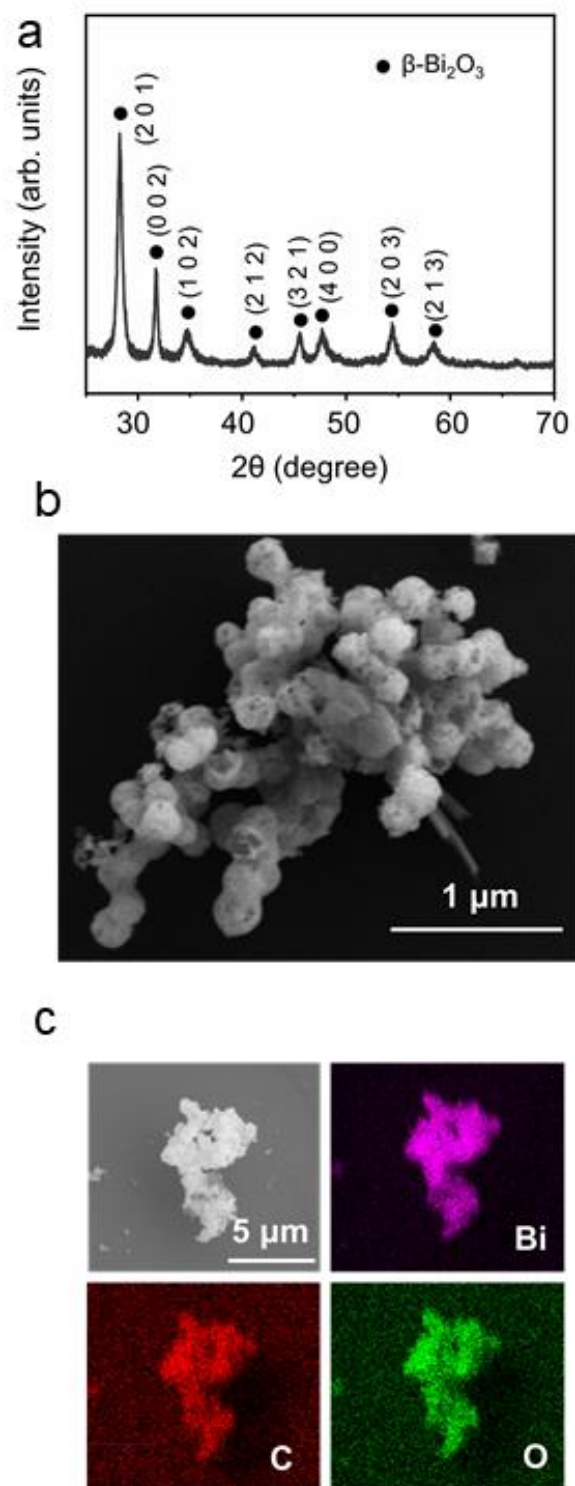
Supplementary Fig. 7. The product distribution of CO₂RR on Zn electrode. FE of various products on (a) Cu and (b) Zn-Cu-500 electrode at different potentials in a H-cell. The error bar represents standard deviation from three independent measurements.



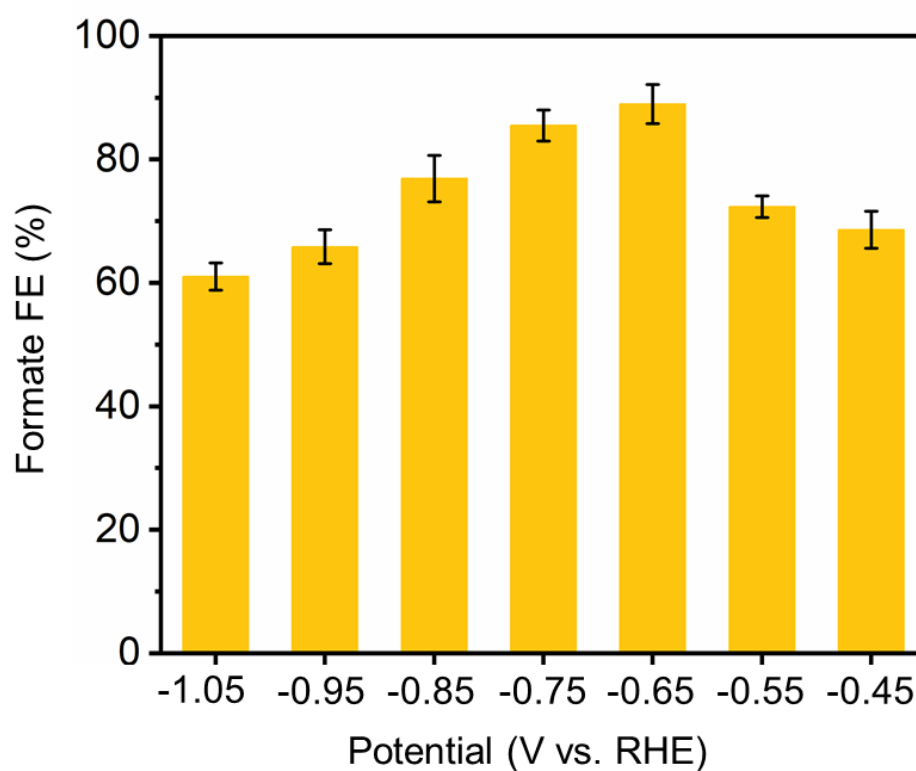
Supplementary Fig. 8. H₂ FE of Cu, Zn-Cu-100, Zn-Cu-500 and Zn-Cu-1000 at different potentials in a H-cell. The error bar represents standard deviation from three independent measurements.



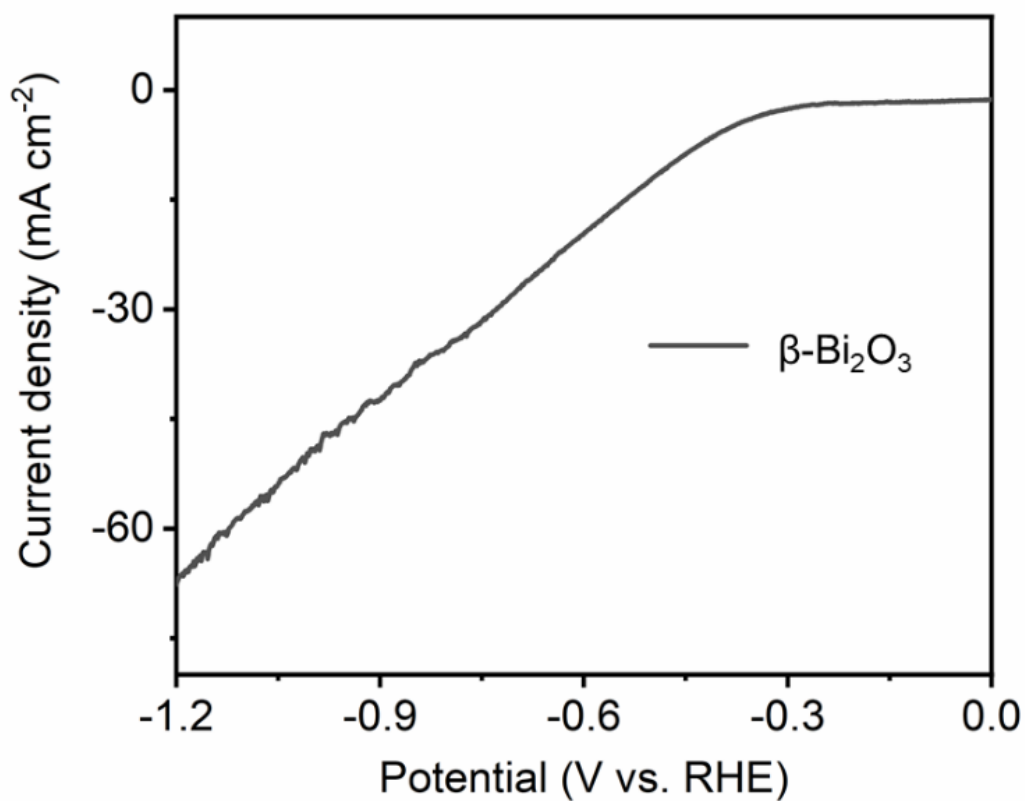
Supplementary Fig. 9. The surface-area-normalized current densities of Zn-Cu-100, Zn-Cu-500 and Zn-Cu-1000 at different potentials.



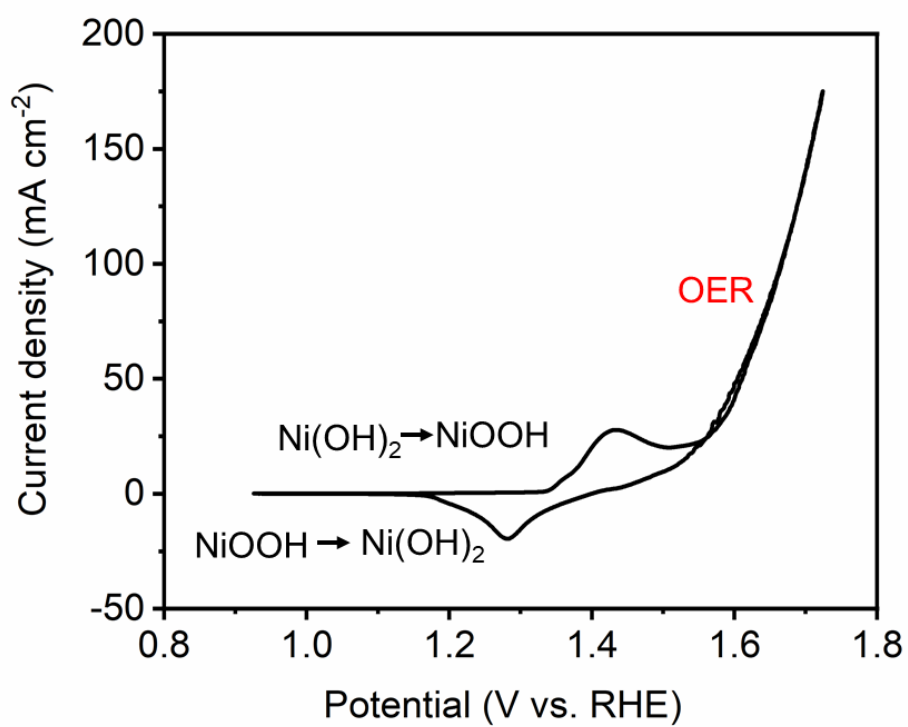
Supplementary Fig. 10. Characterizations of Bi_2O_3 electrode. (a) XRD pattern, (b) SEM image and (c) EDS elemental mappings of nanosphere Bi_2O_3 .



