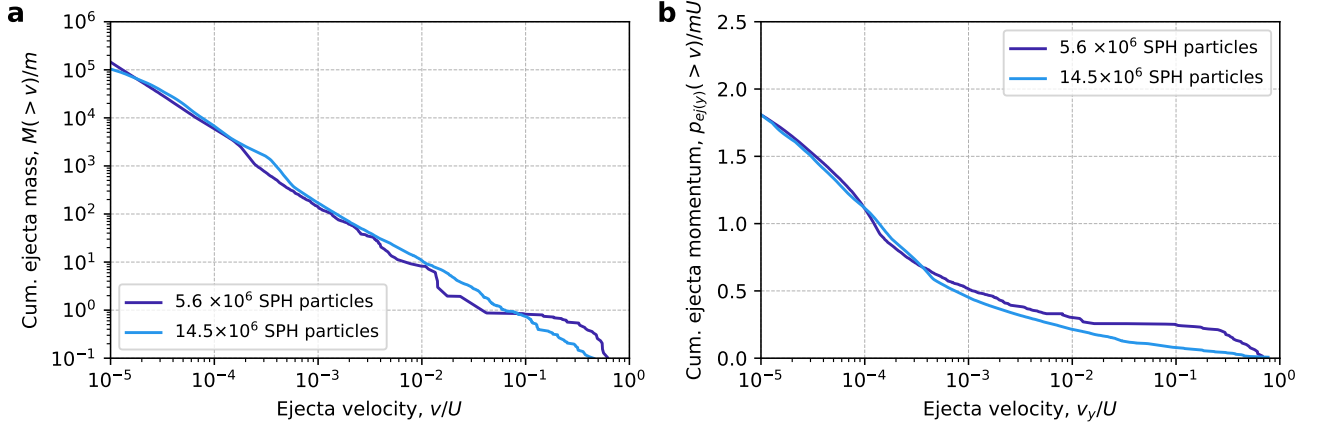


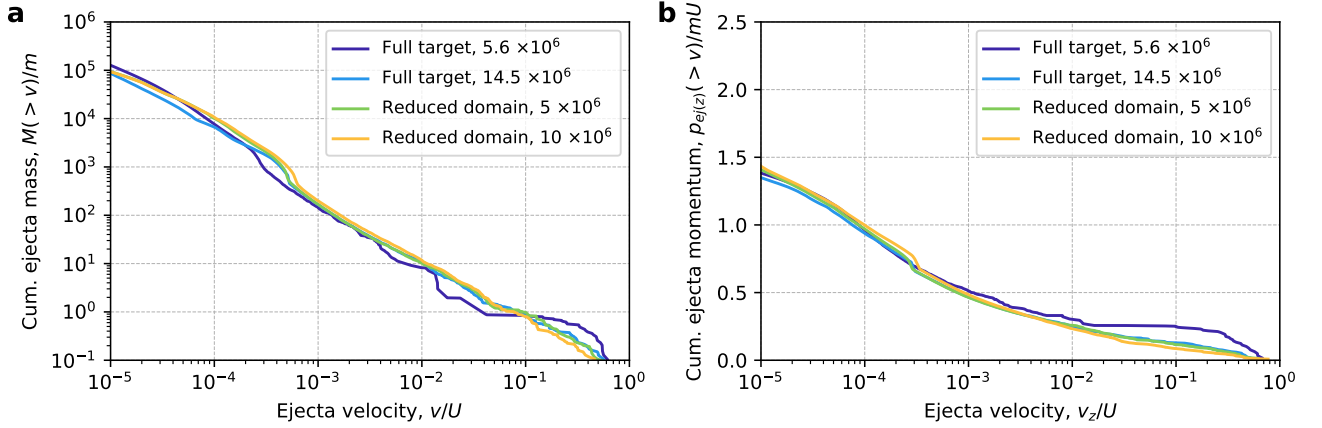
Physical properties of asteroid Dimorphos as derived from the DART impact

