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Constraining CO coverage on copper promotes high-efficiency ethylene electroproduction

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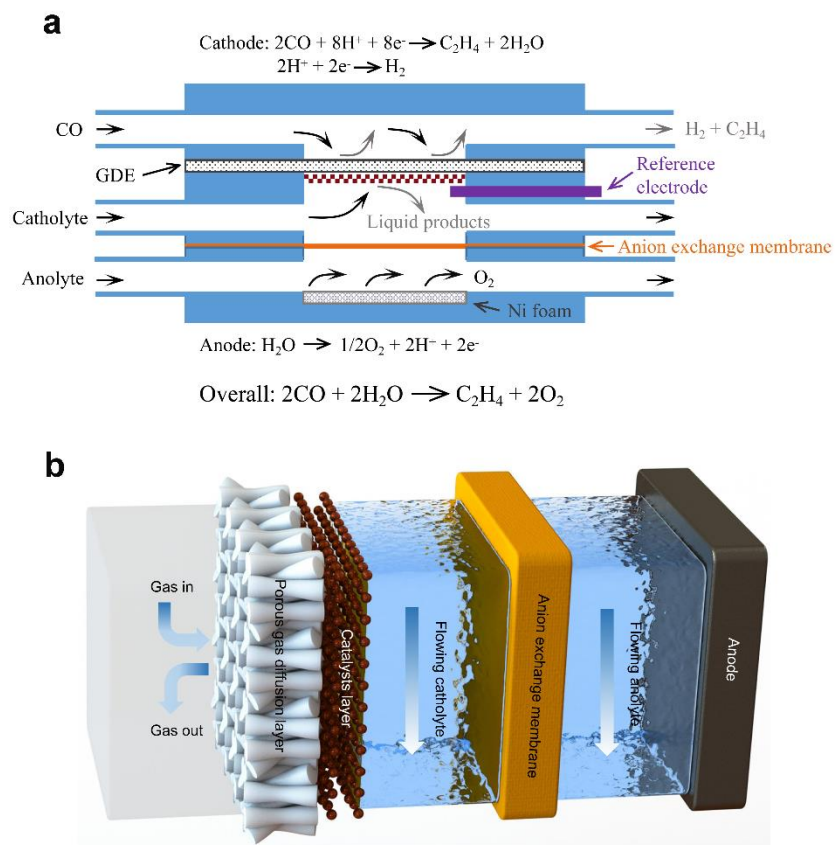
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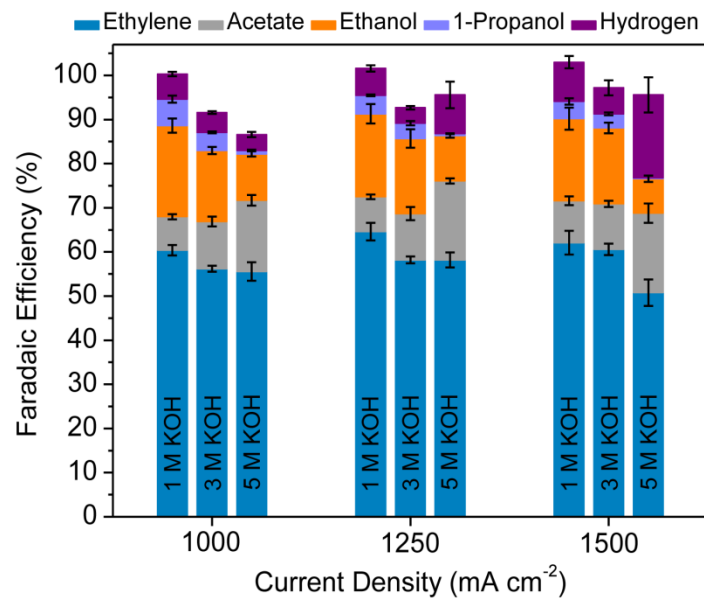
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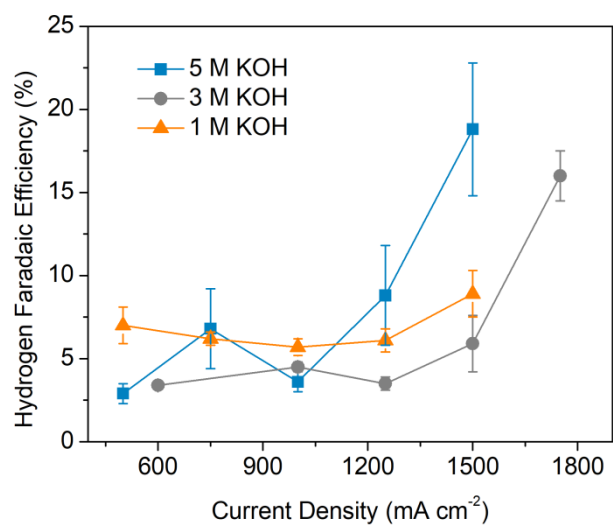
^{*}*Corresponding email: ted.sargent@utoronto.ca; sinton@mie.utoronto.ca*



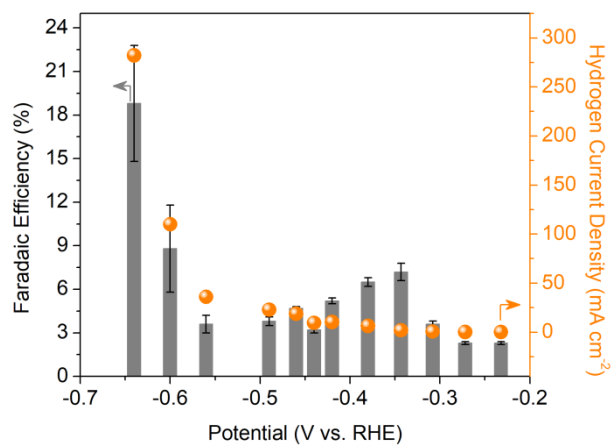
Supplementary Fig. 1. Schematic illustrations of flow cell electrolyzer. a, A two-dimensional cross-section view. **b,** A three-dimensional layout.



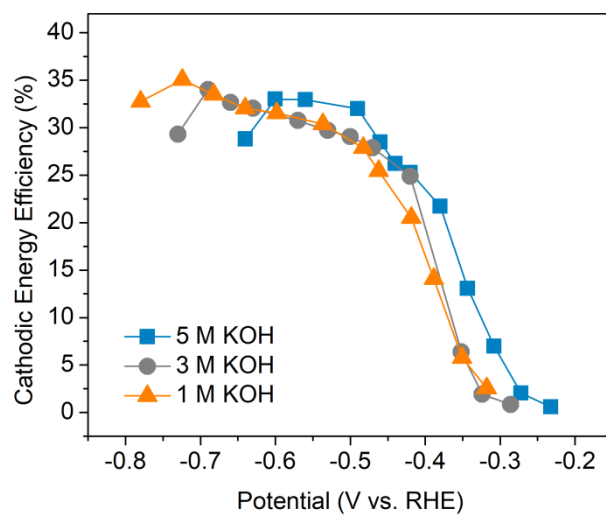
Supplementary Fig. 2. Faradaic efficiencies of all products from CO reduction in 1 M, 3 M and 5 M KOH at selected current densities. Error bars are means $\pm$ SD (n = 3 replicates).



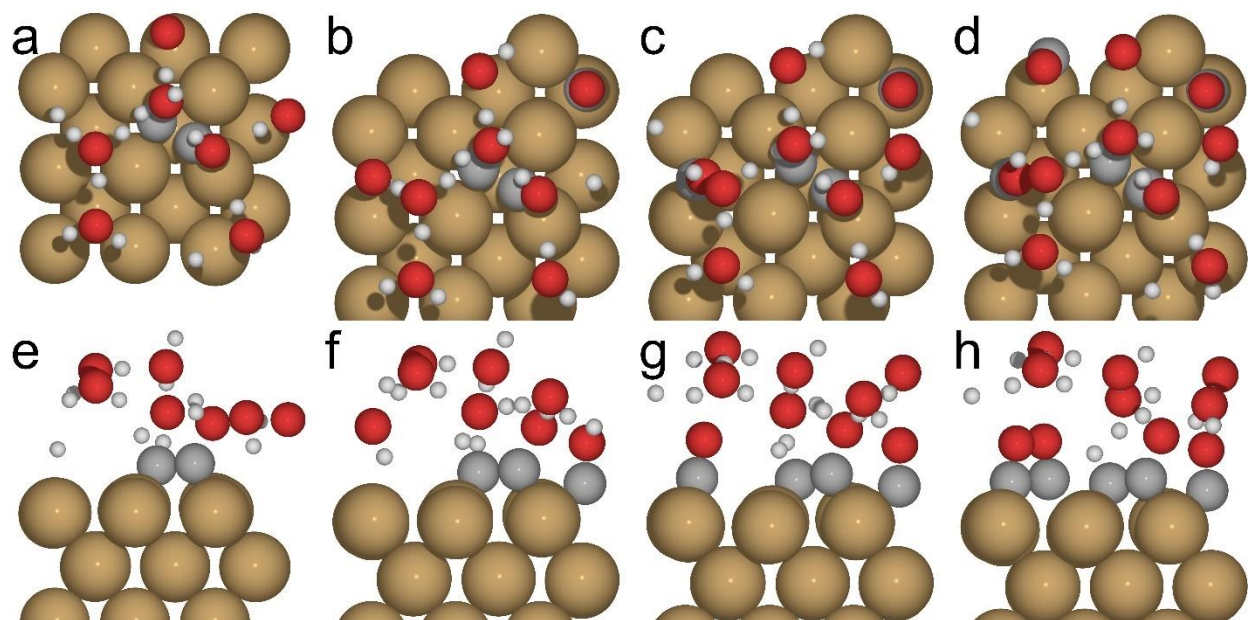
Supplementary Fig. 3. Hydrogen Faradaic efficiencies at various KOH concentrations as a function of applied current density. Error bars are means $\pm$ SD (n = 3 replicates).