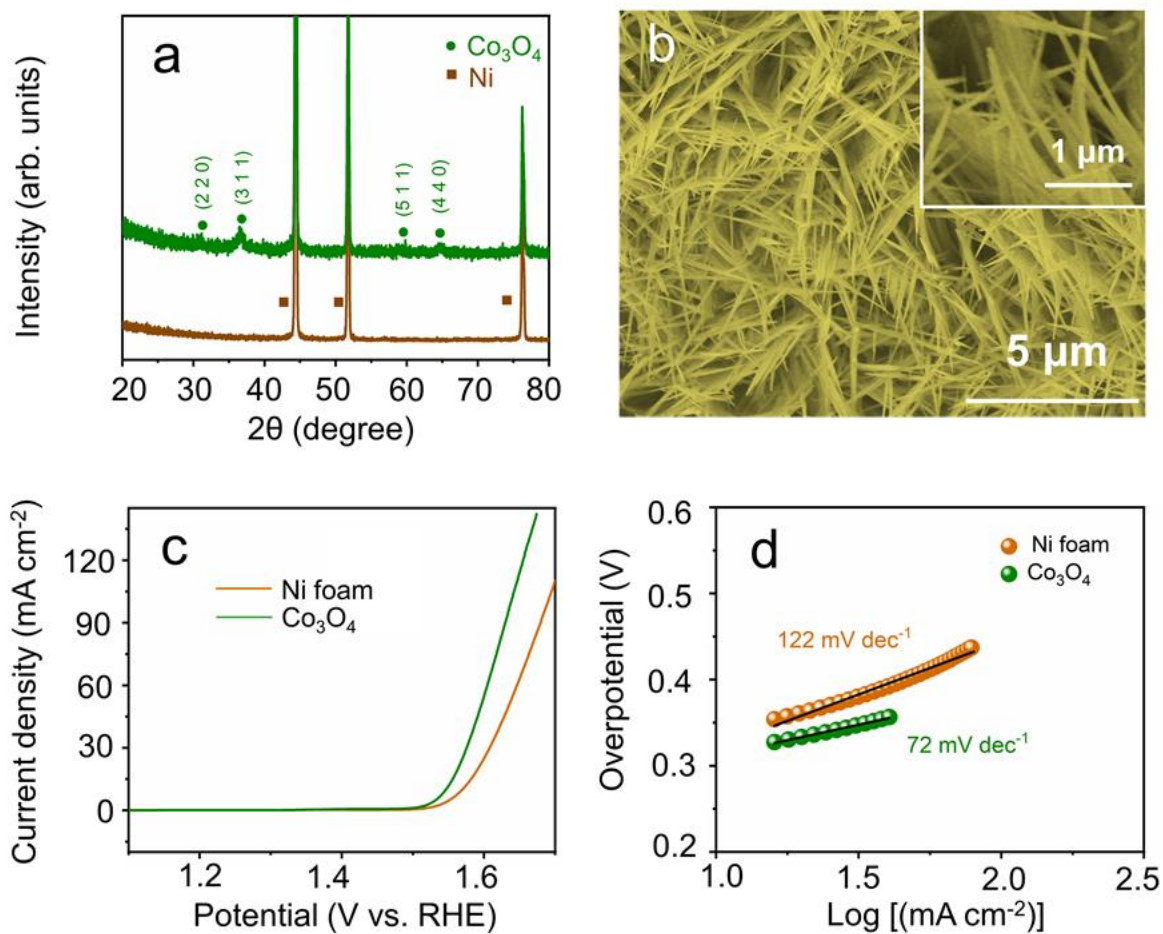
Supplementary Fig. 11. Formate FE of Bi_2O_3 at different potentials in a H-cell. The error bar represents standard deviation from three independent measurements.



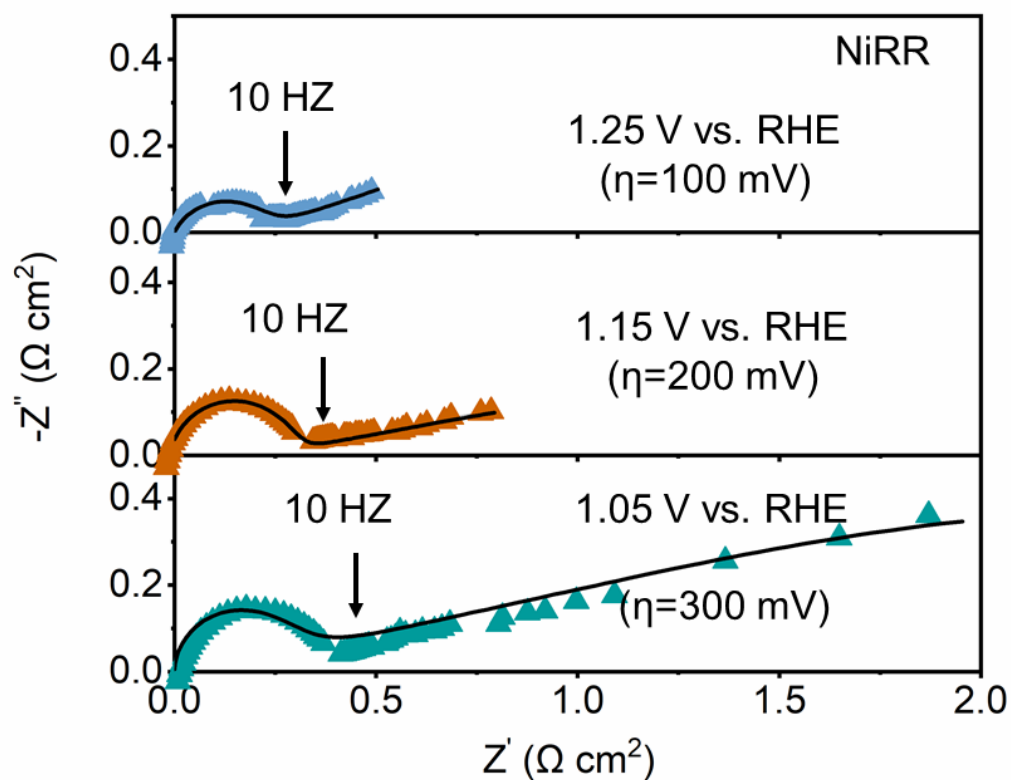
Supplementary Fig. 12. The electrochemical performance of Bi_2O_3 electrode. LSV curve of Bi_2O_3 in CO_2 -saturated 0.5 M KHCO_3 electrolyte with a scan rate of 5 mV s^{-1} .



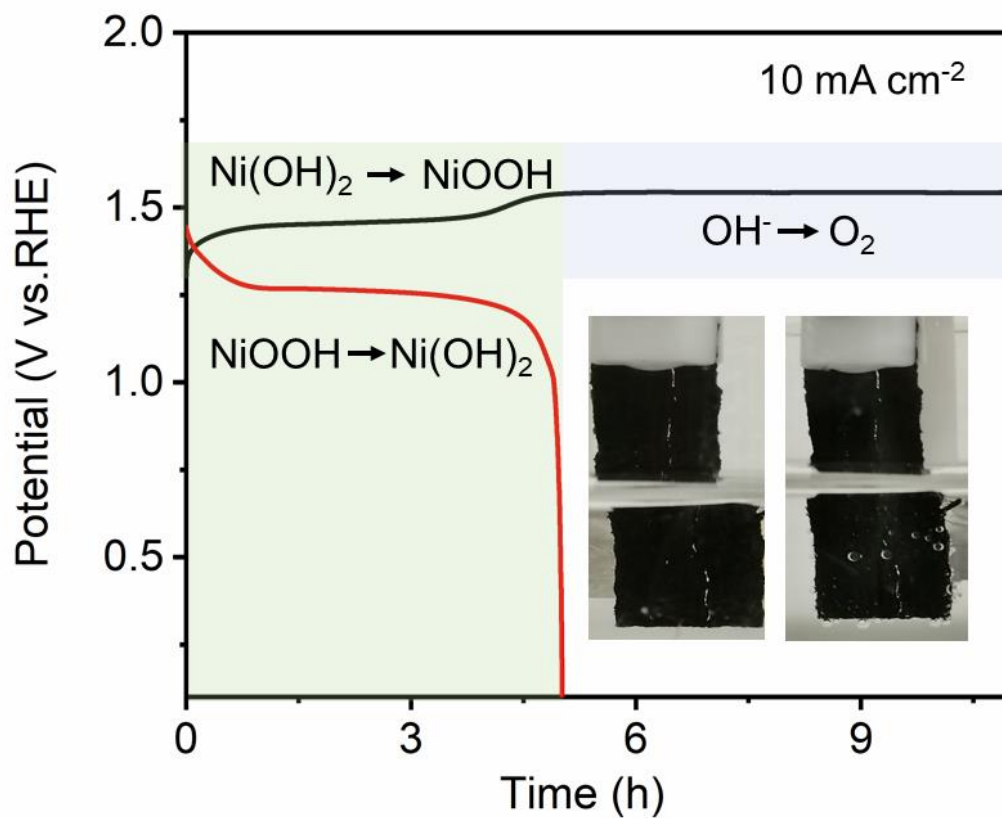
Supplementary Fig. 13. The electrochemical performance of Ni(OH)₂ electrode. CV of the Ni(OH)₂ electrode at scan rate of 1 mV s⁻¹ in 1.0 M KOH at 25 °C. The solution resistance was 1.35 Ω.



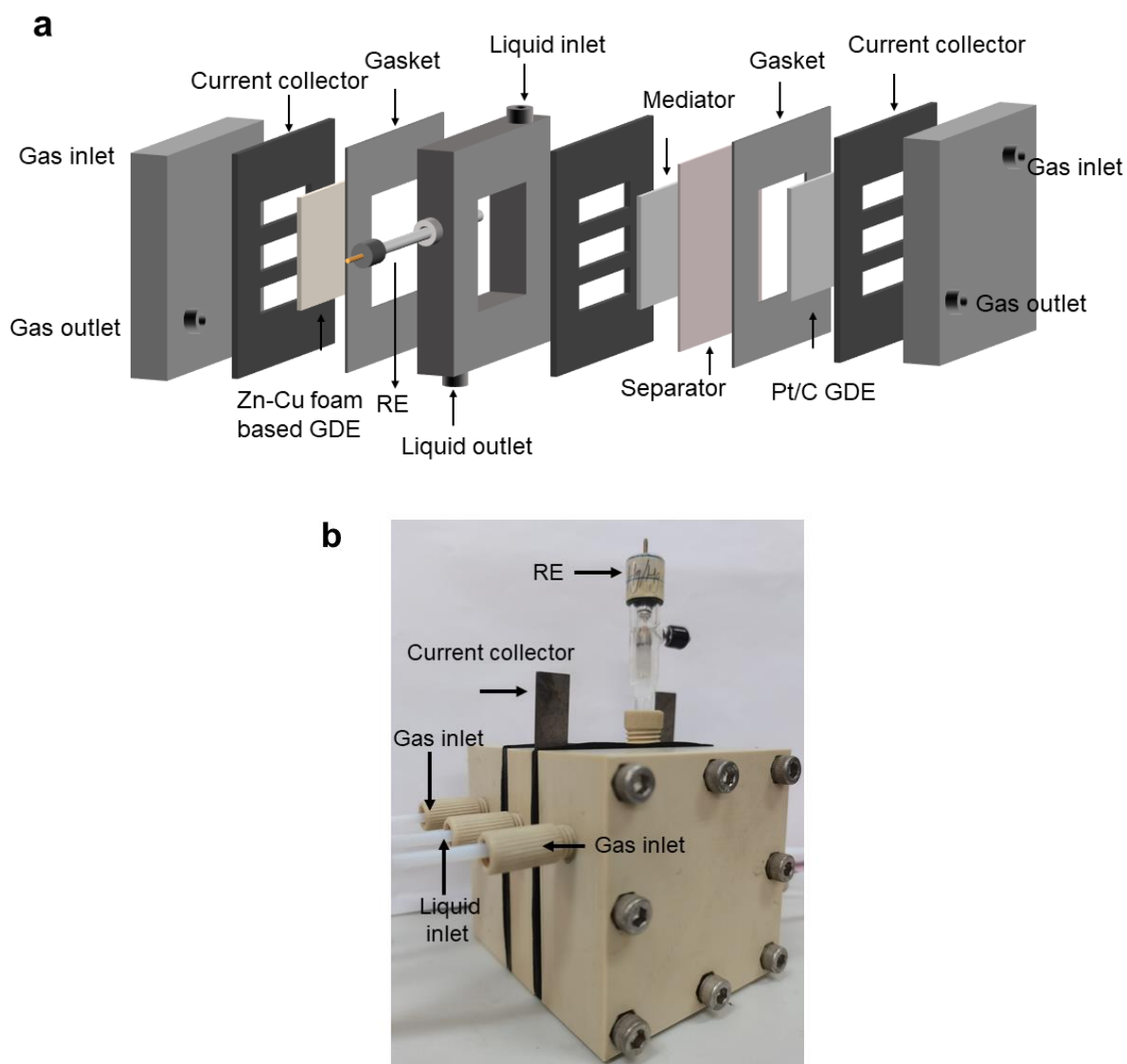
Supplementary Fig. 14. Characterizations and performances of Co₃O₄ electrodes. (a) XRD patterns of Ni foam and Co₃O₄-Ni; (b) SEM image of Co₃O₄ nanowires on the Ni foam; (c) LSV results of Ni foam and Co₃O₄-Ni; (d) Tafel plots of OER on Co₃O₄-Ni and Ni foam. The solution resistances of Ni foam and Co₃O₄ electrode were 1.07 and 1.25 Ω, respectively.