In the format provided by the
authors and unedited

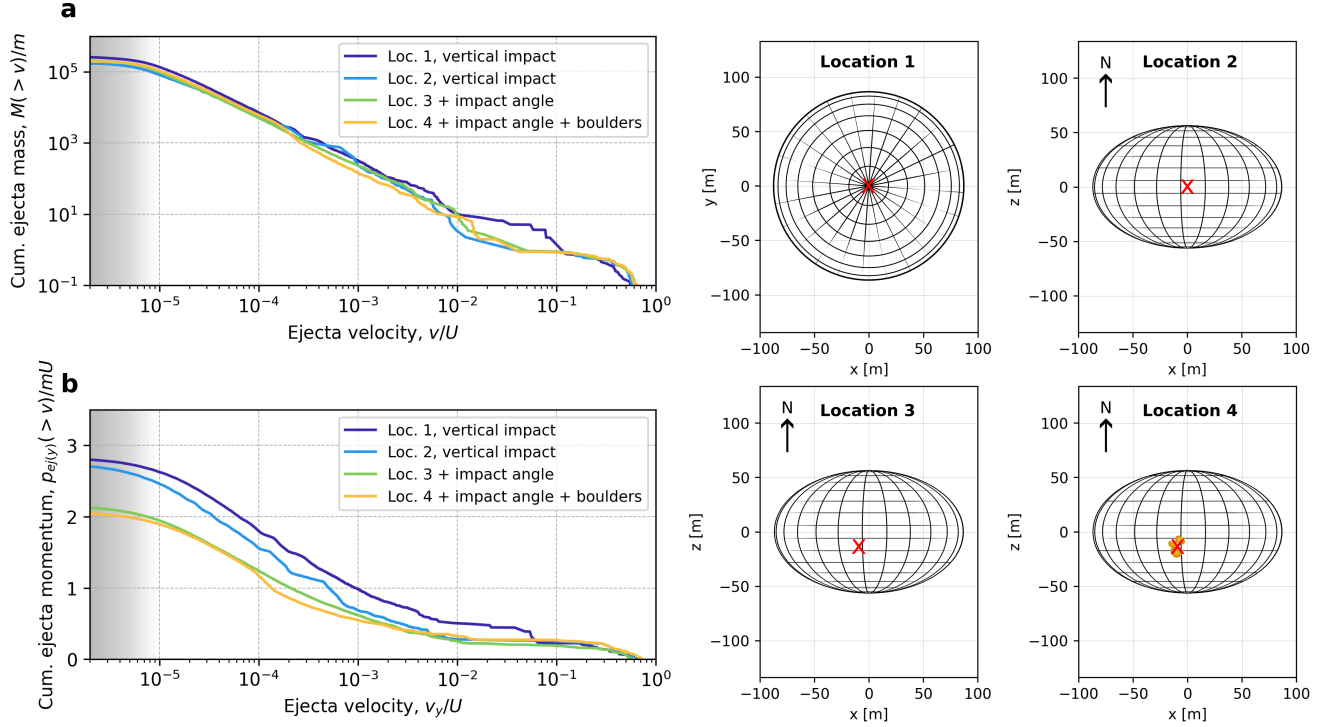
Supplementary



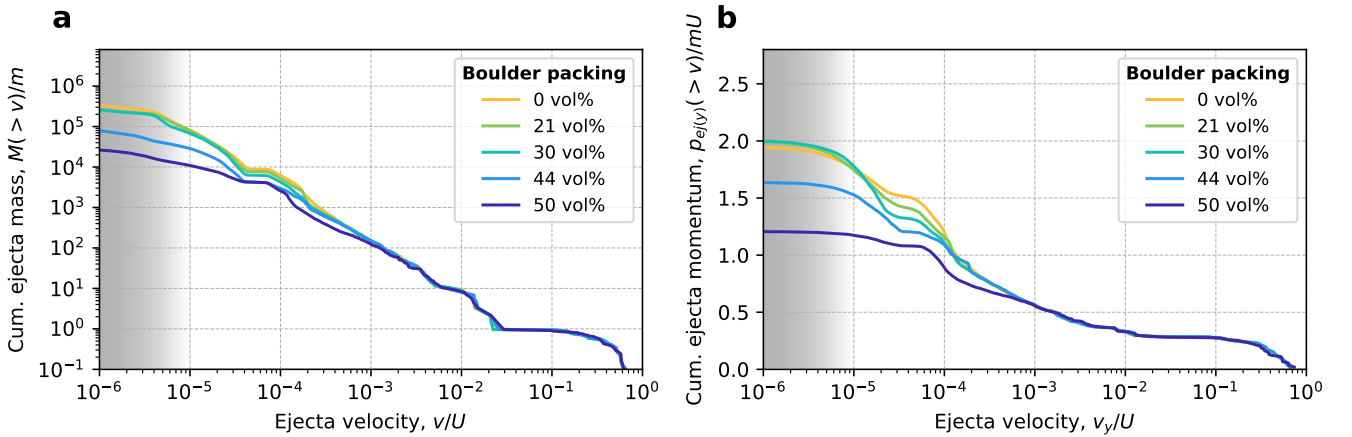
Supplementary Fig. 1: Resolution tests from an impact into rubble-pile targets ($Y_0 = 0$ Pa, $f = 0.55$, $\phi_0 = 45\%$), resolved with 5.6×10^6 and 14.5×10^6 SPH particles. (a) Normalised ejected mass at speeds greater than v , as a function of normalised ejection speed, v/U . (b) Cumulative ejected momentum as a function of normalised vertical ejection velocity (in the $-y$ direction) for impacts into targets resolved with 5.6×10^6 and 14.5×10^6 SPH particles. The data were analysed at $T = 200$ seconds after the impact.