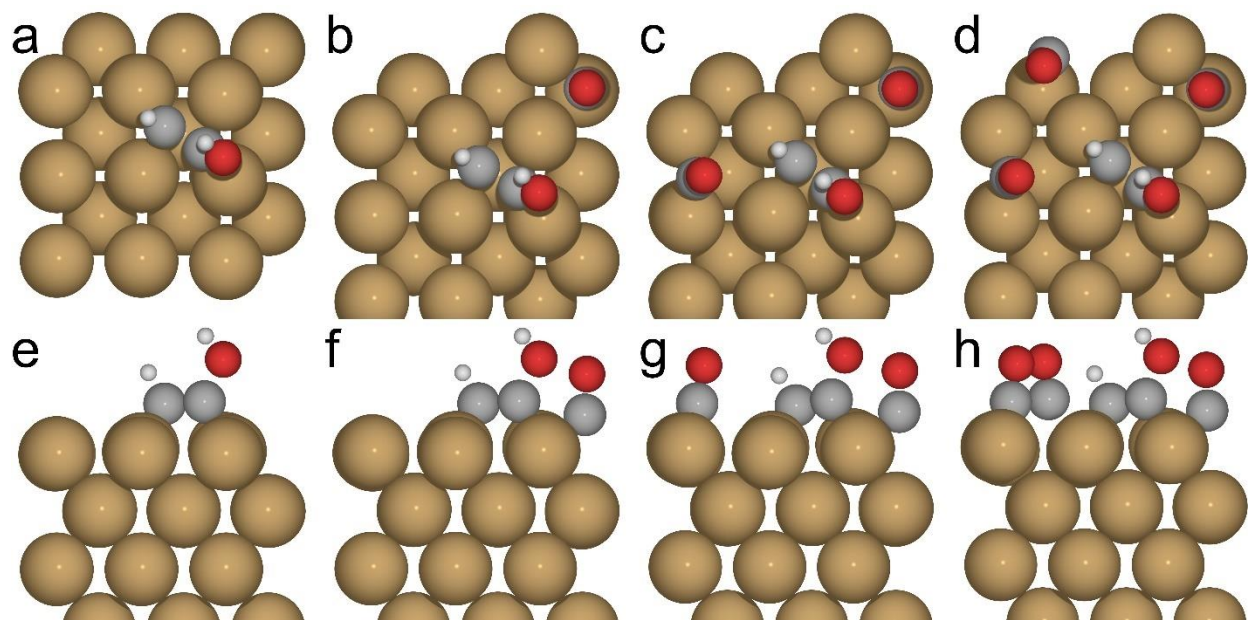
Supplementary Fig. 4. Hydrogen Faradaic efficiency and partial current density from CO reduction in 5 M KOH as a function of applied potential. Error bars are means $\pm$ SD ($n = 3$ replicates).



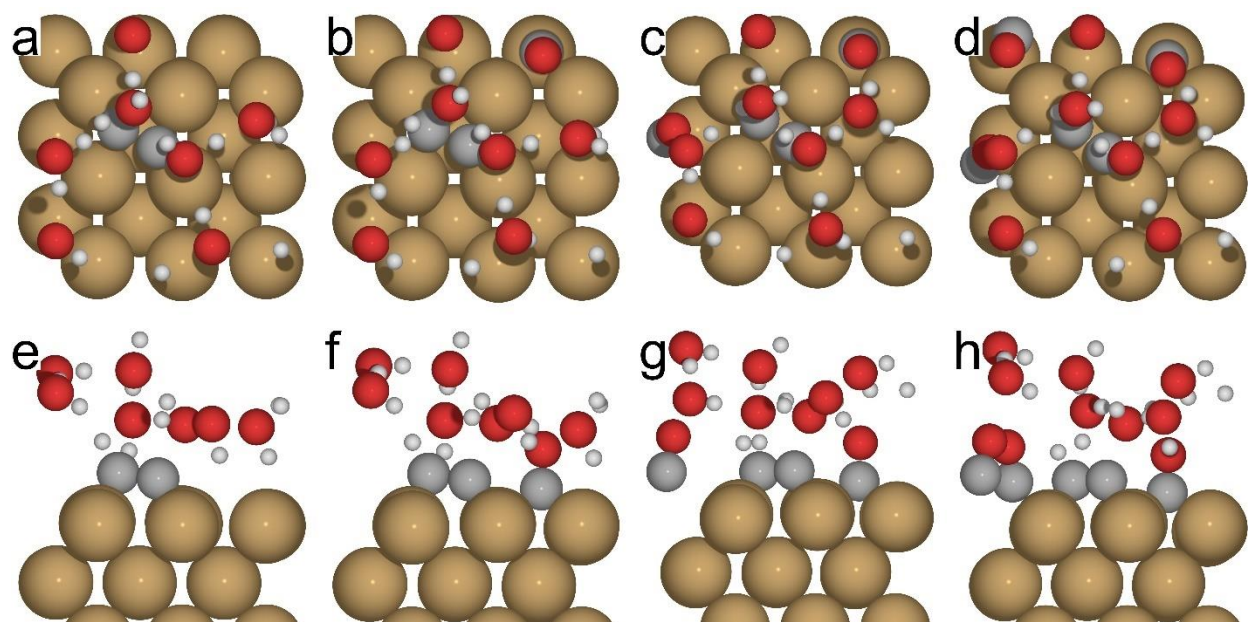
Supplementary Fig. 5. Cathodic energy efficiencies for ethylene electroproduction from CO reduction at various KOH concentrations as a function of applied potential.



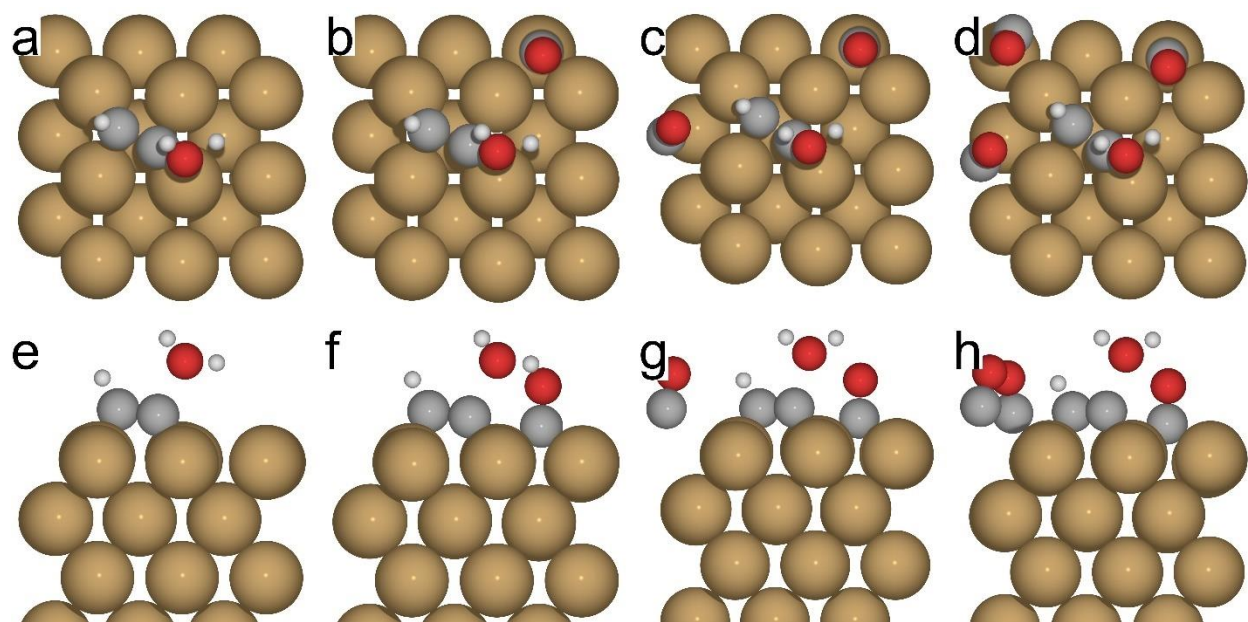
Supplementary Fig. 6. The geometries of key intermediates branching ethylene and ethanol, $^*\text{CHCOH}$, on Cu(100) with solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at $1/9$ ML, **c** and **g** at $2/9$ ML, **d** and **h** at $3/9$ ML. Yellow, red, grey, and white balls stand for copper, oxygen, carbon, and hydrogen atoms, respectively. These notations are used throughout this document.



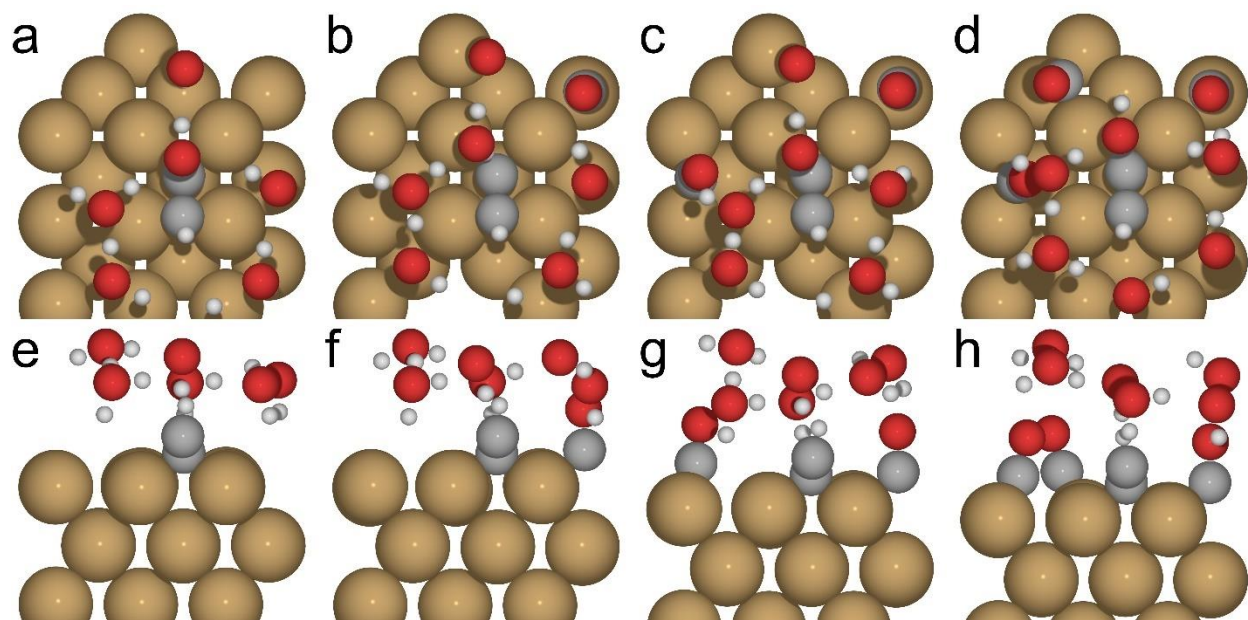
Supplementary Fig. 7. The geometries of key intermediates branching ethylene and ethanol, $^*\text{CHCOH}$, on Cu(100) without solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at 1/9 ML, **c** and **g** at 2/9 ML, **d** and **h** at 3/9 ML.