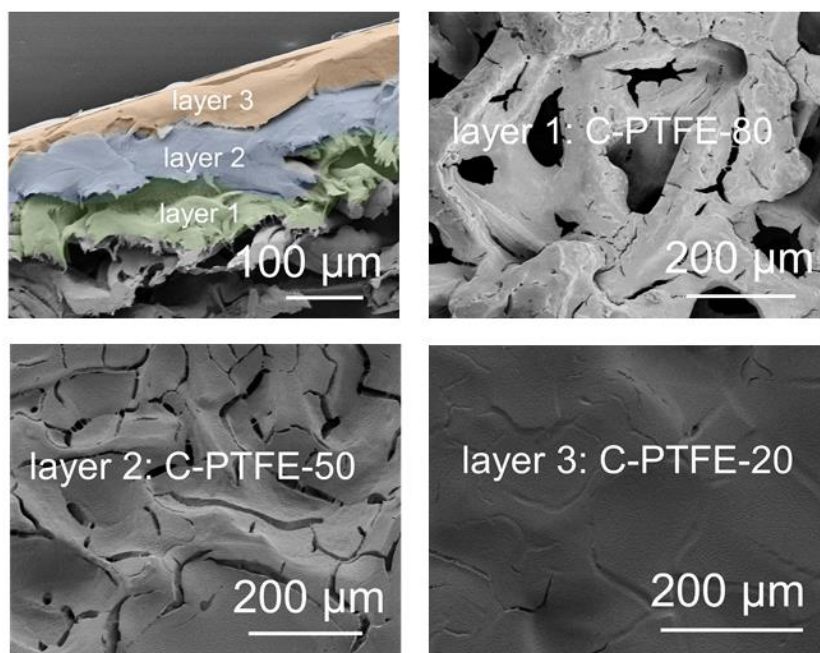
Supplementary Fig. 15. Nyquist plots of Ni(OH)₂/NiOOH electrode acquired at 1.25, 1.15, and 1.05 V vs. RHE.



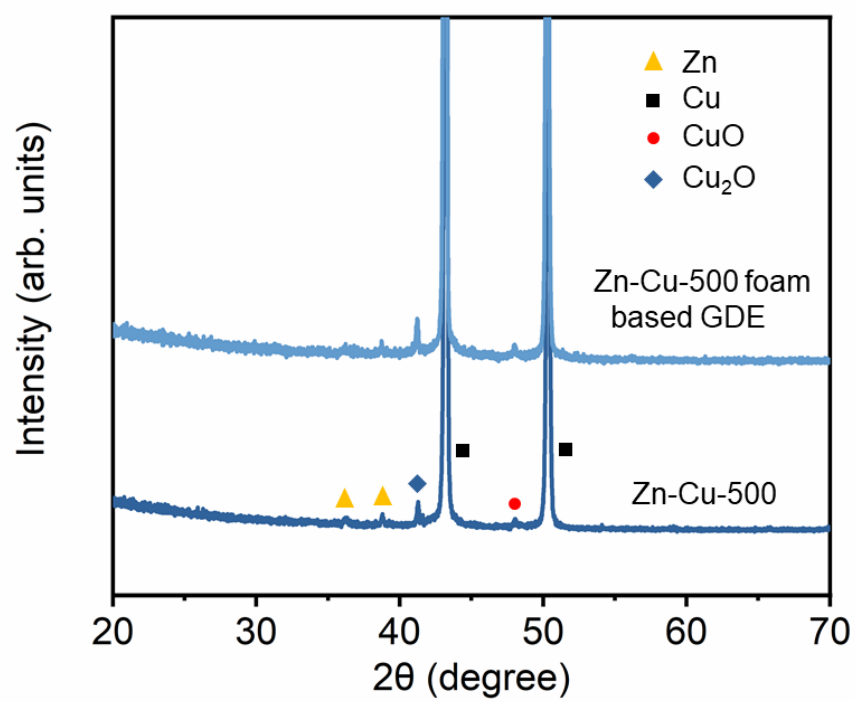
Supplementary Fig. 16. Chronopotentiometric curve of $\text{Ni(OH)}_2/\text{NiOOH}$ conversion at a constant current of 10 mA cm^{-2} ; inset shows photo profiles of Ni(OH)_2 oxidation (left) and overoxidation of Ni(OH)_2 (right) which leads to OER with the bubble evolution.



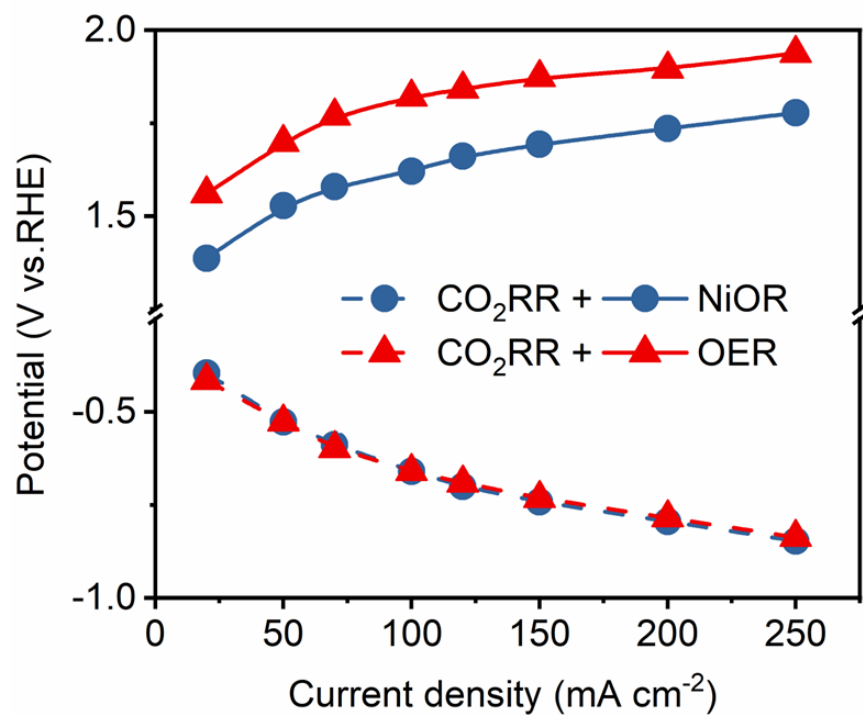
Supplementary Fig. 17. The cell structure of H₂-integrated CO₂RR. (a) schematic representation of the cell assembly; (b) the photograph of the cell.



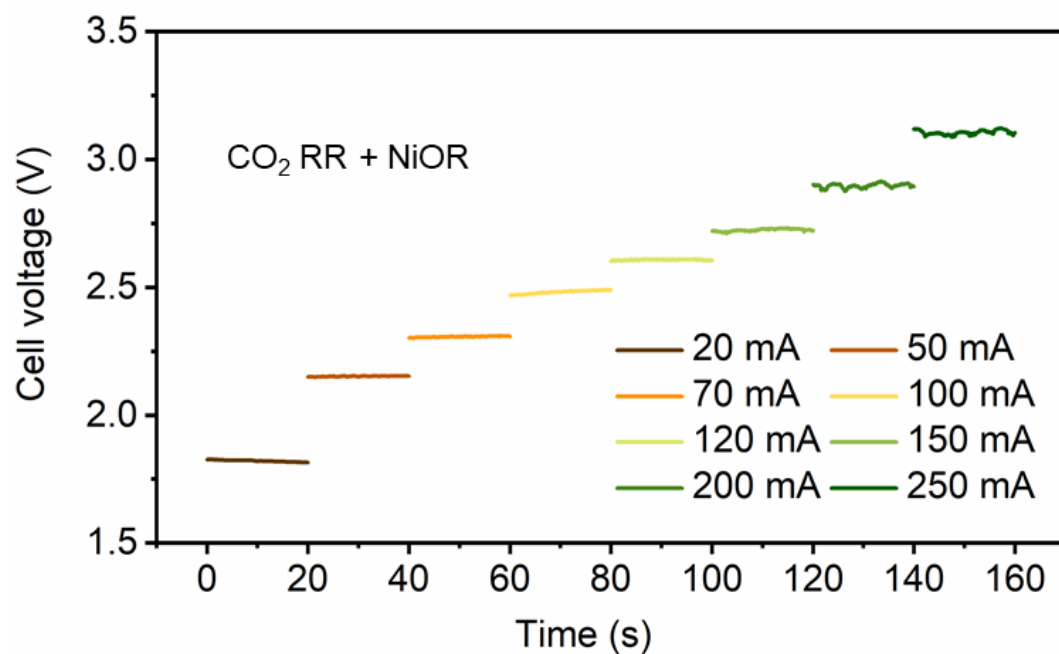
Supplementary Fig. 18. The morphology of Zn-Cu-500 foam GDE. SEM images of the gradient functional layer fabricated via the “layer-by-layer” method and top views of the surface of each layer.



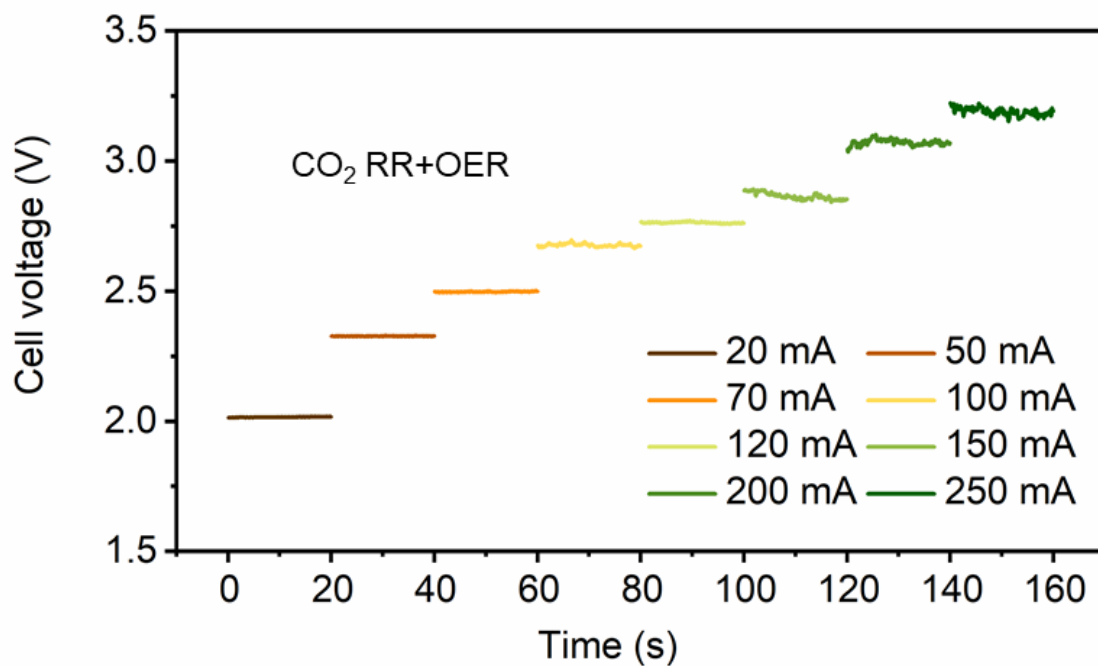
Supplementary Fig. 19. XRD patterns of Zn-Cu-500 foam and Zn-Cu-500 foam based GDE.