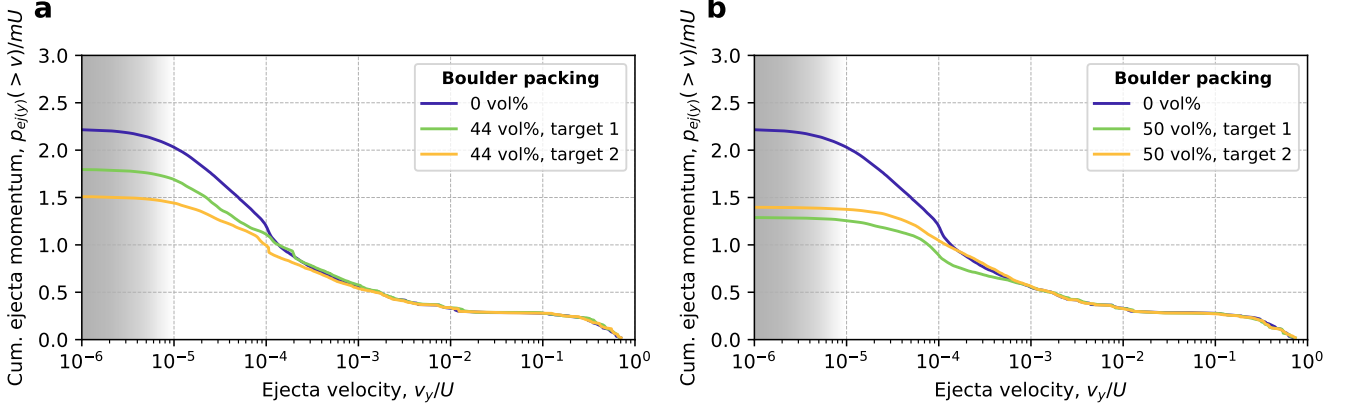
Supplementary Fig. 2: Resolution tests from an impact into rubble-pile targets ($Y_0 = 0$ Pa, $f = 0.55$, $\phi_0 = 45\%$), where the entire target was resolved with 5.6×10^6 and 14.5×10^6 SPH particles and from impacts into targets that had a reduced domain size ($\approx 15\%$ of the target in the y -direction) and was resolved by 5×10^6 and 10×10^6 . (a) Normalised ejected mass at speeds greater than v , as a function of normalised ejection speed, v/U . (b) Cumulative ejected momentum as a function of normalised vertical ejection velocity (in the $-y$ direction). The data were analysed at $T = 1$ second after the impact.