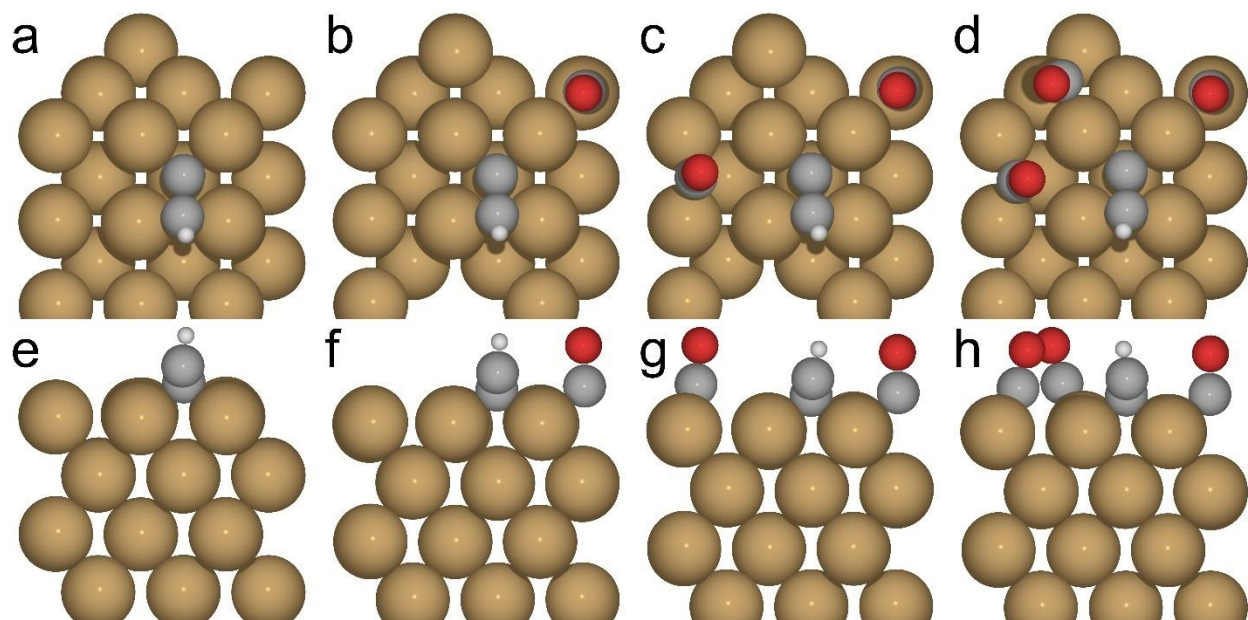
Supplementary Fig. 8. The transition state geometries of *CHCOH dehydroxylation to *CCH on $\text{Cu}(100)$ with solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at 1/9 ML, **c** and **g** at 2/9 ML, **d** and **h** at 3/9 ML.



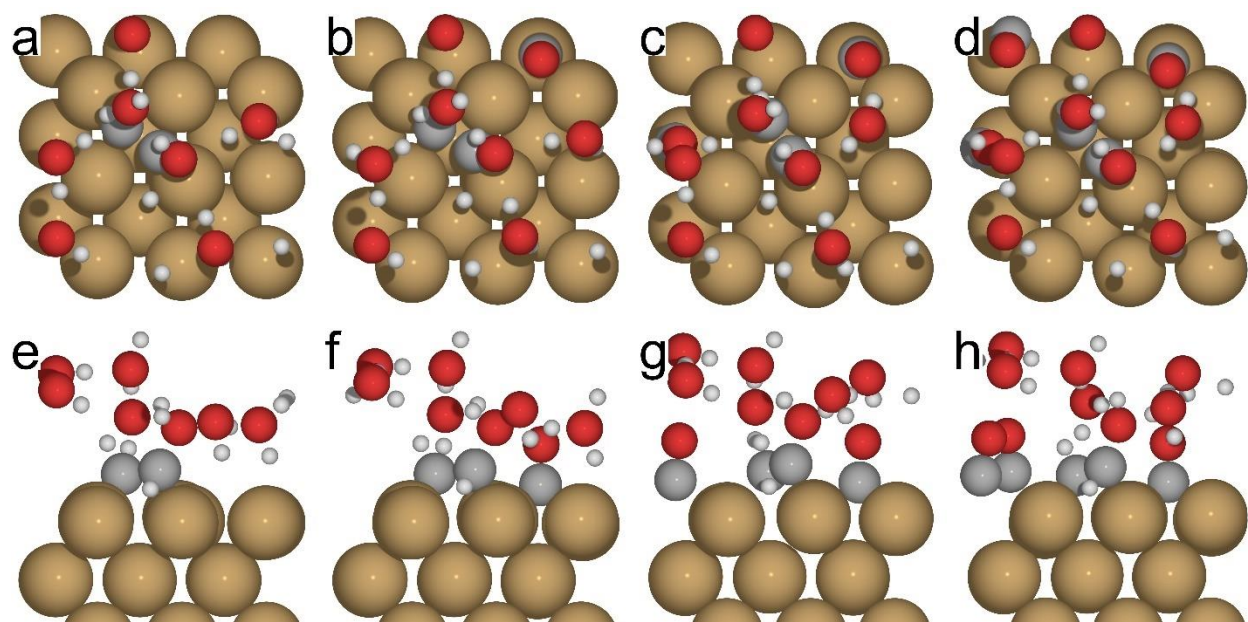
Supplementary Fig. 9. The transition state geometries of *CHCOH dehydroxylation to *CCH on $\text{Cu}(100)$ without solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at 1/9 ML, **c** and **g** at 2/9 ML, **d** and **h** at 3/9 ML.



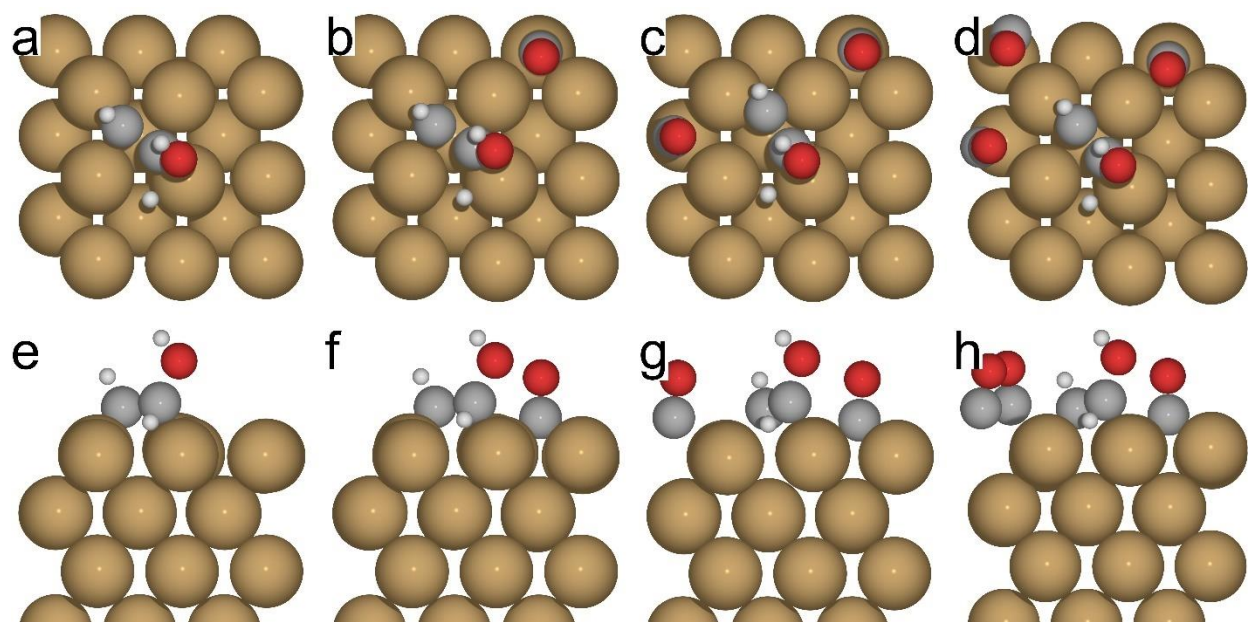
Supplementary Fig. 10. The final state geometries of $*CHCOH$ dehydroxylation to $*CCH$ on Cu(100) with solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at $1/9$ ML, **c** and **g** at $2/9$ ML, **d** and **h** at $3/9$ ML.



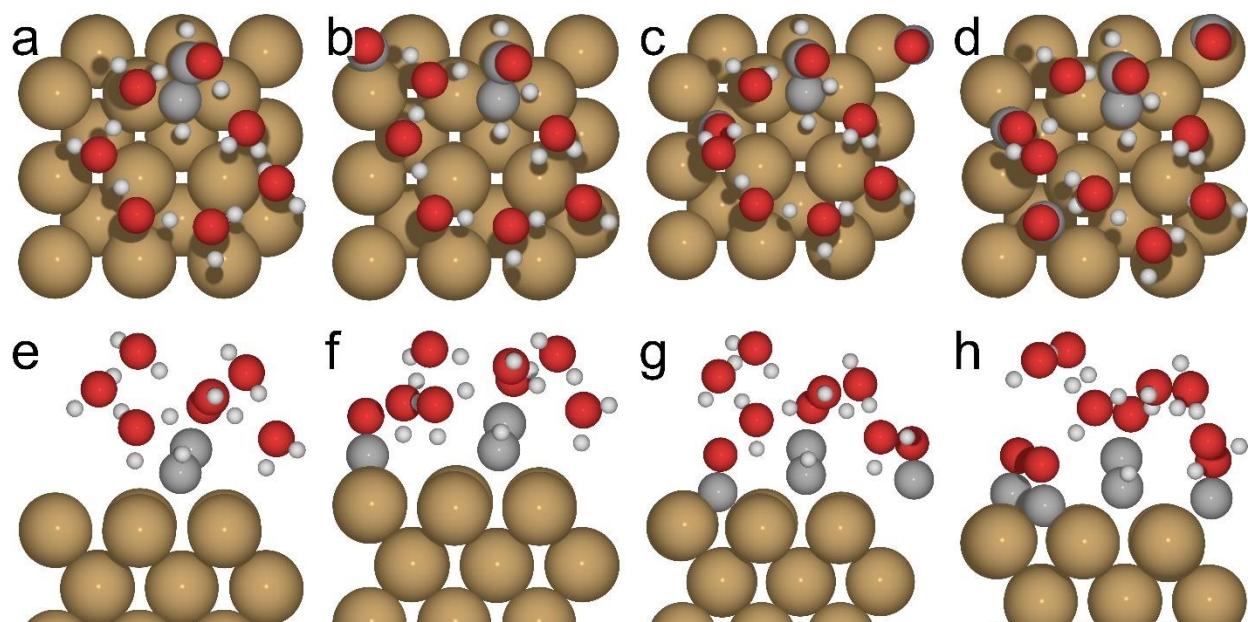
Supplementary Fig. 11. The final state geometries of $^*\text{CHCOH}$ dehydroxylation to $^*\text{CCH}$ on Cu(100) without solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at 1/9 ML, **c** and **g** at 2/9 ML, **d** and **h** at 3/9 ML.