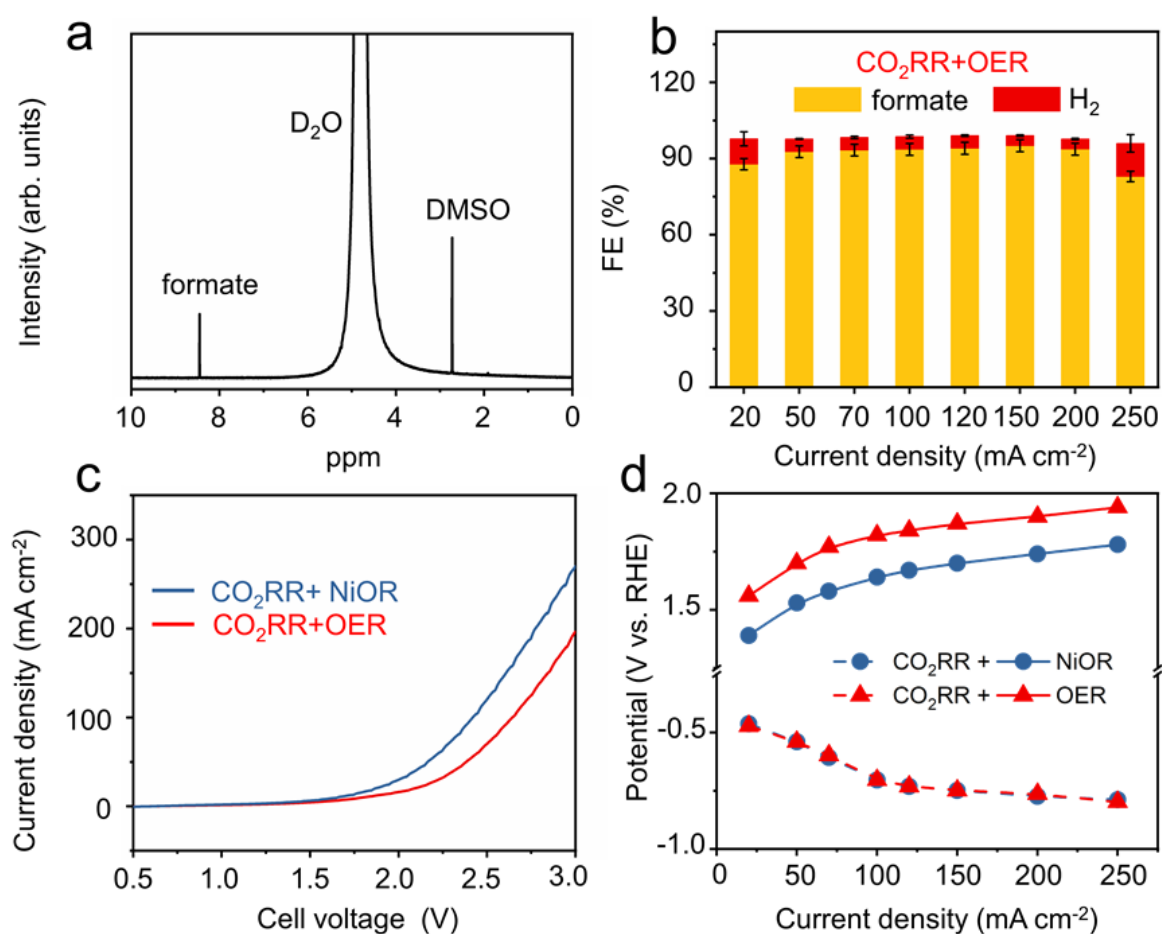
Supplementary Fig. 20. Polarization curves of cathode and anode in the combined CO₂RR+OER and CO₂RR+NiOR processes for CO production.



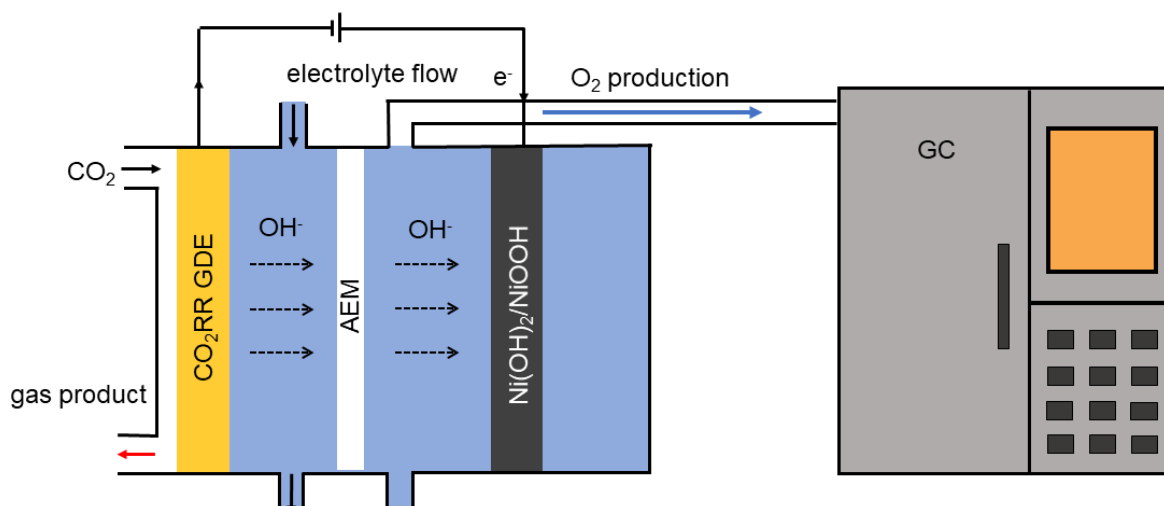
Supplementary Fig. 21. Representative potentials to obtain the polarization curve of CO₂RR+NiOR at 20, 50, 70, 100, 120, 150, 200, and 250 mA cm⁻² for CO production.



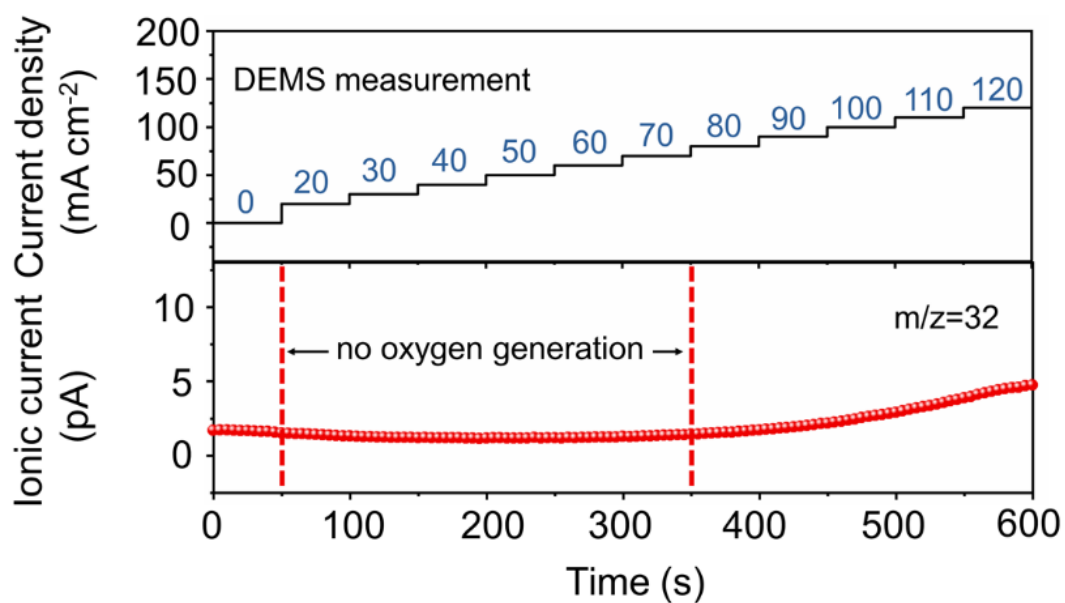
Supplementary Fig. 22. Representative potentials to obtain the polarization curve of $\text{CO}_2\text{RR+OER}$ at 20, 50, 70, 100, 120, 150, 200, and 250 mA cm^{-2} for CO production.



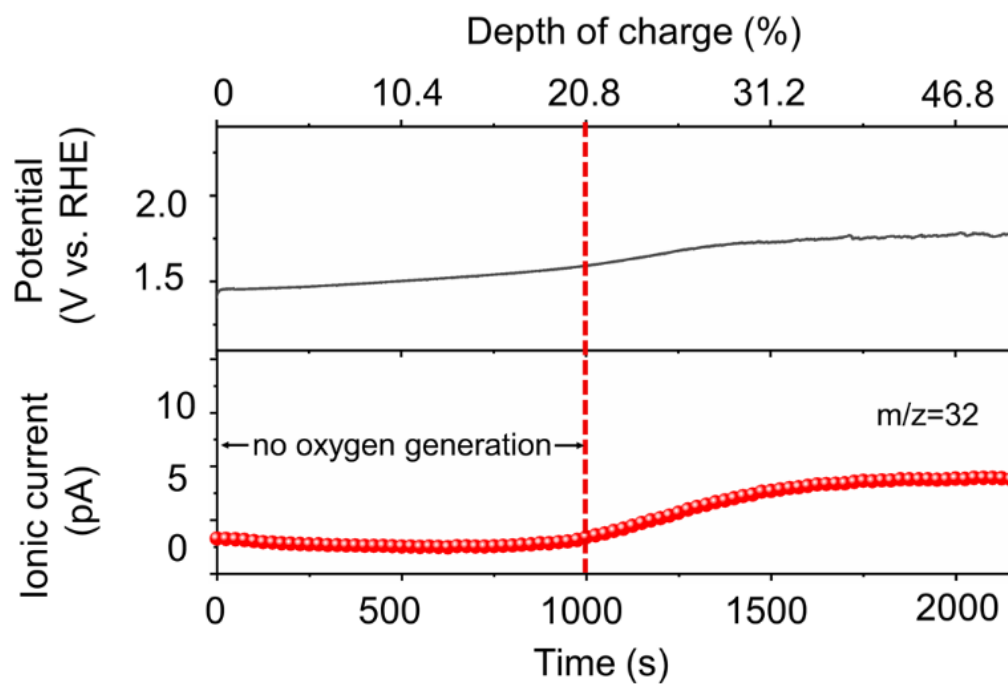
Supplementary Fig. 23. CO_2RR performance for formate production in the cell. (a) ^1H NMR spectra of the cathode effluent from the cell based on a Bi_2O_3 GDE; (b) Faradaic efficiencies in $\text{CO}_2\text{RR}+\text{OER}$ system for formate production (the error bar represents standard deviation from three independent measurements); (c) polarization curves of $\text{CO}_2\text{RR}+\text{NiOR}$ and $\text{CO}_2\text{RR}+\text{OER}$ for formate production; (d) polarization curves of cathode and anode in the combined $\text{CO}_2\text{RR}+\text{OER}$ and $\text{CO}_2\text{RR}+\text{NiOR}$ processes for formate production.