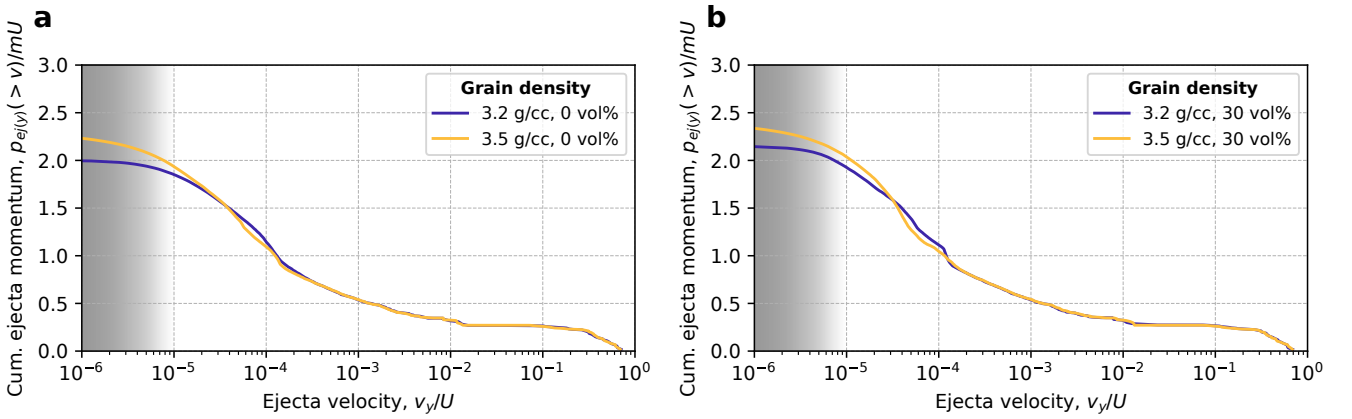
Supplementary Fig. 3: (a) Normalised ejected mass at speeds greater than v as a function of normalised ejection speed, v/U , for DART-like impacts at four different locations. (b) Cumulative ejected momentum as a function of normalised vertical ejection velocity (in the $+z$ direction for location 1 and in the $-y$ direction for locations 2-4). In all cases, the ejecta is analysed at $T \approx 30$ minutes after the impact. The shaded region shows the ejecta with velocities below the escape speed of Dimorphos, which do not contribute toward β .