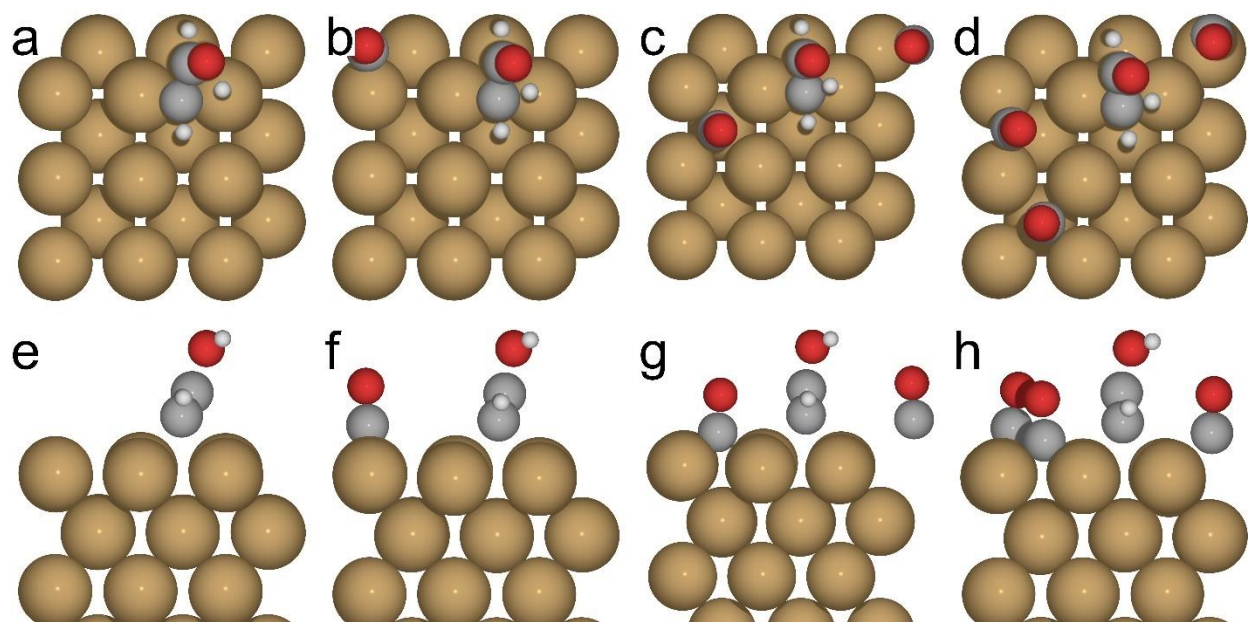
Supplementary Fig. 12. The transition state geometries of *CHCOH hydrogenation to *CHCHOH on Cu(100) with solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at 1/9 ML, **c** and **g** at 2/9 ML, **d** and **h** at 3/9 ML.



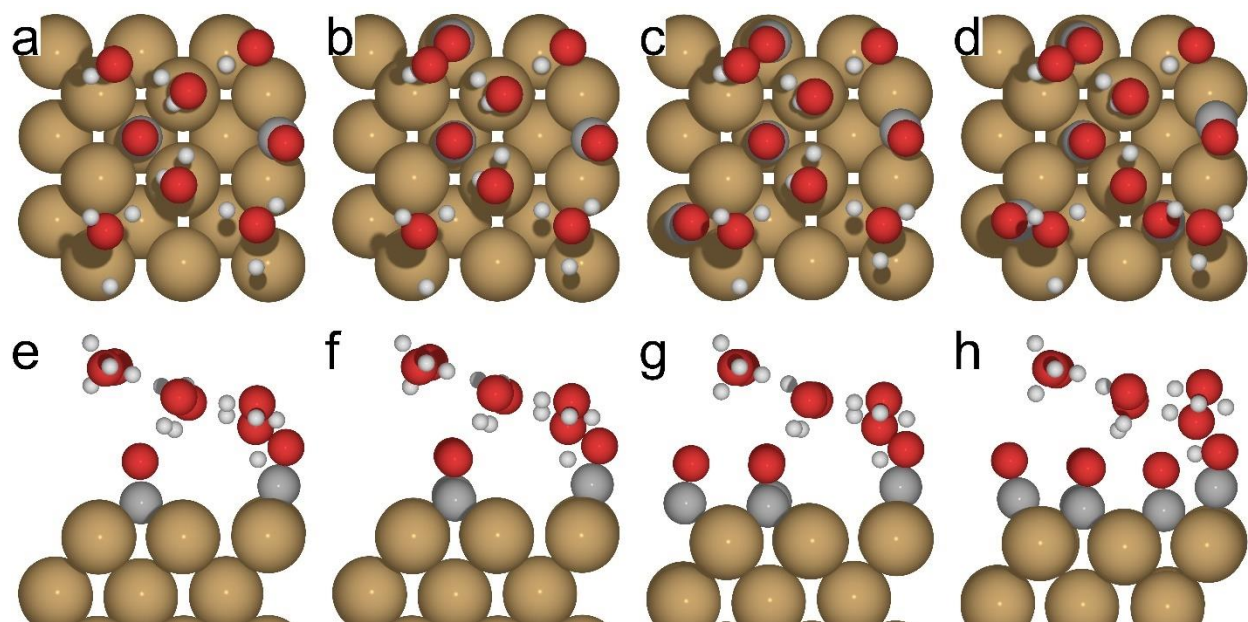
Supplementary Fig. 13. The transition state geometries of $^*\text{CHCOH}$ hydrogenation to $^*\text{CHCHOH}$ on Cu(100) without solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at 1/9 ML, **c** and **g** at 2/9 ML, **d** and **h** at 3/9 ML.



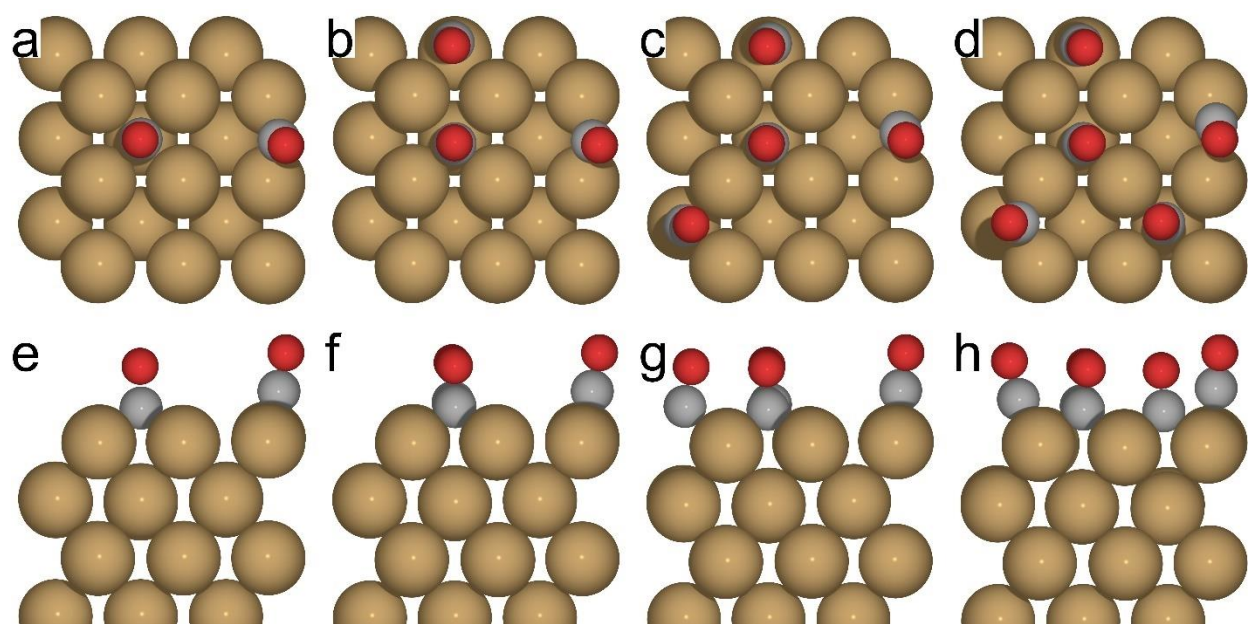
Supplementary Fig. 14. The final state geometries of $^*\text{CHCOH}$ hydrogenation to $^*\text{CHCHOH}$ on Cu(100) with solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at 1/9 ML, **c** and **g** at 2/9 ML, **d** and **h** at 3/9 ML.



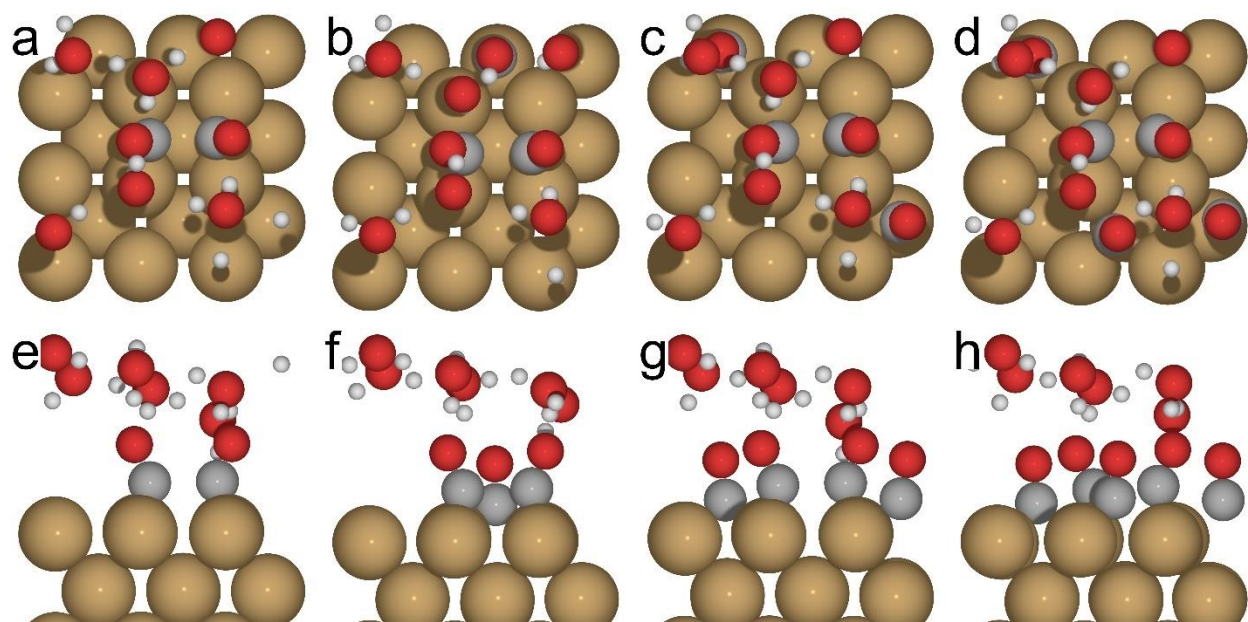
Supplementary Fig. 15. The final state geometries of $^*\text{CHCOH}$ hydrogenation to $^*\text{CHCHOH}$ on Cu(100) without solvent molecules at different CO coverage: **a** and **e** at 0 ML, **b** and **f** at 1/9 ML, **c** and **g** at 2/9 ML, **d** and **h** at 3/9 ML.