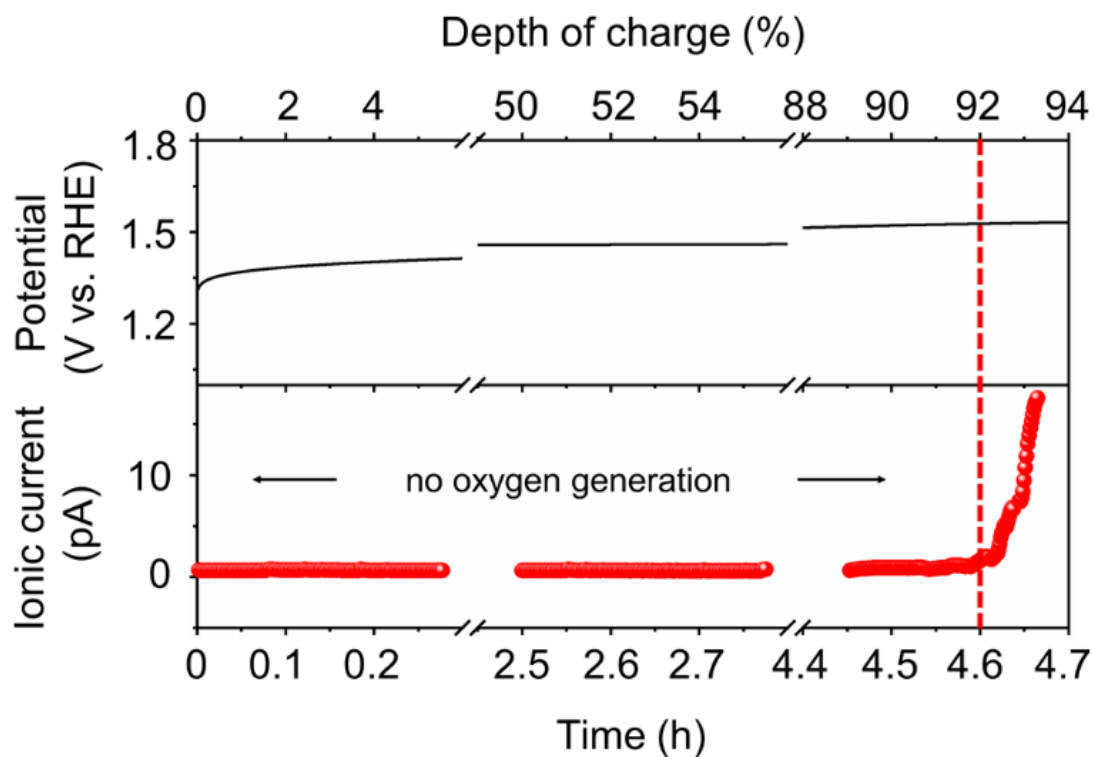
Supplementary Fig. 24. The schematic illustration of the cell optimization to measure O_2 production at the anode side. The anode and cathode compartments were separated by a 130 μm -thick anion-exchange membrane (AEM, Fumasep FAA-3-PK-130). Before test, AEM was immersed in a 0.1 M KOH solution for 6 h.



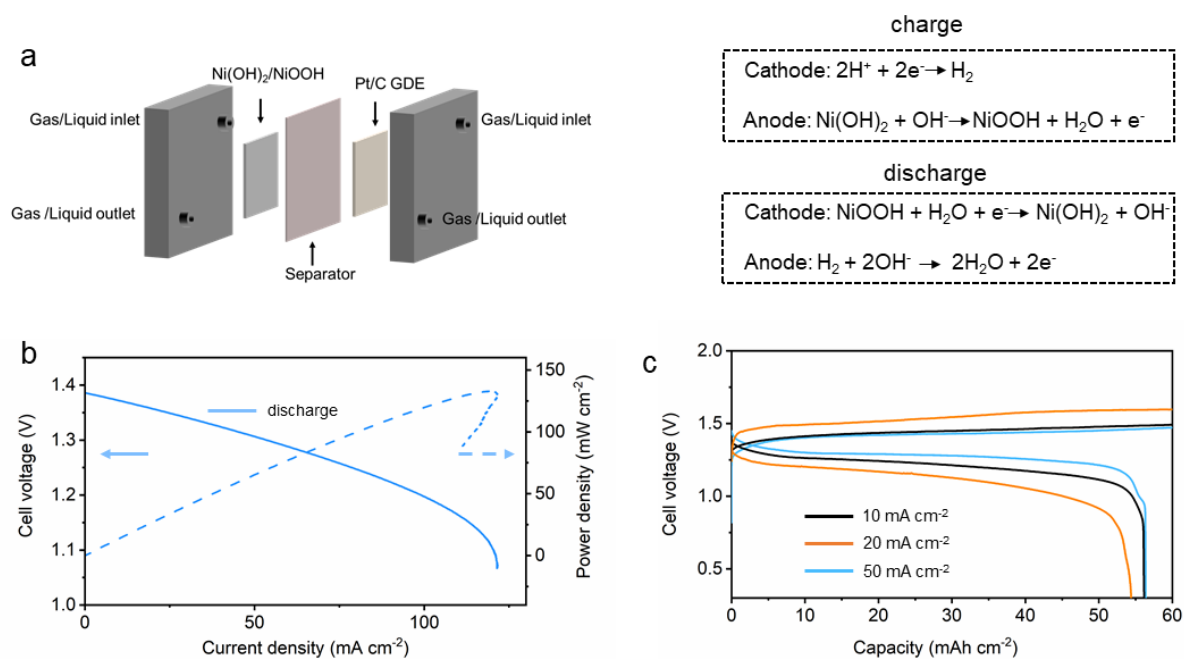
Supplementary Fig. 25. Monitoring O_2 production by DEMS. The ionic current response in the DEMS measurement in which $\text{Ni}(\text{OH})_2$ was used as the working electrode biased at various constant current densities.



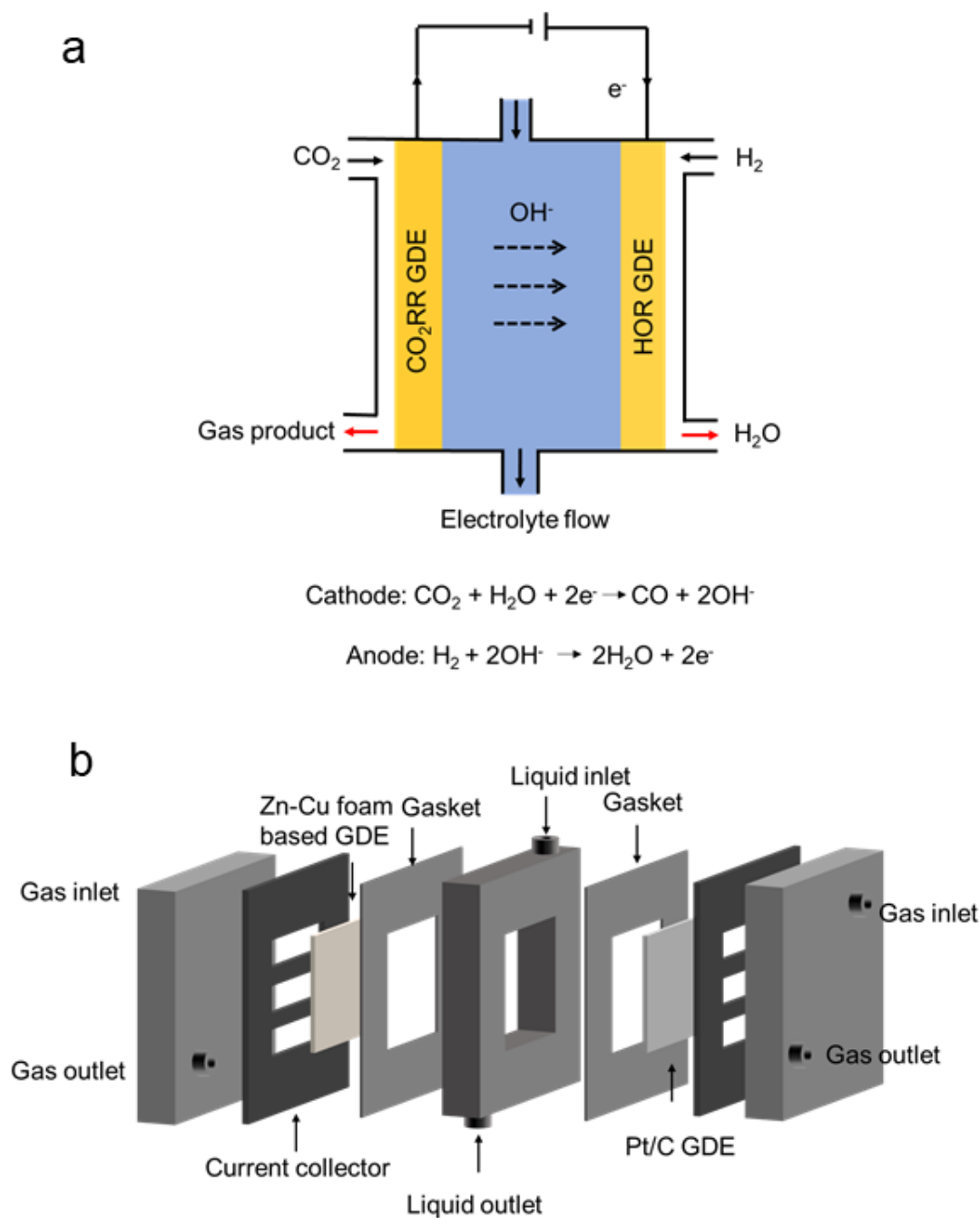
Supplementary Fig. 26. Monitoring O₂ production by DEMS. The ionic current response in the DEMS measurement in which Ni(OH)₂ was used as the working electrode biased at a constant current density equivalent to 150 mA cm⁻² of the cell.



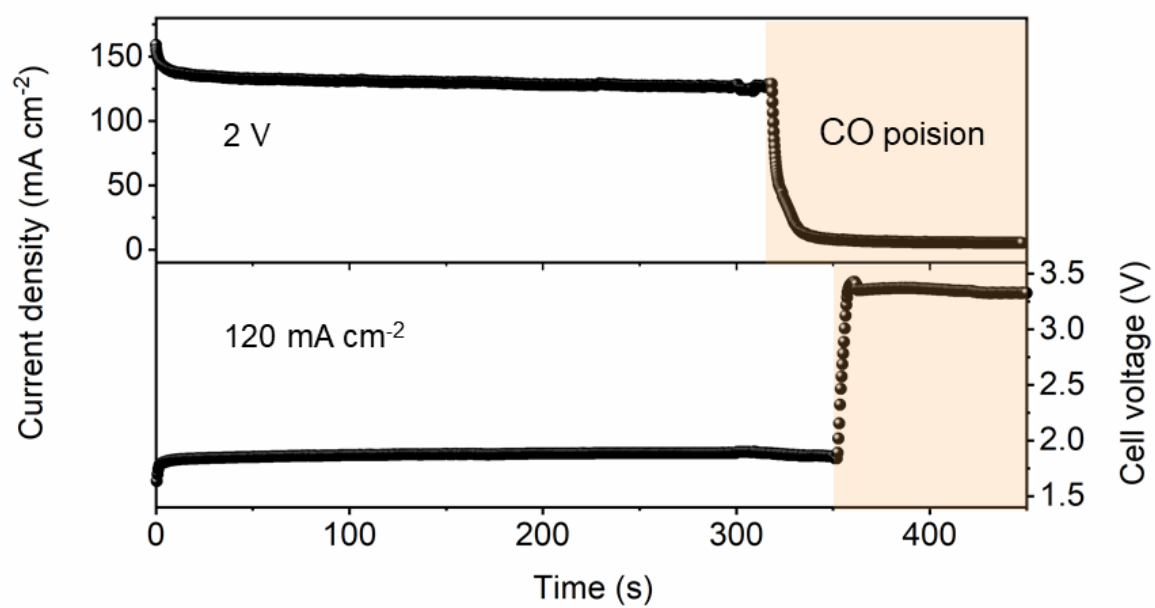
Supplementary Fig. 27. Monitoring O₂ production by DEMS. The ionic current response in the DEMS measurement in which Ni(OH)₂ was used as the working electrode biased at a constant current density equivalent to 40 mA cm⁻² of the cell.