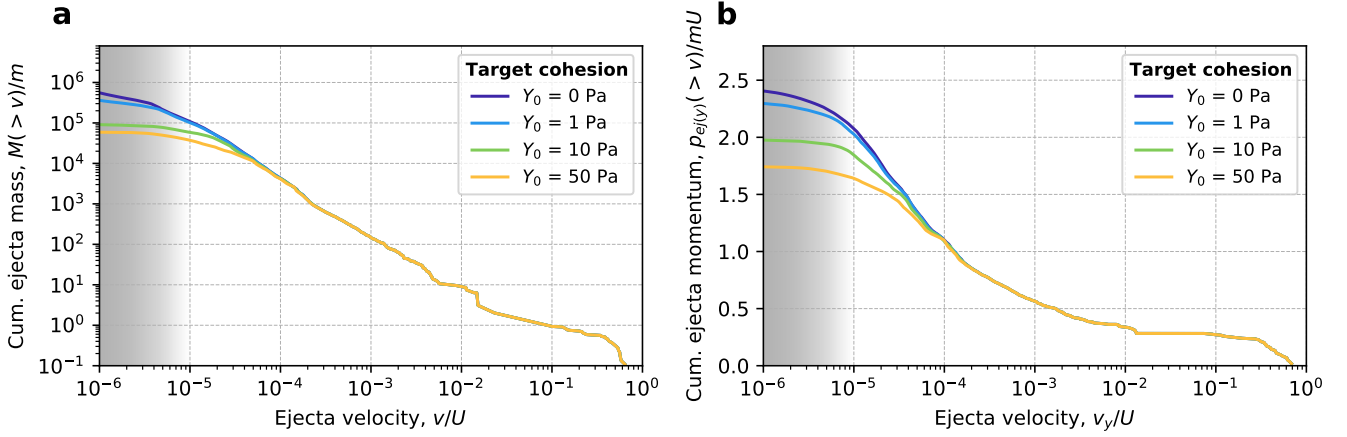
Supplementary Fig. 4: (a) Normalised ejected mass at speeds greater than v as a function of normalised ejection speed, v/U , for the DART impact into rubble-pile targets with boulder volume fractions between 0% (only the three boulders at the impact location) and 50 vol%. (b) Cumulative ejected momentum as a function of normalised vertical ejection velocity (in the $-y$ direction). In all cases, the ejecta is analysed at $T \approx 30$ minutes after the impact. The shaded region shows the ejecta with velocities below the escape speed of Dimorphos, which do not contribute toward β . The gradient is representative of the uncertainty in the escape speed calculation.



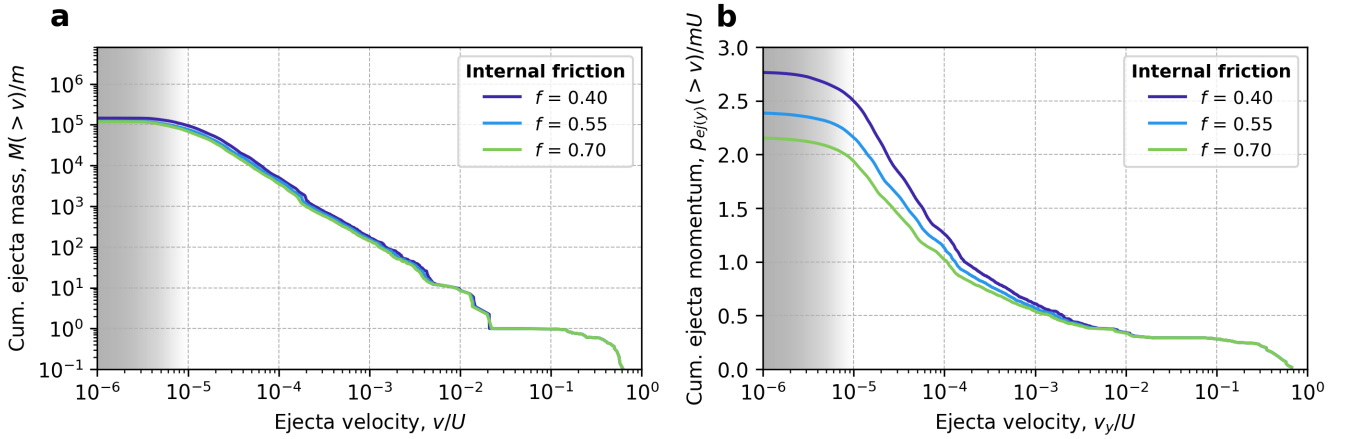
Supplementary Fig. 5: Cumulative ejected momentum as a function of normalised vertical ejection velocity (in the $-y$ direction) from impacts into (a) targets with 44 vol% boulder packing compared to a homogeneous target; (b) targets with 50 vol% boulder packing compared to a homogeneous target. In all cases, the ejecta is analysed at $T \approx 30$ minutes after the impact. The shaded region shows the ejecta with velocities below the escape speed of Dimorphos, which do not contribute toward β . The gradient is representative of the uncertainty in the escape speed calculation.