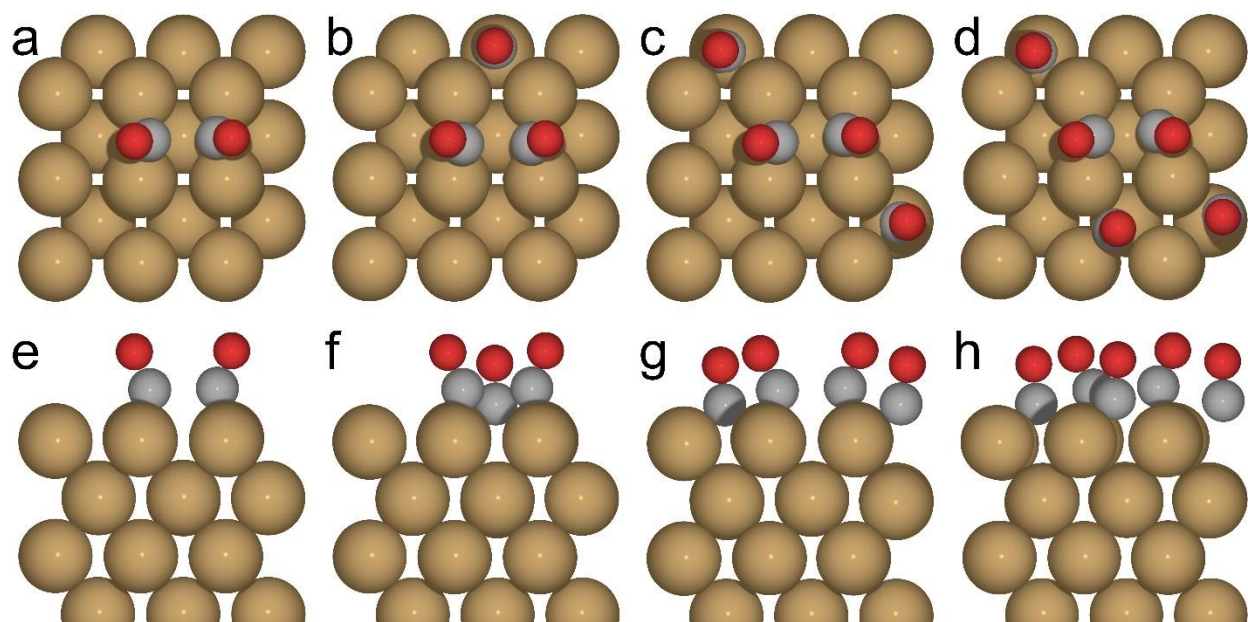
Supplementary Fig. 16. The initial state geometries of CO dimerization on Cu(100) with solvent molecules at different CO coverage: **a** and **e** at 2/9 ML, **b** and **f** at 3/9 ML, **c** and **g** at 4/9 ML, **d** and **h** at 5/9 ML.



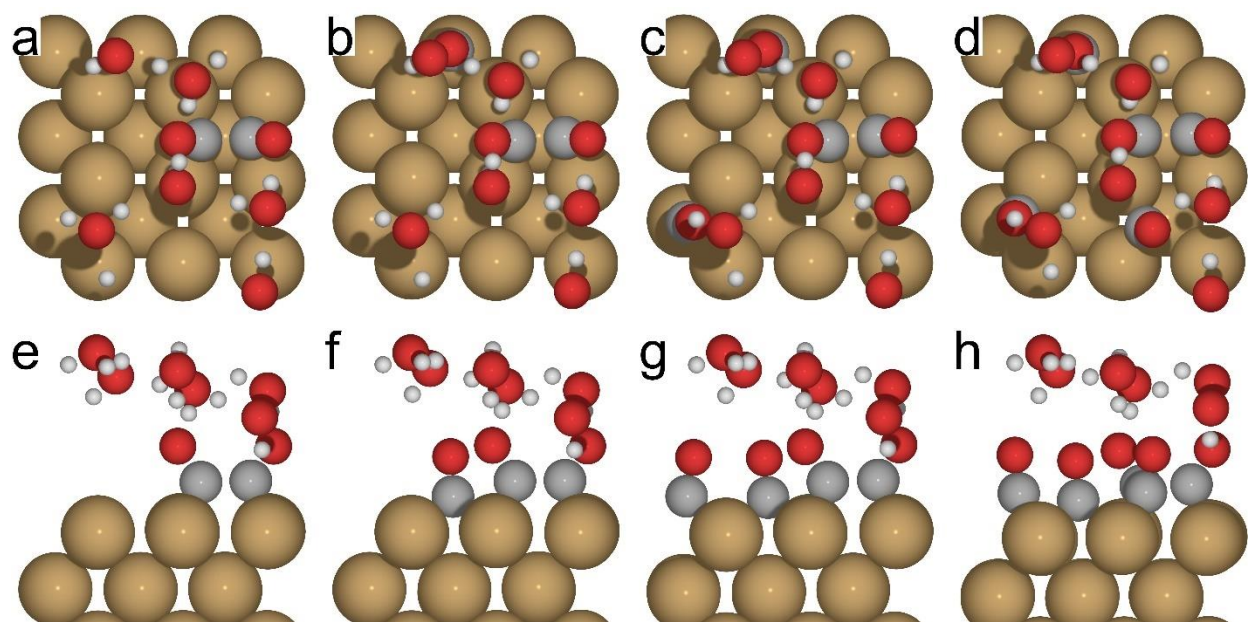
Supplementary Fig. 17. The initial state geometries of CO dimerization on Cu(100) without solvent molecules at different CO coverage: **a** and **e** at 2/9 ML, **b** and **f** at 3/9 ML, **c** and **g** at 4/9 ML, **d** and **h** at 5/9 ML.



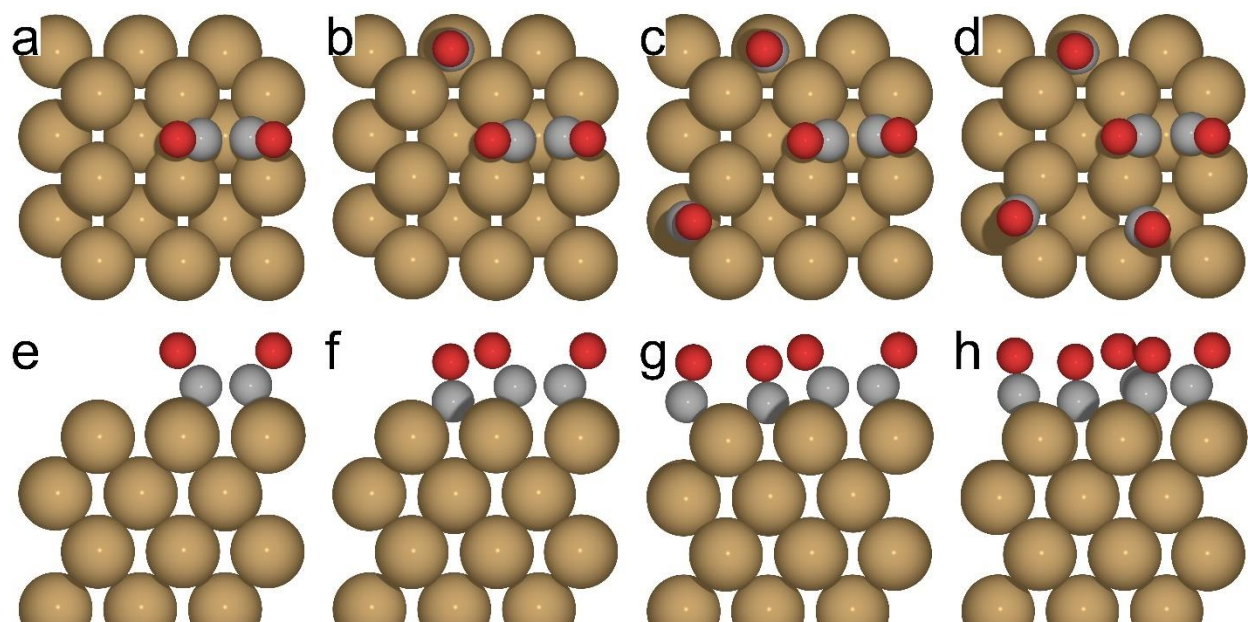
Supplementary Fig. 18. The transition state geometries of CO dimerization on Cu(100) with solvent molecules at different CO coverage: **a** and **e** at 2/9 ML, **b** and **f** at 3/9 ML, **c** and **g** at 4/9 ML, **d** and **h** at 5/9 ML.



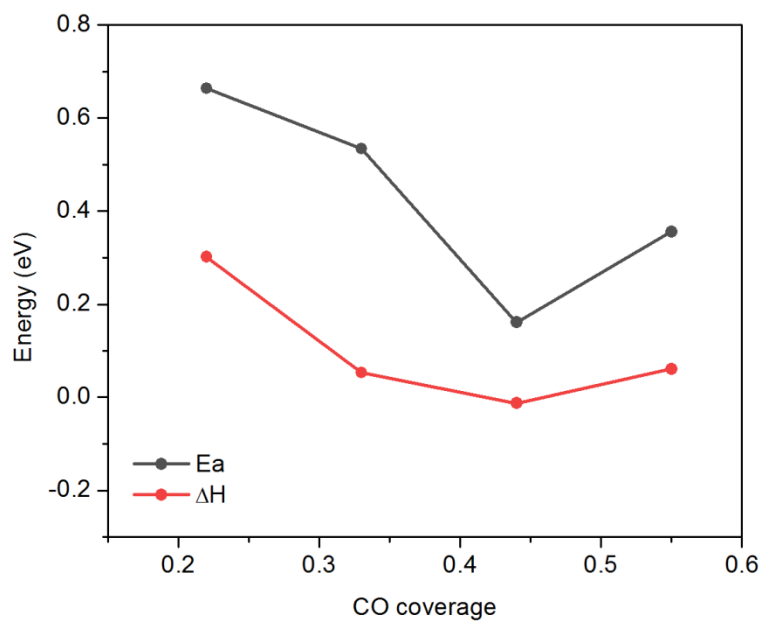
Supplementary Fig. 19. The transition state geometries of CO dimerization on Cu(100) without solvent molecules at different CO coverage: **a** and **e** at 2/9 ML, **b** and **f** at 3/9 ML, **c** and **g** at 4/9 ML, **d** and **h** at 5/9 ML.