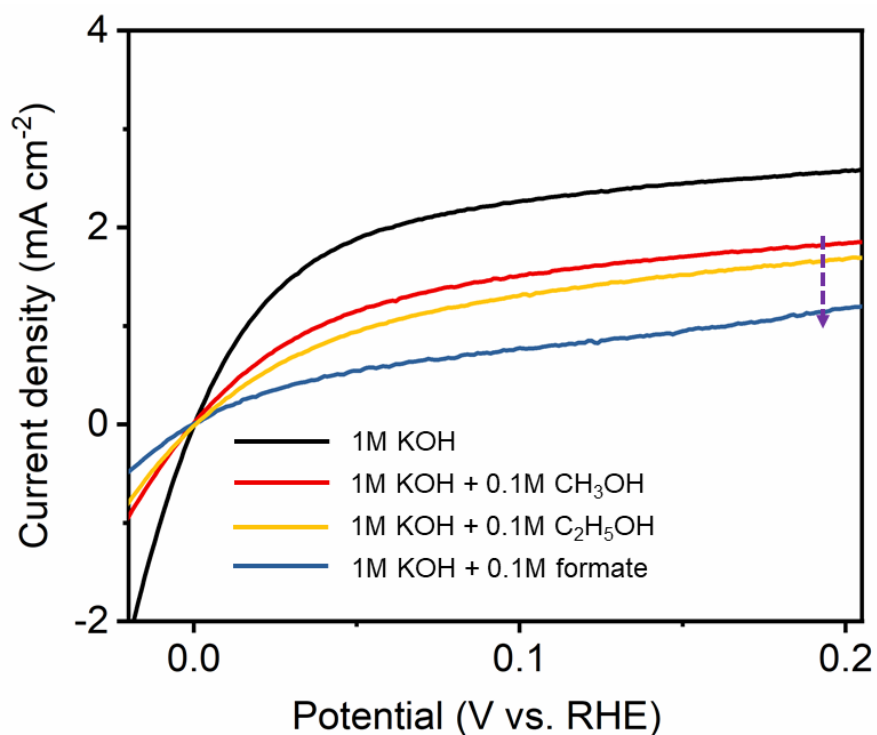
Supplementary Fig. 28. The performance of a home-built Ni-H₂ battery. (a) Schematic structure representation of Ni-H₂ battery; (b) I-V and I-P curves of the battery; (c) galvanostatic charge-discharge curves of the battery at different currents. The electrolyte was 1 M KOH.



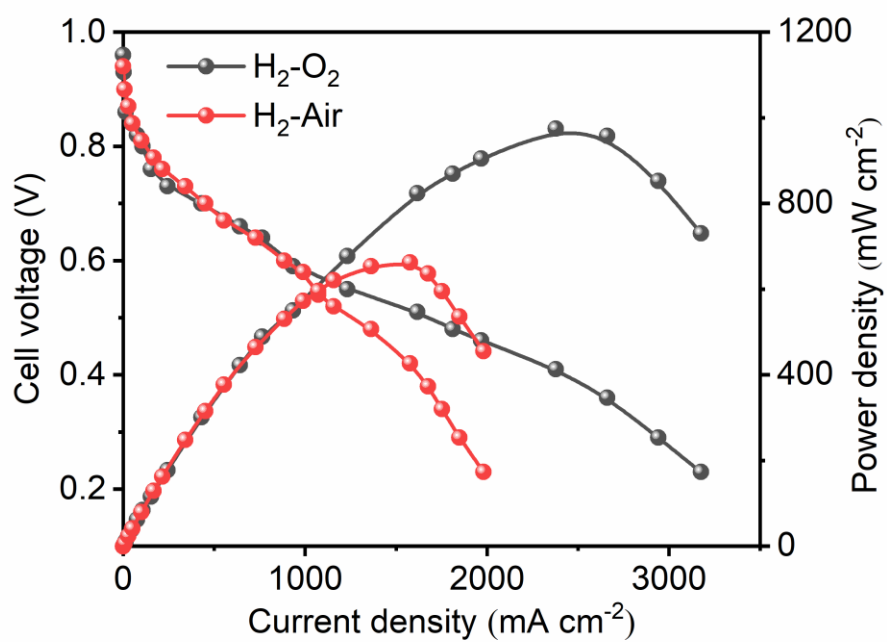
Supplementary Fig. 29. The cell structure for direct pairing of CO₂RR with HOR. (a) The working principle of CO₂RR coupled with the anodic HOR directly; (b) schematic representation of the cell configurations for CO₂RR with HOR occurring on the anode directly.



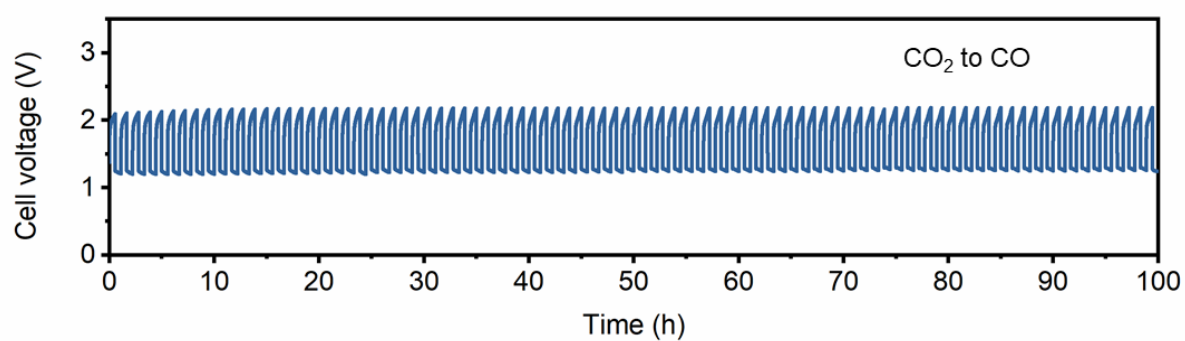
Supplementary Fig. 30. I-t and V-t curves of CO_2RR coupled with HOR occurring at the anode simultaneously in the cell.



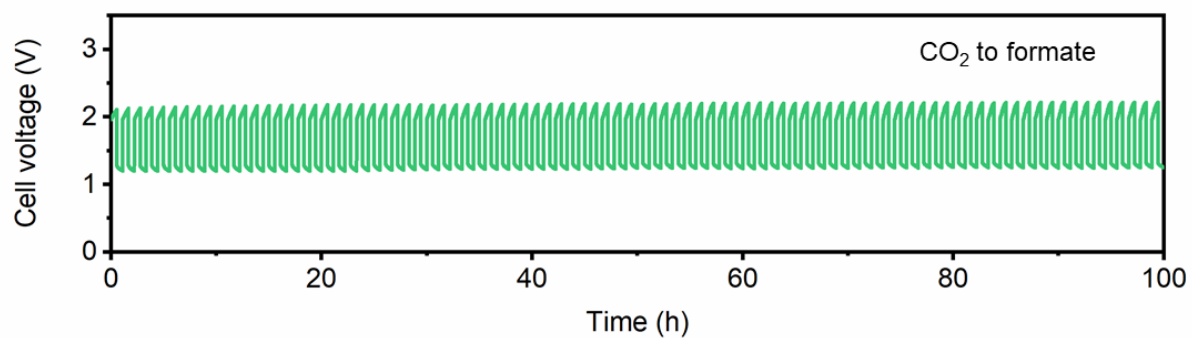
Supplementary Fig. 31. The influence of typical CO_2RR product on the HOR activity of Pt/C electrode. HOR polarization curves of Pt/C in 1 M KOH, 1 M KOH + 0.1 M CH_3OH , 1 M KOH + 0.1 M $\text{C}_2\text{H}_5\text{OH}$, and 1 M KOH + 0.1 M formate.



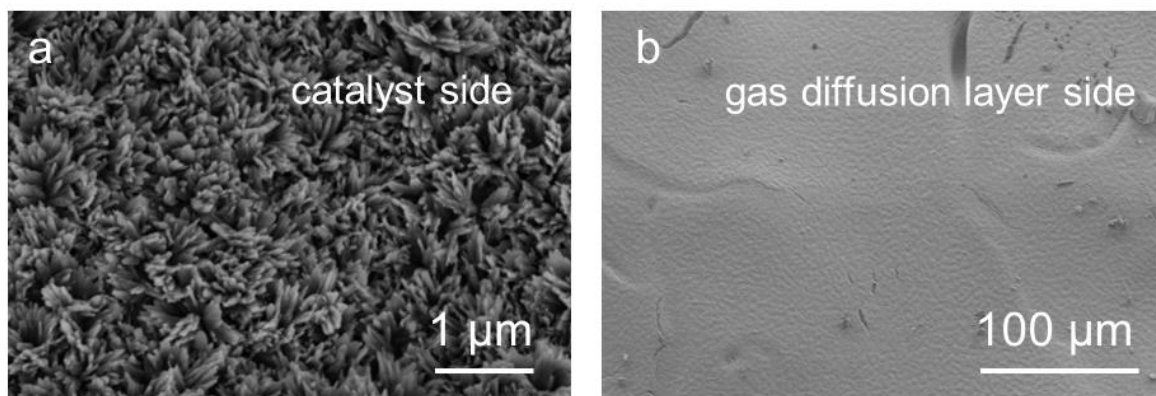
Supplementary Fig. 32. PEMFC performance. Polarization and power density plots of H₂-O₂ and H₂-air PEMFC.



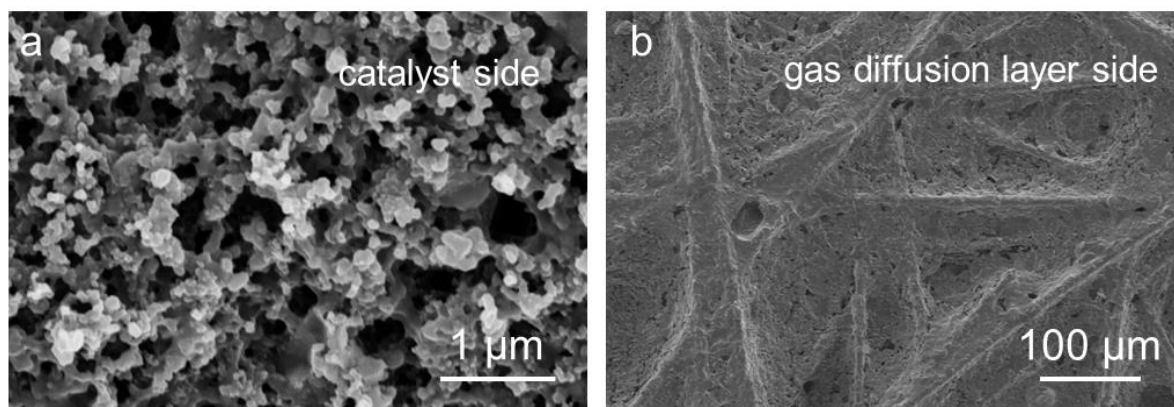
Supplementary Fig. 33. Longevity test of H₂-integrated CO₂RR combining periodical swap between Step 1 and Step 2 at 50 mA cm⁻² for CO production.