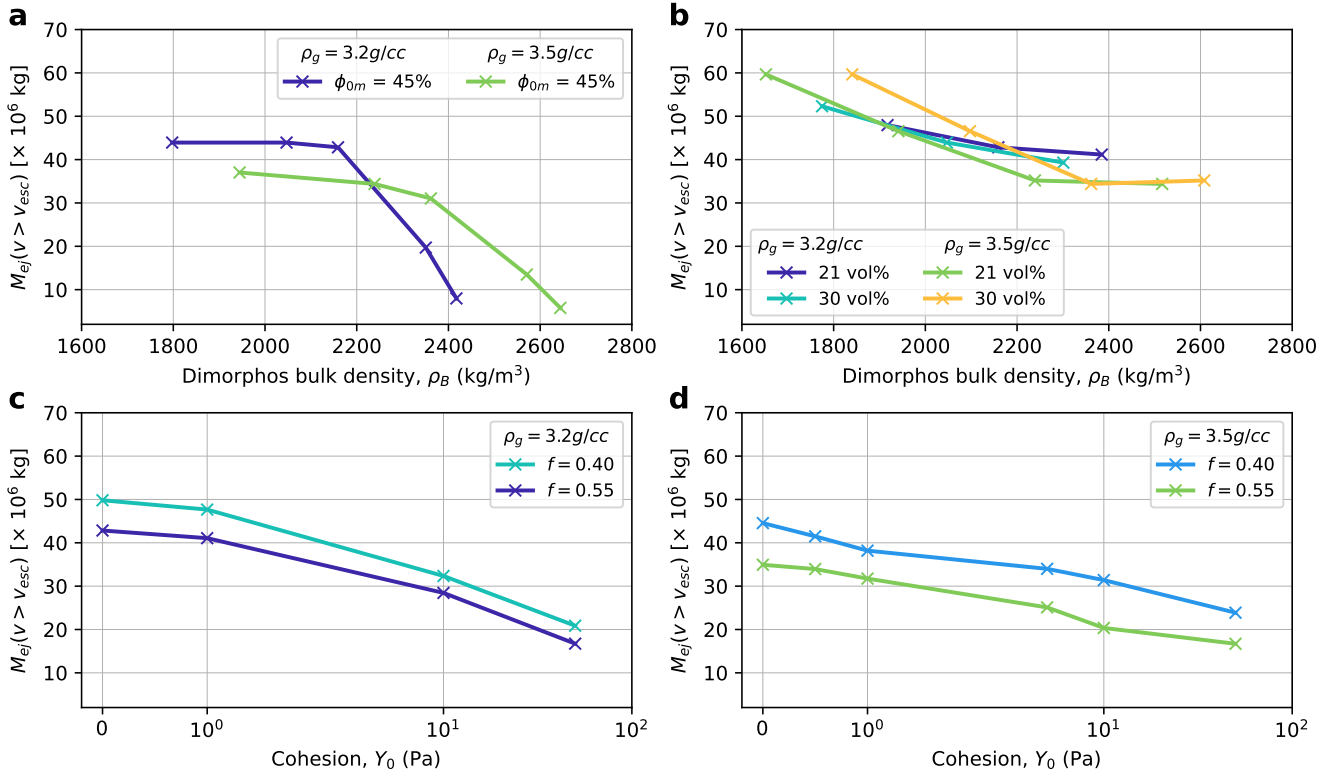
Supplementary Fig. 6: Cumulative ejected momentum as a function of normalised vertical ejection velocity (in the $-y$ direction) from impacts into (a) homogeneous targets (0 vol% occupied by boulders) and grain densities, $\rho_g = 3.2$ and 3.5 g/cc; (b) rubble-pile targets with 30 vol% occupied by boulders and $\rho_g = 3.2$ and 3.5 g/cc. The data is analysed at $T \approx 30$ minutes after the impact. The shaded region shows the ejecta with velocities below the escape speed of Dimorphos, which do not contribute toward β . The gradient is representative of the uncertainty in the escape speed calculation.