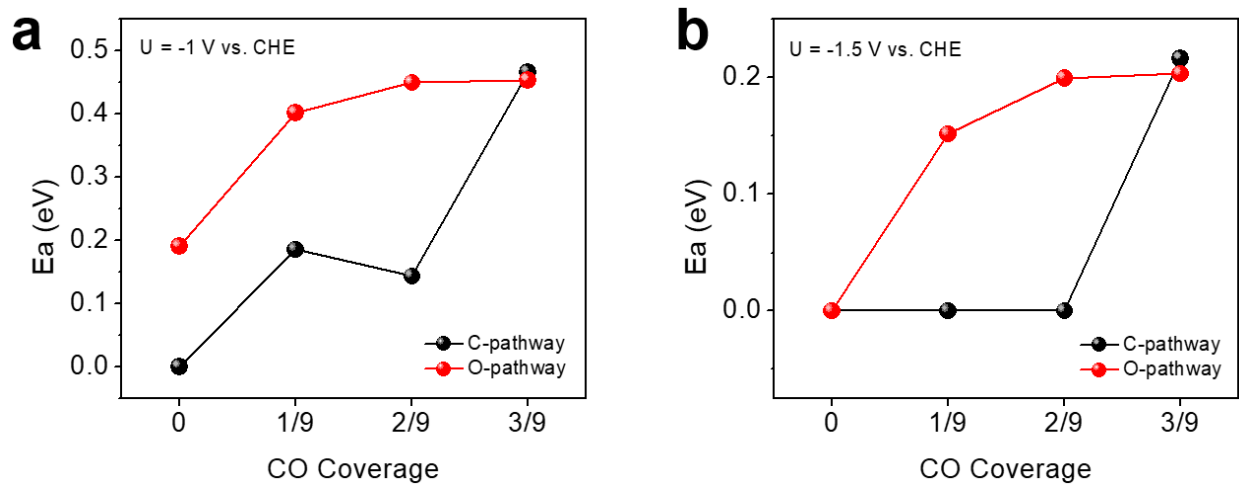
Supplementary Fig. 20. The final state geometries of CO dimerization on Cu(100) with solvent molecules at different CO coverage: **a** and **e** at $2/9$ ML, **b** and **f** at $3/9$ ML, **c** and **g** at $4/9$ ML, **d** and **h** at $5/9$ ML.



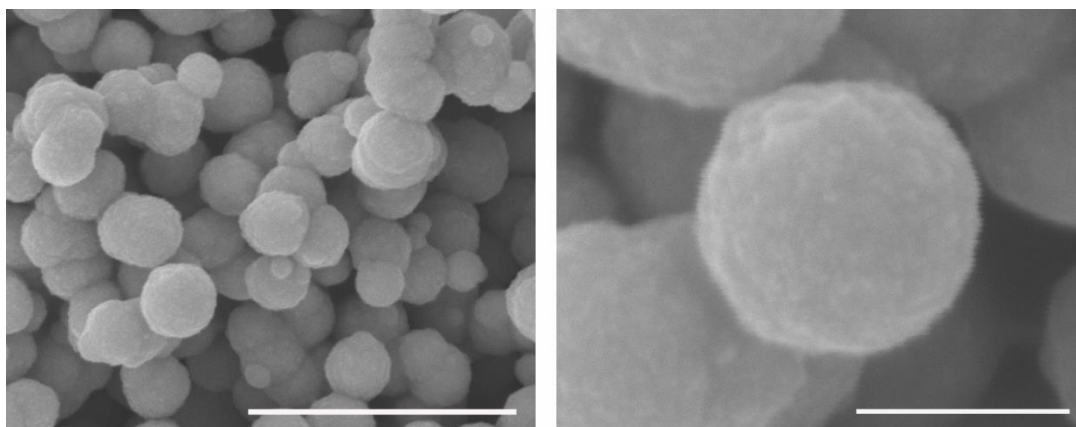
Supplementary Fig. 21. The final state geometries of CO dimerization on Cu(100) without solvent molecules at different CO coverage: **a** and **e** at 2/9 ML, **b** and **f** at 3/9 ML, **c** and **g** at 4/9 ML, **d** and **h** at 5/9 ML.



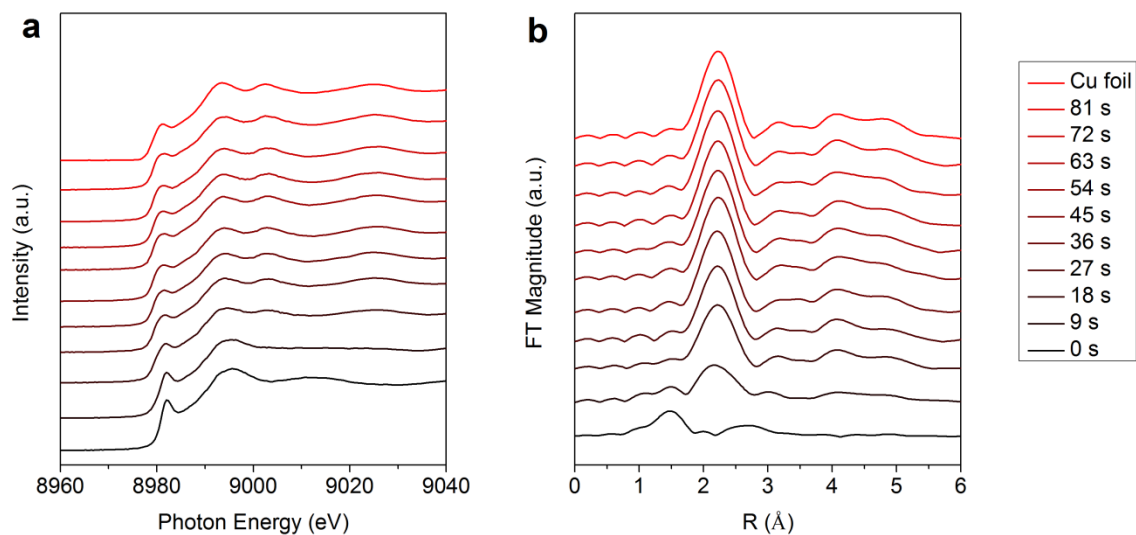
Supplementary Fig. 22. The reaction barrier and enthalpy change of CO dimerization on Cu(100) at different CO coverage.



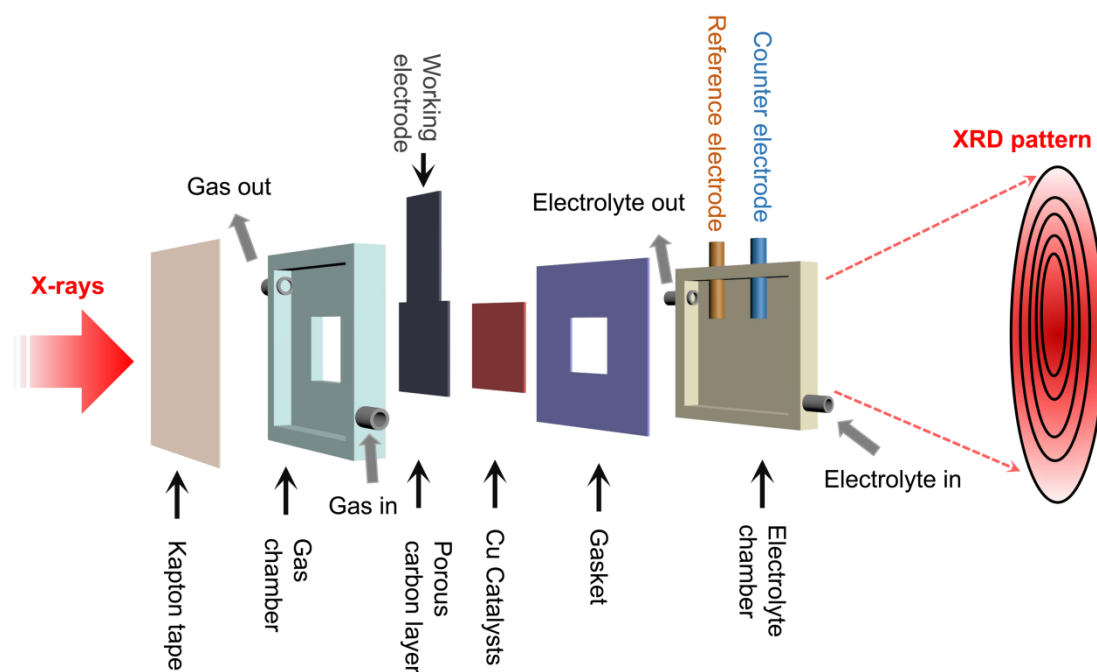
Supplementary Fig. 23. a, b, Activation energy as a function of coverage for the C- and O-pathways, at -1 V (**a**) and -1.5 V (**b**) versus the computational hydrogen electrode (CHE = SHE).



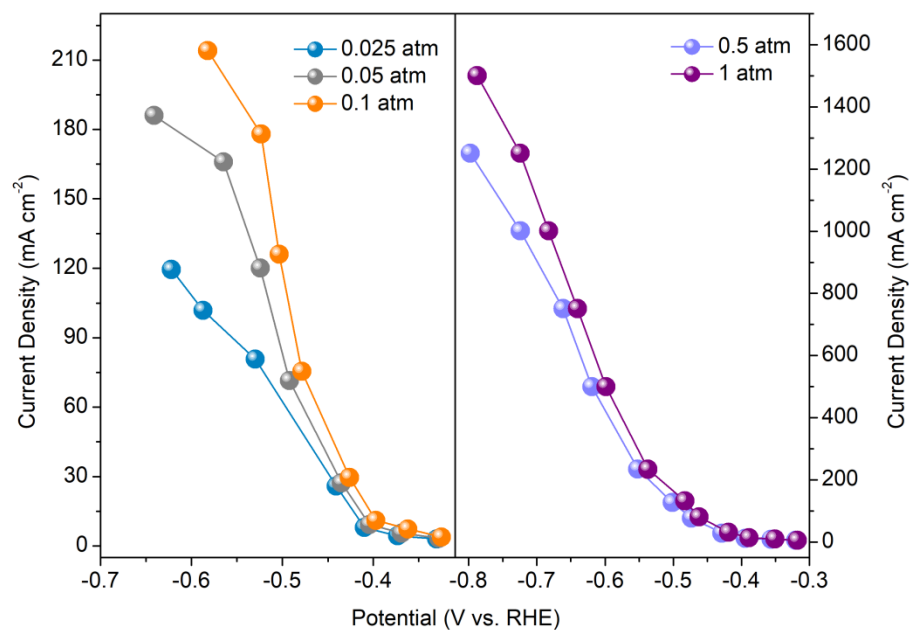
Supplementary Fig. 24. SEM images of oxide pre-catalysts. The scale bars are 1 μm on the left and 200 nm on the right.