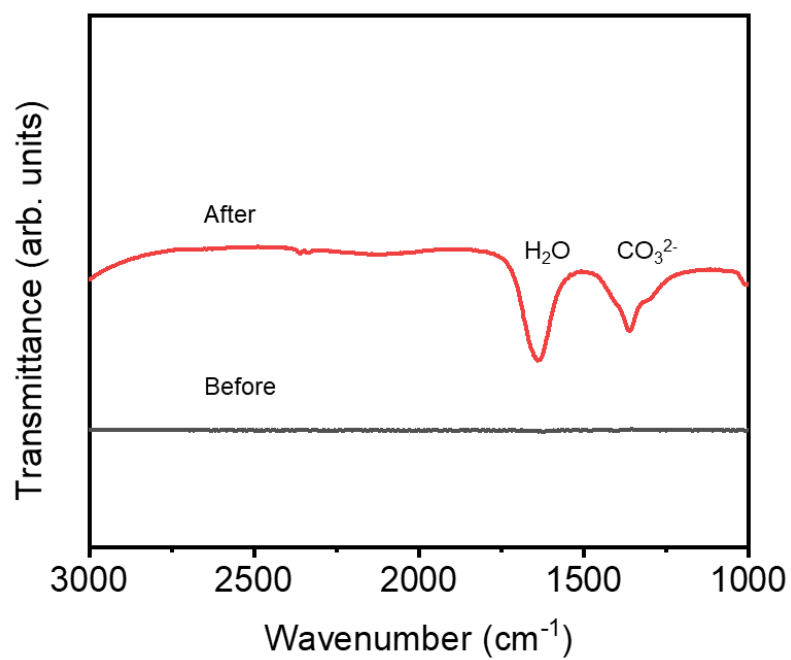
Supplementary Fig. 34. Longevity test of H₂-integrated CO₂RR combining periodical swap between Step 1 and Step 2 at 50 mA cm⁻² for formate production.



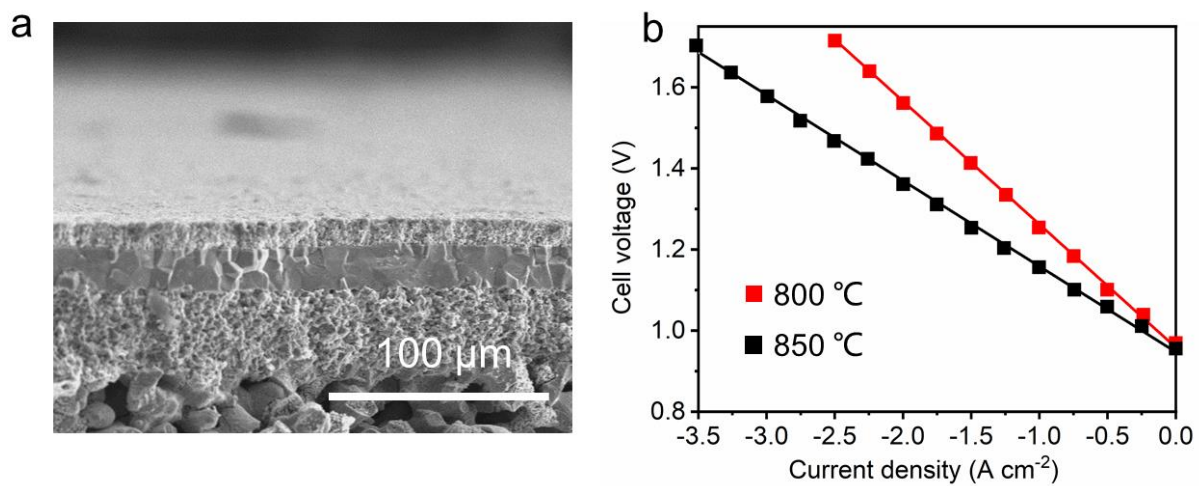
Supplementary Fig. 35. Characterizations of spent GDE. SEM images of Zn-Cu foam based GDE at the (a) catalysts side and (b) gas diffusion layer side after longevity test.



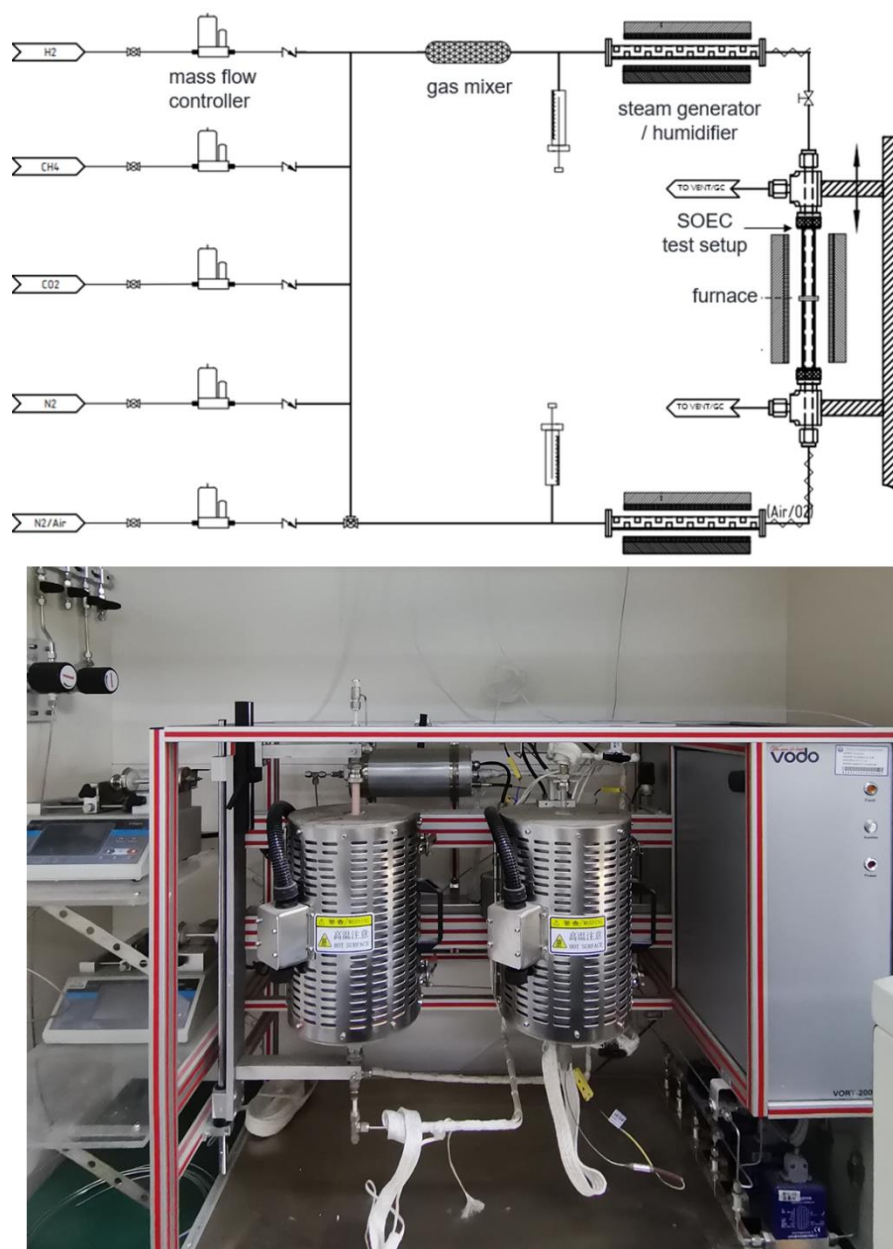
Supplementary Fig. 36. Characterizations of spent GDE. SEM images of Bi_2O_3 -based GDE at the (a) catalysts side and (b) gas diffusion layer side after longevity test.



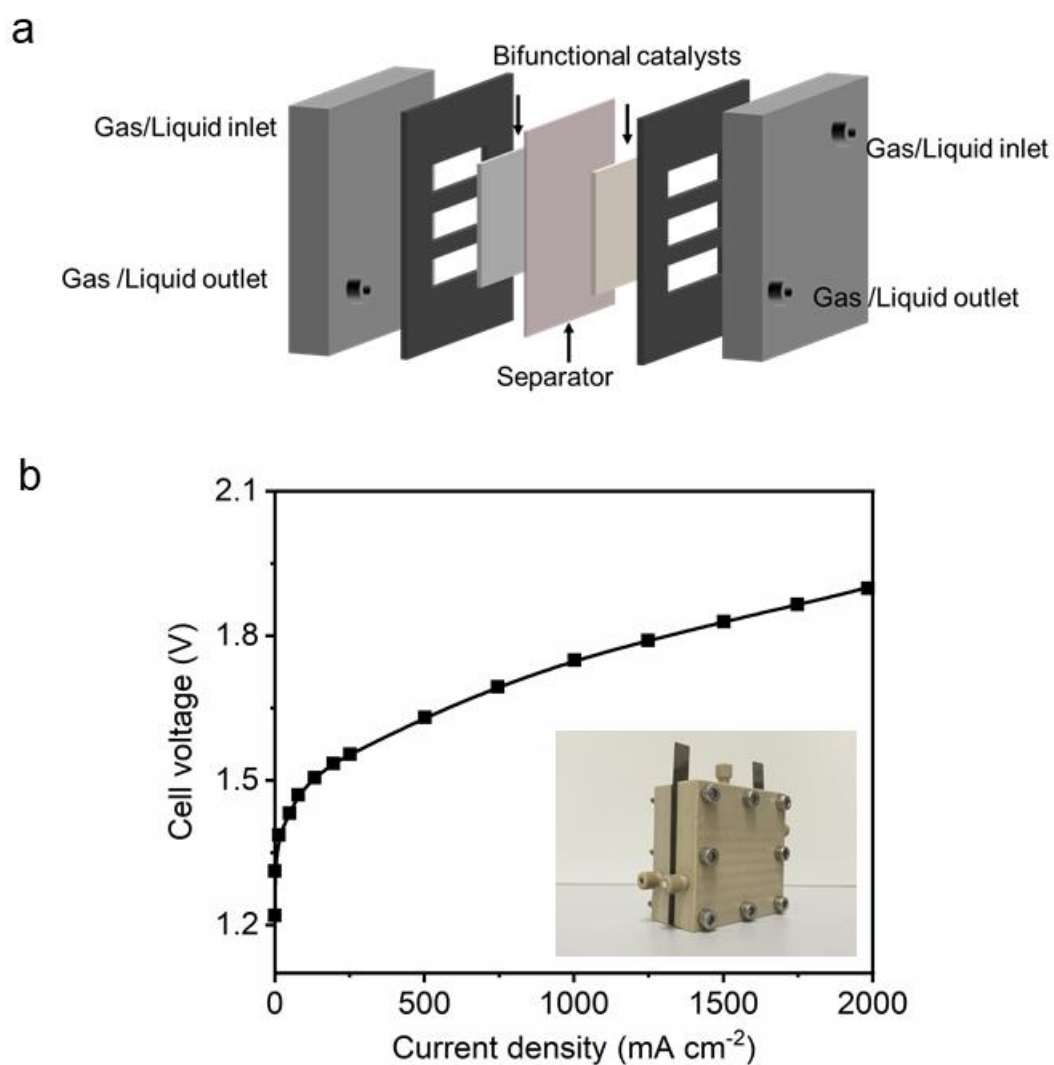
Supplementary Fig. 37. FTIR spectra of the Pt/C GDE before and after the operation in the H₂-integrated CO₂RR for the generation of CO.