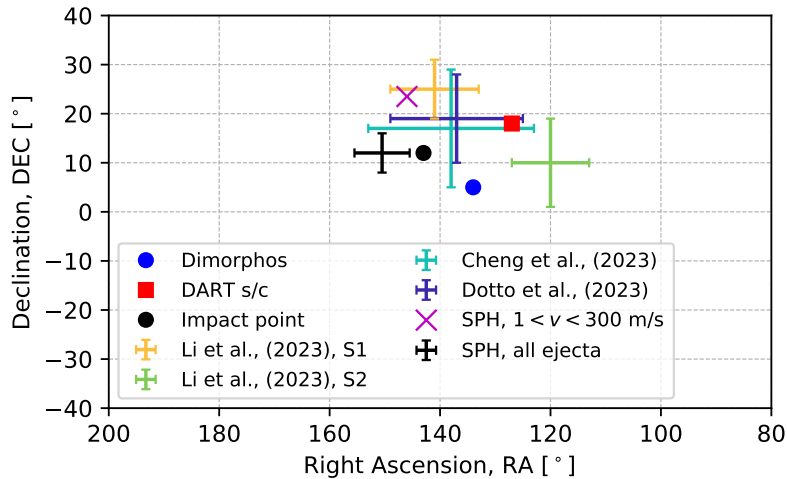
Supplementary Fig. 7: (a) Normalised ejected mass at speeds greater than v as a function of normalised ejection speed, v/U , for target matrix cohesions, Y_0 , between 0 and 50 Pa. (b) Cumulative ejected momentum as a function of normalised vertical ejection velocity (in the $-y$ direction). The shaded region shows the ejecta with velocities below the escape speed of Dimorphos, which do not contribute toward β . The gradient is representative of the uncertainty in the escape speed calculation.



Supplementary Fig. 8: (a) Normalised ejected mass at speeds greater than v as a function of normalised ejection speed, v/U , for target matrix coefficient of internal frictions, f between 0.4 and 0.7. (b) Cumulative ejected momentum as a function of normalised vertical ejection velocity (in the $-y$ direction). The shaded region shows the ejecta with velocities below the escape speed of Dimorphos, which do not contribute toward β . The gradient is representative of the uncertainty in the escape speed calculation.



Supplementary Fig. 9: Ejecta mass from SPH simulations. (a) Ejecta mass, $M_{ej}(v > v_{esc})$, as a function of Dimorphos' bulk density, ρ_B , for Dimorphos-like targets with boulder volume fractions ranging from 0 vol% (no boulders) to 50 vol%. (b) $M_{ej}(v > v_{esc})$ as a function of bulk density, ρ_B , for Dimorphos-like targets with varying matrix porosity, between 35 and 65%. ρ_B is calculated for a fixed volume of 0.00181 km³. (c) $M_{ej}(v > v_{esc})$ as a function of cohesion (Y_0) for the DART impact into targets with $f = 0.4$ and 0.55. (d) $M_{ej}(v > v_{esc})$ as a function of cohesion (Y_0) for the DART impact into targets with $f = 0.4$ and 0.55.



Supplementary Fig. 10: Ejecta cone orientation as derived from the HST data [$141 \pm 8^\circ$, $25 \pm 6^\circ$; $120 \pm 9^\circ$, $10 \pm 7^\circ$ Li2023], the LICIACube data [$137 \pm 9^\circ$, $19 \pm 12^\circ$ Dotto2023] and both [$138 \pm 15^\circ$, $+13 \pm 15^\circ$ Cheng2023], compared to cone orientation derived from SPH simulations for ejecta with velocities between 1 and 300 m/s and for the entire range of ejecta [$150.5 \pm 4^\circ$, $12 \pm 5^\circ$; 1- σ uncertainty]. The blue dot shows Dimorphos's velocity vector [134° , $+5^\circ$], the red square is the direction of the incoming DART trajectory [128° , $+18^\circ$] and the black dot shows the impact point at [143° , $+12^\circ$].