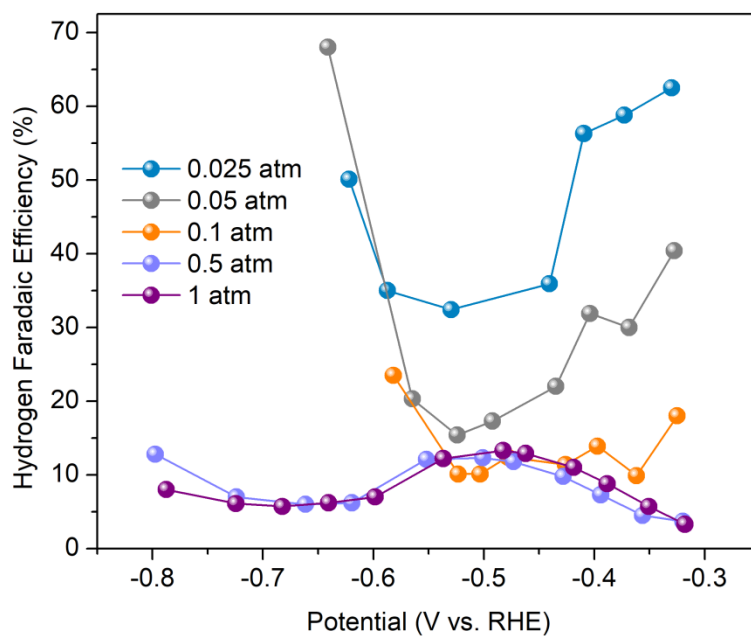
Supplementary Fig. 25. Operando X-ray absorption spectroscopy (XAS) analysis. **a**, A real-time Cu K-edge XAS tracking of the oxide reduction process. Each spectrum was collected at a time scale of 9 s. **b**, A Fourier Transform (FT) process of XAS spectra in (a). Ex-situ Cu foil spectra are included for comparison. The oxide reduction completes in ~1 min during CORR in 1 M KOH with the application of a constant current density of 120 mA cm^{-2} .



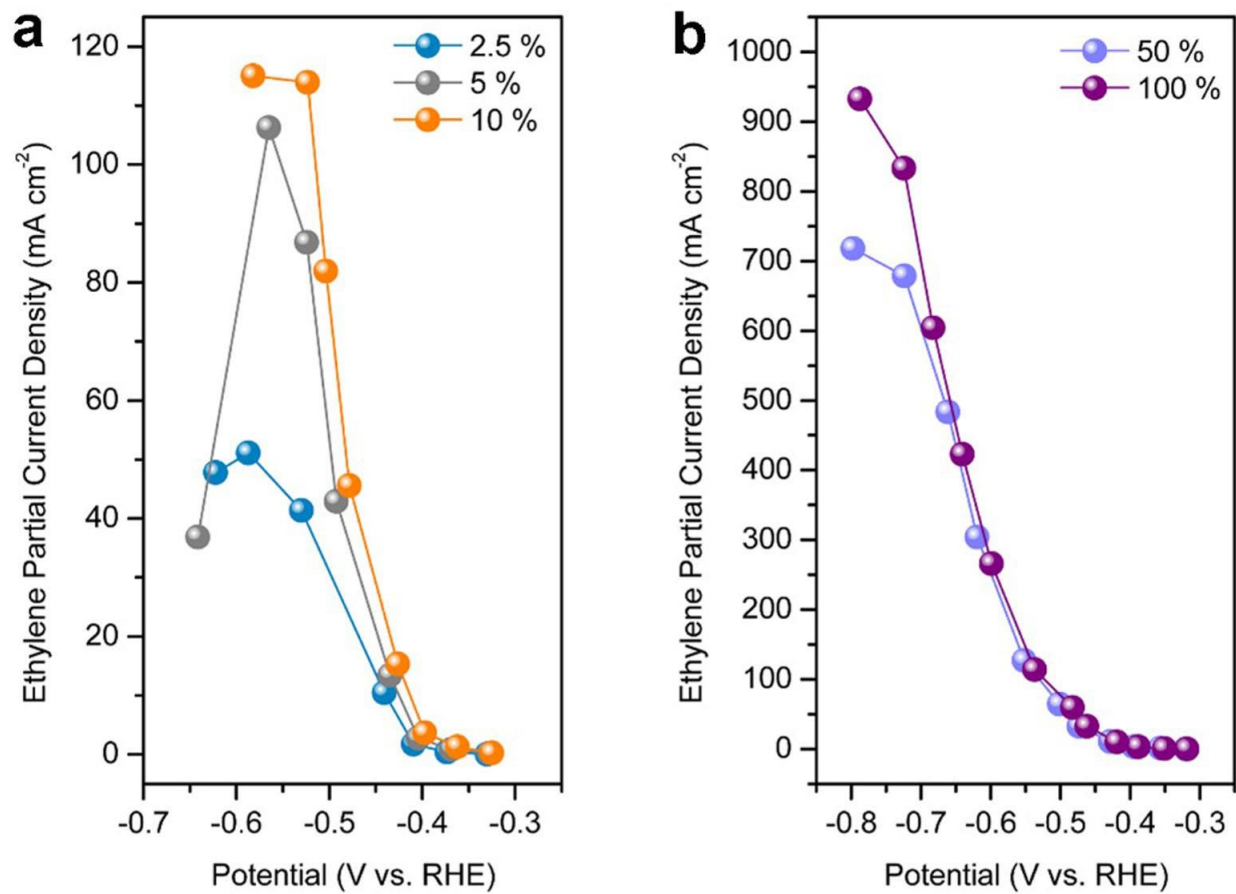
Supplementary Fig. 26. A schematic view of a flow cell design for high-resolution in operando X-ray diffraction test.



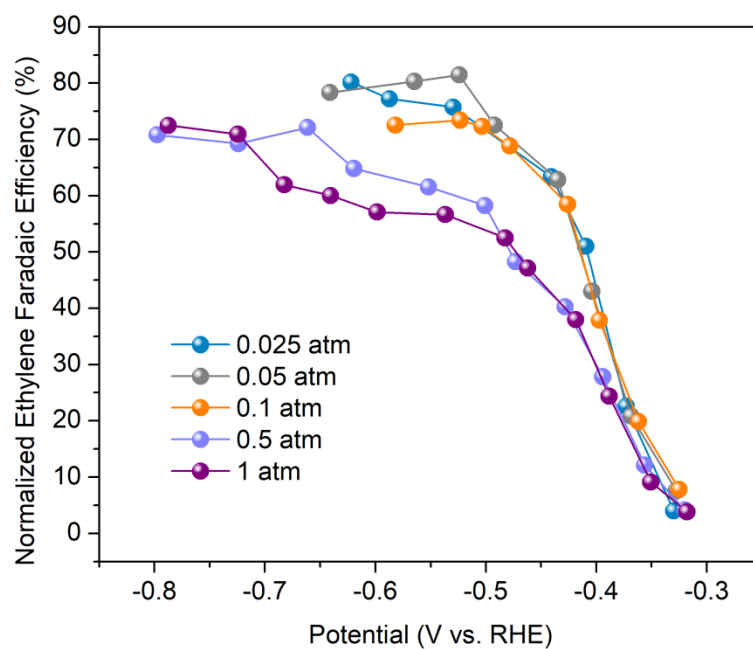
Supplementary Fig. 27. Total current densities of CORR at various CO pressures as a function of applied potential in 1 M KOH.



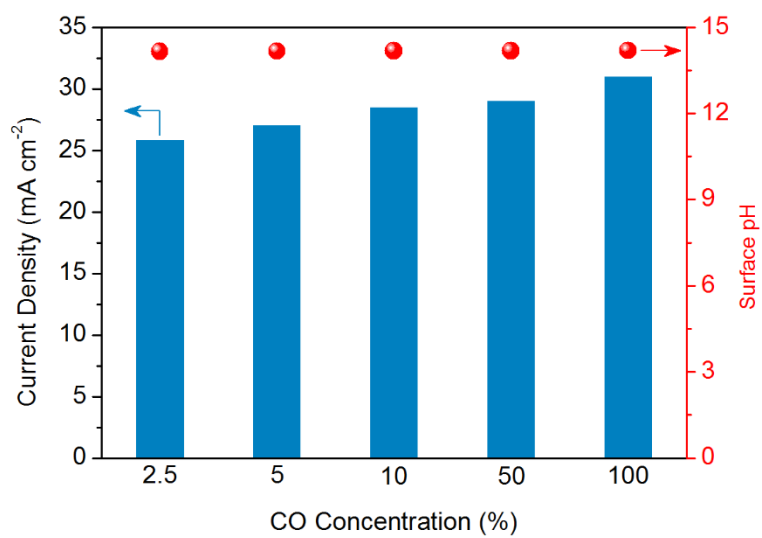
Supplementary Fig. 28. Hydrogen Faradaic efficiencies at various CO pressures as a function of applied potential in 1 M KOH.



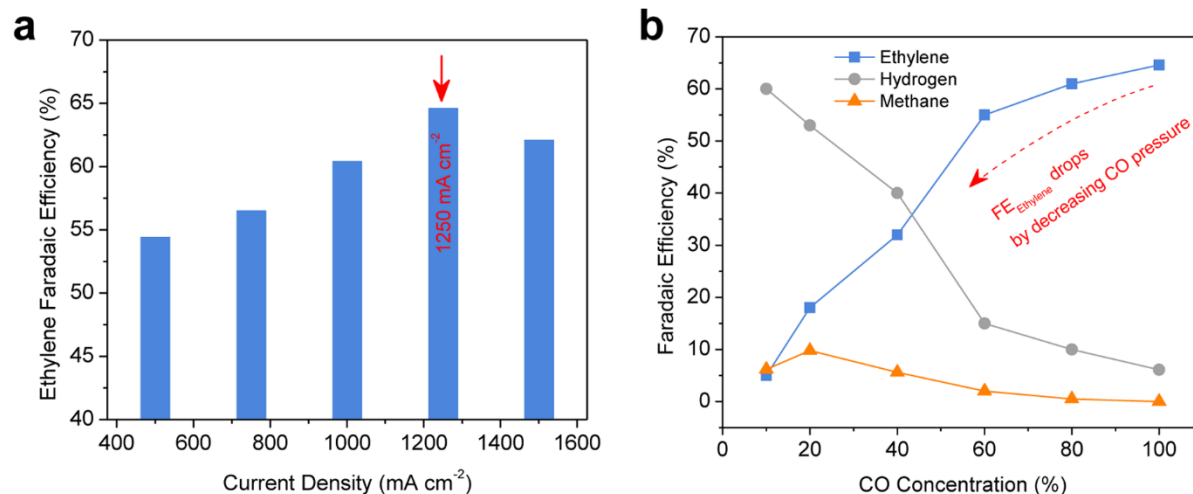
Supplementary Fig. 29. Ethylene partial current densities at various CO pressures as a function of applied potential in 1 M KOH.