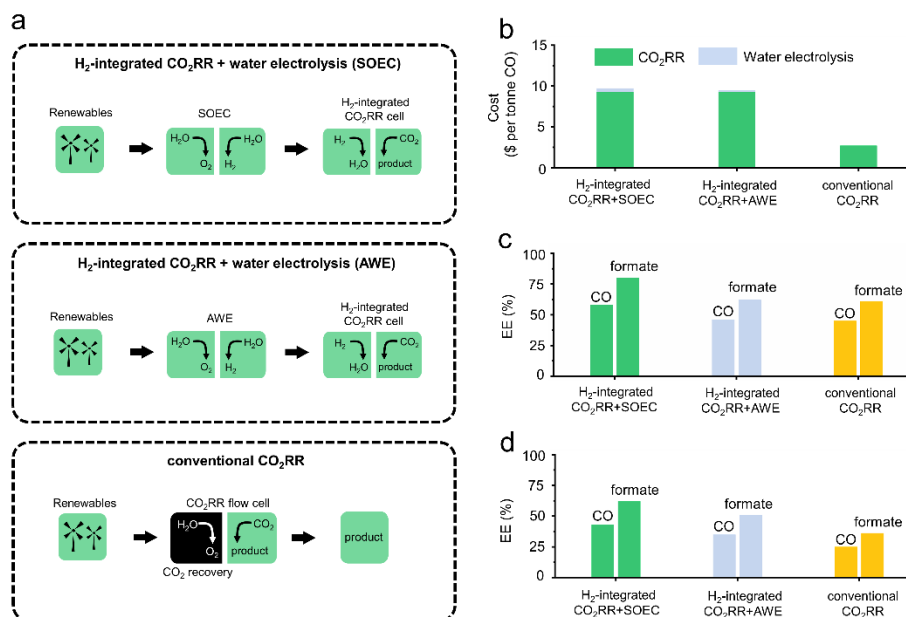
Supplementary Fig. 38. The characterizations and performance of SOEC. (a) cross-sectional SEM image of the electrode-supported SOEC; (b) polarization plots of water electrolysis at 800 °C and 850 °C, the inlet feedstock is 50 vol% H_2O balanced by H_2 .



Supplementary Fig. 39. The design and photograph of a home-built solid oxide cells (SOC) test system for both SOEC and solid oxide fuel cells (SOFC) test.



Supplementary Fig. 40. The cell structure and performance of alkaline water electrolyzer (AWE). (a) Schematic structure of a home-built AWE; (b) the polarization plot of water electrolysis in 6M KOH at 85 °C and ambient pressure.



Supplementary Fig. 41. Techno-economic and energy efficiency analysis of H₂-integrated CO₂RR coupled with water electrolysis. (a) Schematic illustration of H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR; (b) preliminary techno-economic analysis based on CO production for H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR, only materials cost was considered; comparison of energy efficiency between H₂-integrated CO₂RR coupled with water electrolysis and conventional CO₂RR at 50 mA cm⁻² in (c) alkaline and (d) neutral electrolyte.

3. Supplementary Notes

Supplementary Note 1: Calculation of voltage efficiency

The voltage efficiency of CO₂RR (Step 1 or conventional) was calculated as follows:

$$\text{Voltage efficiency}_1 = \frac{E_0}{E_c} \times 100\% \quad \text{Supplementary Equation (1)}$$

where E_c is the measured cell voltage, E_0 is the Nernst potential at standard conditions.

The voltage efficiency of “H₂-electricity” conversion (Step 2 or fuel cell) was calculated as follows:

$$\text{Voltage efficiency}_2 = \frac{E_c}{E_0} \times 100\% \quad \text{Supplementary Equation (2)}$$

For Step 2 in our cell, E_0 equals to 1.35 V. And for conventional H₂ fuel cell, E_0 equals to 1.23 V.

Supplementary Note 2: Energy consumption analysis

We carried out the energy consumption analysis (GJ per tonne product) to evaluate the energy efficiency of H₂-integrated CO₂RR coupled with representative water electrolysis technologies (SOEC or AWE) in comparison with the conventional CO₂RR. The schematic comparison of three systems is shown in Supplementary Fig. 41. All values were obtained from the polarization curve of the corresponding electrochemical device. The total energy consumption for a specific process may comprise the following components:

(1) CO₂RR. The energy consumption of CO₂RR could be expressed as follows:

$$W[J] = E_c[V] \times \frac{Q[C]}{FE_{product}} \quad \text{Supplementary Equation (3)}$$

where E_c is the cell voltage at the selected current density; Q is the consumed electric charge when 1 tonne product was produced; $FE_{product}$ is the Faradaic efficiency of the desired product.

(2) SOEC. The total electric charge consumed in the production of H₂ equals to that consumed in the H₂-integrated CO₂RR cell. Thus, the energy consumption of SOEC at a given condition could be calculated via equation (3) where Q becomes the total charge.

(3) AWE. The method is identical with that of calculating SOEC energy consumption.

(4) Anodic CO₂ recovery. At pH=7, the energy consumption of anodic CO₂ recovery must be considered. The CO₂ crossover rate at the anode is proportional to the current. We assumed that 0.5 moles of CO₂ is lost per mole of electron transferred based on the literatures^{19-20, 31}. Thus, the amount of evolved CO₂ at the anode could be determined using the following

equation:

$$\text{Theoretical } CO_2 \text{ crossover [mol]} = 0.5 \times \frac{Q[C]}{F[\frac{C}{mol}] \times FE_{product}} \quad \text{Supplementary Equation (4)}$$

we assume the CO₂ capture cost, via amine scrubbing, is 4.0 GJ per tonne CO₂³²⁻³⁴. CO₂ loss at the cathode and in the electrolyte was not considered.

The energy efficiency (EE) of each process could be expressed as follows:

$$EE = \frac{n_j \times LHV_j}{W_{consumption}} \times 100\% \quad \text{Supplementary Equation (5)}$$

where $W_{consumption}$ is the total energy consumption, including that of water electrolysis when applicable, for each route; LHV_j is the lower heating value of product (CO: 282.98 kJ mol⁻¹; HCOOH: 209.82 kJ mol⁻¹); and n_j is the molar amount of product.

Supplementary Note 3: Techno-economic analysis

The techno-economic analysis of three processes was also evaluated based on an established model in the literature assuming a pilot plant producing 100 tonne of CO per day³⁵. To simplify our calculation model, we only consider the material cost as the operational cost of the new process is challenging to quantify accurately. The materials cost was calculated via the following equation:

$$C_{materials}[\frac{\$}{kW}] = \frac{\sum_n p_n A_n [\$]}{P[kW]} \quad \text{Supplementary Equation (6)}$$

where p is the operation power of the cell, p_n is unit price of the cell component n , and A_n is the area of each cell component. Details are shown below.

H₂-integrated CO₂RR + SOEC. The total cost for H₂-integrated CO₂RR + SOEC is ~\$9.7 per tonne CO which comprises of:

(1) Step 1 of H₂-integrated CO₂RR. The cell components contain Zn-Cu foam GDE and Ni(OH)₂/NiOOH electrode (the unit prices were shown in Supplementary Table 20). We selected the power at 50 mA cm⁻² (2.15 V, 0.11 W cm⁻²) as a reference. Thus, the calculated materials cost of Step 1 was ~\$64 kW⁻¹. The total equivalent current needed to produce 100 tonne CO per day can be obtained via Equation (7) assuming 100% CO FE.

$$\text{Total current needed [A]} = \frac{\text{mole number of CO production} [\frac{mol}{day}] \times \text{electrons transfer} \times F [\frac{C}{mol}]}{24 \times 3600 [\frac{s}{day}]}$$

Supplementary Equation (7)

The total equivalent current needed was thus 7976604 A. The required power was 17149.7 kW using the following equation:

$$\text{Power consumed [kW]} = \text{Total current needed [A]} \times \text{cell voltage [V]}$$

Supplementary Equation (8)

Then, the total materials cost of Step 1 was \$1097580 using the following equation:

$$\text{Total materials cost [\$/]} = \text{Power Consumed [kW]} \times \text{Electrolyzer Cost [\$/kW]} \quad (9)$$

This cost refers to the overall one-time investment cost of materials, which needs to be translated into a cost per tonne of CO. Turning a long-term investment into a daily cost is based on a capital recovery factor (CRF) defined as follows:

$$\text{CRF} = \frac{i(1+i)^{\text{lifetime}}}{(1+i)^{\text{lifetime}}-1} \quad \text{Supplementary Equation (10)}$$

where i is a discount rate assumed to be 7%³⁵; the lifetime of 5 years is used for all materials and all conditions. Thus, CRF was calculated to be 0.24389.

The final materials cost can be expressed as:

$$\text{materials cost} \left[\frac{\$}{\text{tonne CO}} \right] = \frac{\text{CRF} \times \text{total materials cost [\$/]}}{\text{capacity factor} \left[\frac{\text{days}}{\text{year}} \right] \times \text{production} \left[\frac{\text{tonne CO}}{\text{day}} \right]} \quad \text{Supplementary Equation (11)}$$

Assuming a plant capacity factor of 0.9, we found the material cost was \$8.1 per tonne CO in the Step 1 of H₂-integrated CO₂RR.

(2) Step 2 of H₂-integrated CO₂RR. We only considered Pt GDE and separator, as other components were considered in Step 1. The selected the maximum power density of 0.22 W cm⁻². Thus, the calculated materials price for Step 2 was ~\$15.4 kW⁻¹. Because the consumed charge in Step 1 and Step 2 is identical, the total equivalent current needed here was the same as that in Step 1. Using equations (8)-(11), the materials cost was ~\$1.2 per tonne CO.

(3) SOEC. The cell contains cathode (NiO and YSZ), YSZ electrolyte and anode (La_{0.8}Sr_{0.2}MnO_{3-x}). All unit prices were shown in Supplementary Table 20. The power density was selected at 2 A cm⁻² as a reference (1.34 V, 2.68 W cm⁻², see the polarization plot at 850 °C in Supplementary Fig. 38). Thus, the calculated cost was ~\$5.1 kW⁻¹, or \$0.4 per tonne CO.

H₂-integrated CO₂RR + AWE. The total cost for H₂-integrated CO₂RR + AWE is ~\$9.5 per tonne CO which comprises of

(1) H₂-integrated CO₂RR cell. See calculation details above.

(2) AWE. The AWE cell contains two Co-Ni phosphide/spinel oxide hybrid bifunctional electrodes, and a piece of separator (the unit prices were shown in Supplementary Table 20). We selected the typical working condition of 500 mA cm⁻² as a reference (1.63V, 0.3 W cm⁻², see the polarization plot in Supplementary Fig. 40). Thus, the calculated materials cost was ~\$1.9 kW⁻¹, or \$0.2 per tonne CO.

Conventional CO₂RR. The cell components contain Zn-Cu foam GDE and Co₃O₄-Ni electrode (the unit prices were shown in Supplementary Table 20). The selected power was also at 50 mA cm⁻² (2.32V, 0.12 W cm⁻²). Thus, the calculated cost was ~\$19 kW⁻¹, or \$2.7 per tonne CO.

4. Supplementary References

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