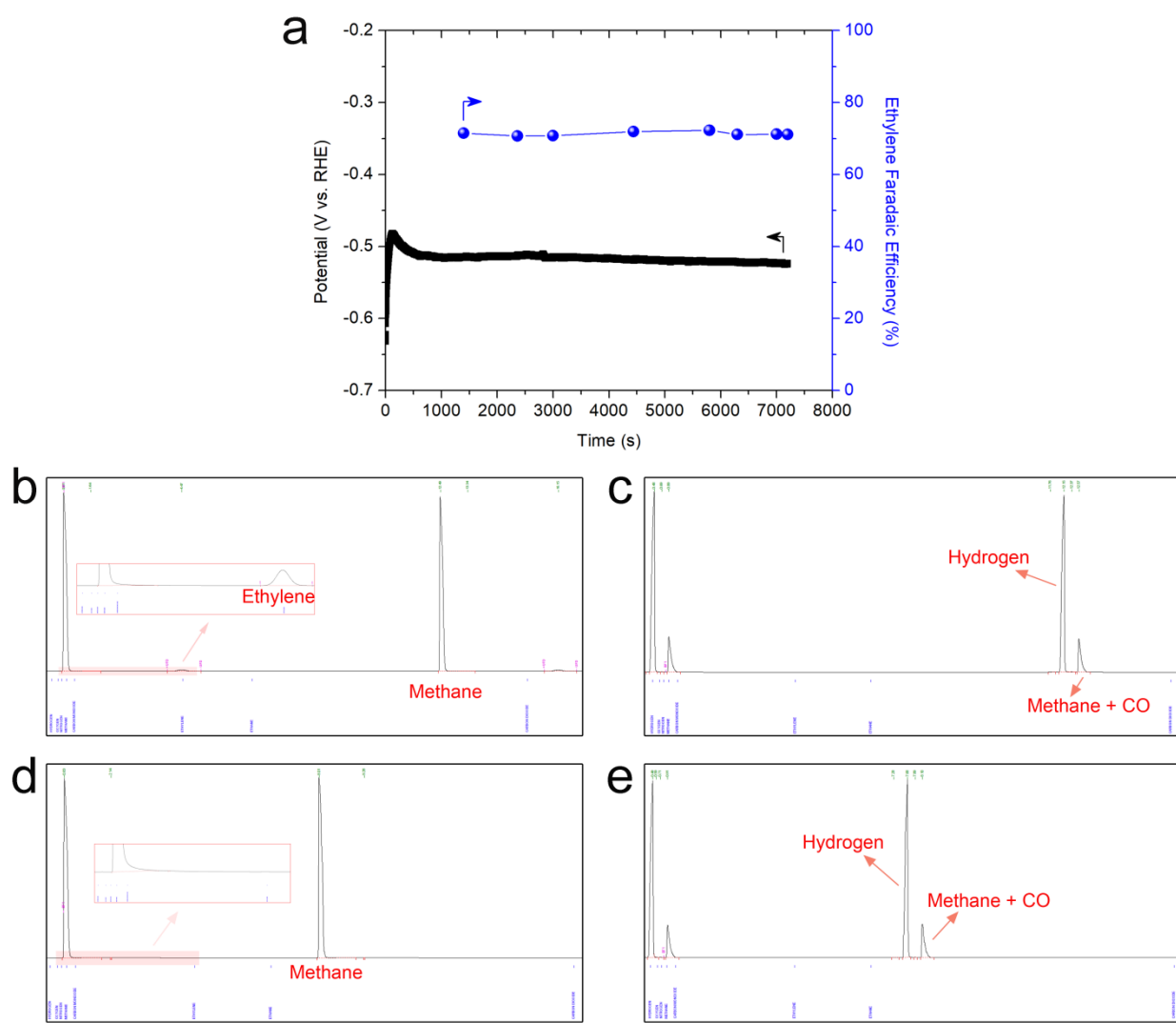
Supplementary Fig. 30. Normalized FE_{ethylene} at different CO pressures as a function of applied potential in 1 M KOH.



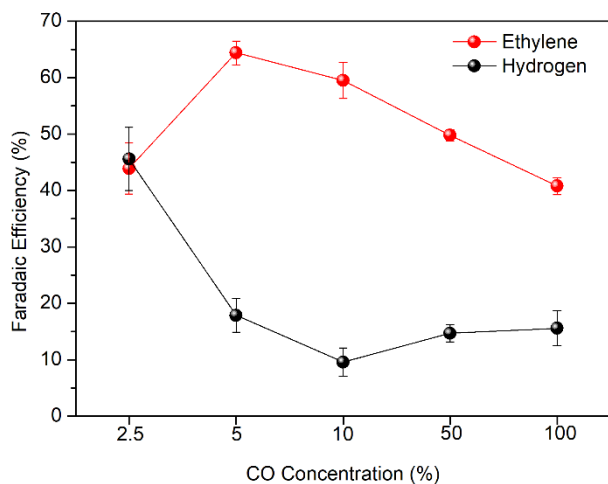
Supplementary Fig. 31. Current densities (mA cm^{-2} , left) & simulated pH at catalyst surface (right) from CORR at different CO concentrations operating at a fixed potential of -0.44 V vs. RHE in 1 M KOH .



Supplementary Fig. 32. a, Ethylene Faradaic efficiency as a function of applied current density at 1 M KOH using pure CO (100%), in which FE_{Ethylene} peaks at 1250 mA cm^{-2} . **b**, Faradaic efficiencies of CORR products at different CO concentrations at a constant current density of 1250 mA cm^{-2} in 1 M KOH. When CO concentration is decreased, keeping the reaction rate at the level corresponding to peak ethylene FE for 100% CO input, mass transport limitations result in lower ethylene selectivity.



Supplementary Fig. 33. A representative CORR test using simulated coke oven gas. a. A selective ethylene production from CORR using simulated coke oven gas (10% CO + 30% CH₄ + 60% H₂) in 1 M KOH at a constant current density of 150 mA cm⁻². **b, c,** Representative GC traces of CORR gaseous products by feeding simulated coke oven gas from FID (**b**) and TCD (**c**) channels. **d, e,** Representative GC traces of simulated coke oven gas from FID (**d**) and TCD (**e**) channels for comparison.



Supplementary Fig. 34. Faradaic efficiencies of CORR products at different CO concentrations at a constant current density of 120 mA cm^{-2} in 1 M KOH using commercial polycrystalline Cu ($\sim 100 \text{ nm}$ particle size, *Sigma Aldrich*). Error bars are means $\pm$ SD ($n = 3$ replicates).

Supplementary Table 1. Summary of ethylene electroproduction efficiency from CO₂/CO reduction.

Catalyst	Reaction and cell type	Electrolyte	FE _{C₂H₄} (%)	<i>j</i> _{C₂H₄} (mA cm ⁻²)	Potential (V vs. RHE)	Cathodic energy efficiency (%)
This work	5% CORR in flow cell	1 M KOH	72	87	-0.52	44
	100% CORR in flow cell	1 M KOH	65	808	-0.72	35
Oxide derived Cu ¹	100% CORR in flow cell	1 M KOH	44	462	-0.72	24
Copper acetate derived Cu ²	100% CORR in H-cell using a gas diffusion electrode	10 M KOH	16	50	-0.78	8.4
Abrupt Cu interface ³	100% CO ₂ RR in flow cell	10 M KOH	66	184	-0.54	44
CuAg alloy ⁴	100% CO ₂ RR in flow cell	1 M KOH	55	172	-0.68	30
Electro-redeposited Cu ⁵	100% CO ₂ RR in flow cell	1 M KOH	36	161	-1	17
Nanoporous Cu film ⁶	100% CO ₂ RR in flow cell	1 M KOH	38	72	-0.6	22

Supplementary Note 1

The calculation of half-cell cathodic energy efficiency (CEE) is based on the assumption of a zero overpotential of the oxygen evolution reaction at the anode side, which is shown in equation below^{3,7}:

$$CEE = \frac{(1.23 + (-E_{C_2H_4})) * FE_{C_2H_4}}{1.23 + (-E)} \quad (1)$$

Where $E_{C_2H_4} = 0.17$ V is the thermodynamic potential (vs. RHE) of CO reduction to ethylene ($E_{C_2H_4} = 0.08$ V for CO₂ reduction); $FE_{C_2H_4}$ is the Faradaic efficiency of ethylene production; E is the applied potential vs. RHE.

Supplementary Note 2

The degree of unsaturation (DU) is defined as:

$$DU = 1 + \frac{\sum n_i(v_i-2)}{2} \quad (2)$$

where n_i is the number of atoms with valence v_i .

Supplementary Note 3

The volume concentration of CO and OH⁻ in the electrolyte was simulated using a 1D reaction-diffusion model. The governing equations:

$$\frac{\partial[CO]}{\partial t} = D_{CO} \frac{\partial^2[CO]}{\partial x^2} - R_{CO} \quad (3)$$

$$\frac{\partial[OH]}{\partial t} = D_{OH} \frac{\partial^2[OH]}{\partial x^2} - R_{OH} \quad (4)$$

were solved in COMSOL (COMSOL Multiphysics v5.3a, Stockholm, Se) using the transport of dilute species physics for a domain size of 500 μm with a 5 μm catalyst at x=0, where D_{CO} and D_{OH} are the CO and OH⁻ diffusivities, and R_{CO} and R_{OH} account for the CO reduction and OH⁻ production in the catalyst layer.

$$R_{CO} = \frac{[CO]}{[CO_{sat}]} \frac{j}{F} \frac{\epsilon}{L_{catalyst}} \sum \frac{FE_{CORR}}{ne_{CORR}} \quad (5)$$

$$R_{OH} = \frac{j}{F} \frac{\epsilon}{L_{catalyst}} \quad (6)$$

where $[CO_{sat}]$ is the saturation concentration of CO based on the KOH concentration (to account for Sechenov salting out effects), as well as on the temperature and partial pressure (according to Henry's law), j is the current density, F is Faraday's constant, ϵ is the porosity, FE_{CORR} is the total CORR FE, and ne_{CORR} is the number of electrons transferred per CO molecule consumed. The transport simulation assumes a uniform, porous catalyst, across which the volume concentration is determined and does not take into account pore-scale concentration variation or surface species concentration. A no flux boundary condition is applied for OH⁻ at x=0, and $[OH^-] = [KOH]$ at x=500 μm. For CO, a flux condition is applied at x=0 to simulate mass transfer at the gas-liquid interface:

$$\frac{\partial[CO]}{\partial x} = ka ([CO_{sat}] - [CO]) \quad (7)$$

where ka is the mass transfer coefficient (equal to $1\text{e-}4\text{ m s}^{-1}$), and $[\text{CO}] = 0$ at $x=500\text{ }\mu\text{m}$. Simulations are time-dependent and run until steady-state occurs ($\sim 10^3\text{ s}$).

Supplementary References

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